# ElectronicDesig <br> VOL. 14, NO <br> THE MAGAZINE OF ESSENTIAL NEWS, PRODUCTS AND TECHNOLOGY 



STIMILGEENERTOORS -oscillators, squarewave, pulse, sweep and noise generatorsover 1500 are on the market.

Next time you need one, check this special reference issue first. Comprehensive specs, prices and technical articles will make you a more informed buyer and user.


If you simply need something that will put out a signal at some frequency with reasonable accuracy, buy one of our many oscillators. But if you want superior performance in a truly versatile laboratory signal source that can tackle practically any job, you want one of our synthesizers - the $70-\mathrm{MHz}$ Type $1164-\mathrm{A}$, or one our other models that cover ranges up to $100 \mathrm{kHz}, 1 \mathrm{MHz}$, and 12 MHz .

These synthesizers give you quartz-crystal stability, a frequency settable from 3 to 9 figures or more, manual or electrical sweeping, flat output, and programmability (if you need it). In short, these signal sources will do the job for you with a minimum of complications and without need for time-consuming corrections to improve accuracy of results - yet the price is within reach.

## Here are features of our $70-\mathrm{MHz}$ synthesizer, the latest in our series:

## - Frequencies Up To 70 MHz

$10-\mathrm{kHz}$ to $70-\mathrm{MHz}$ output with resolution as fine as 0.1 Hz . Internal crystal-controlled oscillator may be phase-locked to external standard frequency.

## - Electrical Sweeping and Manual-Search Capabilities

Continuously Adjustable Decade (CAD) allows a portion of the frequency range to be swept manually or electrically. The CAD will functionally replace any digit up to 1 MHz for sweep widths from a megahertz to a fraction of a hertz. This module also adds at least 2 places of resolution beyond the last decade.

## - Leveled, Monitored Output That Can Be Remotely Or Manually Controlled

Output is adjustable from 0.2 to 2 V behind $50 \Omega$ and is monitored by a panel meter. Level is held constant within $\pm 0.3 \mathrm{~dB}$ for all load and frequency variations and can be adjusted manually from the front panel or remotely by a potentiometer or a dc control voltage.

- Modular Construction

Buy only the resolution you require; add modules as your requirements expand. Modules may be easily removed or interchanged for servicing or calibration to cut down time to practically zero.

## - Other Features

Remotely programmable (optional) . . Can operate from ac line or battery for field use . . . In-line, easy-to-read numerals . . . GR-quality construction... All in $5 \frac{1}{4}$ inches of rack space.

- Now Look At The Price

Prices start at $\$ 4745$ for the simplest 3-decade, 70 MHz model; the most complete model costs $\$ 7515$.

## Other GR synthesizers in the series:

Type 1161 - dc to $100-\mathrm{kHz}$ Synthesizer Type 1162 - dc to $1-\mathrm{MHz}$ Synthesizer Type $1163-30-\mathrm{Hz}$ to $12-\mathrm{MHz}$ Synthesizer
\$3640 to \$6590 \$3775 to \$6725 $\$ 3895$ to $\$ 6755$

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WEST CONCORD, MASSACHUSETTS ON READER-SERVICE CARD CIRCLE 161

# Signal Generator Reterence issue 

David H. Surgan New Products Editor

This directory is valuable. Use it properly, and you can make an intelligent, comparative instrument selection from the 1500 signal sources currently available.
Tables of specifications, including prices, have been supplied by the Technical Information Corp., P. O. Box 514, Smithtown, N. Y. They are up-to-date, complete and specific. Check them before you buy.
In addition, there are four technical articles, written by engineers at Tektronix, General Radio, Polarad and Marconi. They will help you "read between the lines" and develop an applications-oriented point of view.
To make the best use of the directory, follow this easy procedure:

- Compare the specs and get a feeling for performance/cost ratios.
- Bring your literature file up-to-date by using the Master Cross Index on page 4
- Follow the selection-application guidelines offered in the articles.

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## How to Use the Tables

The tables in this directory have been arranged for simple and rapid reference. Each table covers a particular type of signal generator, and lists pertinent technical specifications for instruments of that type. Unless otherwise specified in the tables, the following condition applies to all the instruments listed:

- Input voltage: 105-125 Vac, $60 \mathrm{~Hz}, 1$ phase

Prices indicated in the tables are subject to change by the manufacturer.
An index of manufacturers and models is included at the end of each table. These indexes are alphabetical, by manufacturer, and list the various instruments of each manufacturer. A location key is included after each model in the index. This permits easy spotting in the table of the specifications for that instrument, by means of the location-key column (first column) in the table.

## How the tables are arranged

Within the tables, instrument specifications are given in separate, appropriately headed columns. The complete specifications for any one instrument can thus be read across the page.
For each table the instruments are listed in ascending order of upper frequency limit. To facilitate table use, the columns containing this parameter are tinted. In cases where the upper frequency limit of several units is the same, the instruments are listed in increasing order of frequency swing.
Manufacturers are identified in the Mfr. column by an abbreviation. The complete name of each manufacturer can be found in the index at the end of the section. For manufacturers' addresses and Reader Service literature offerings, see the master index, which starts on page 4.
All notes and symbols used in a table are defined at the end of that table.
At the top of each page of a table the frequency range covered by the instruments listed on that page is specified. This is to expedite the location of a unit having a particular frequency output.

## To use the tables effectively

1. Note how the instruments are listed.

They are in ascending order of upper frequency limit. Where this is the same, they are in order of increasing frequency swing.
2. Select the most likely candidates.
3. Obtain supplementary data from the manufacturer.

Manufacturers' addresses, together with Reader-Service numbers for specific types of signal generators, are given in the master cross index.

[^0]

## FACTS MAKE FEATURES:

Popular streamlined tester with long meter scales arranged for easy reading. Fuse protected.
Single control knob selects any of 32 ranges-less chance of incorrect settings and burnouts.
Four resistance ranges-from .1 ohm reads direct; $41 / 2$ ohm center scale; high 100 megohms.

Attention to detail makes the Triplett Model $630 \mathrm{~V}-\mathrm{O}-\mathrm{M}$ a lifetime investment. It has an outstanding ohm scale; four ranges-low readings .1 ohm, high 100 megs. Fuse affords extra protection to the resistors in the ohmmeter circuit, especially the XI setting, should too high a voltage be applied. Accuracy $2 \%$ DC to 1200 V . Heavy molded case.
${ }^{\dagger} 630 \mathrm{~A}$ same as 630 plus $11 / 2 \%$ accuracy and mirror scale only $\$ 6500$ TRIPLETT ELECTRICAL INSTRUMENT COMPANY, BLUFFTON, OHIO

## RANGES

| DC VOLTS | $0-3-12-60-300-1,200-6,000$ <br> at 20,000 ohms per volt. |
| :--- | :--- |
| AC VOLTS | $0-3-12-60-300-1,200-6000$ <br> at 5,000 ohms per volt. |
| OHMS | $0-1,000-10,000$. |
| MEGOHMS | $0-1-100$. |
| DC MICRO- <br> AMPERES | $0-60$ at 250 millivolts. |
| DC MILLI- <br> AMPERES | $0-1.2-12-120$ at 250 millivolts. |
| DC AMPERES | $0-12$. |

DB: -20 to +77 ( 600 ohm line at 1 MW ).
OUTPUT VOLTS: 0-3-12-60-300-1,200; jack with condenser in series with $A C$ ranges.


630

630.A


630-PI


630-APL


630-1



630-m


THE WORLD'S MOST COMPLETE LINE OF V-O-M'S. AVAILABLE FRON YOUR TRIPLETT DISTRIBUTOR'S STOCK.

## Master Cross Index

Manufacturers of the product types listed in this issue are indicated either by stars or by Reader Service numbers (if supplementary literature is available). Bring your literature file up to date by circling the appropriate numbers on the Reader Service card at the back of the issue.

| Manufacturer |  | Oscillator | Signal | Noise | Pulse | Sweep | Squarewave | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Address | Abbreviation |  |  |  |  |  |  |  |
| Adar Associates 73 Union Square Somerville, Mass | Adar |  |  |  | $\star$ |  |  |  |
| Advanced Measurement Instruments Inc 109 Dover St Somerville, Mass | AMI |  | 1 |  |  | 2 |  |  |
| Aerospace Research, Inc 130 Lincoln St Boston, Mass | ARI |  |  | 3 |  |  |  |  |
| Airborne Instrument Laboratory Comac Rd Deer Park, LI, NY | Airborne | 4 |  | 5 |  |  |  |  |
| Aircraft Radio Corp Rockaway Valley Rd Boonton, NJ | Aircraft Radio |  | * | , |  |  |  |  |
| Alfred Electronics 3176 Porter Drive Palo Alto, Calif | Alfred |  |  |  | 6 | 7 | 8 |  |
| Allison Laboratories, Inc 11301 Ocean Ave La Hambra, Calif | Allison |  |  | 9 |  |  |  |  |
| American Electronic Labs, Inc P.O. Box 552 Lansdale, Pa | AEL |  |  |  | $\star$ |  |  |  |
| Anadex Instruments, Inc 7833 Haskell Ave Van Nuys, Calif | Anadex |  |  |  |  |  | 10 |  |
| Antlab, Inc 6330 Proprietors Rd Worthington, Ohio | Antlab |  |  |  |  |  | $\star$ |  |
| Applied Microwave Laboratory 106 Albion St Wakefield, Mass | App <br> Microwave | 11 |  |  |  |  |  |  |
| Arenburg Ultrasonic Lab, Inc 94 Green St Jamaica Plain, Mass | Arenburg | 12 |  |  |  |  |  |  |
| Argonaut Associates, Inc P.O. Box 273 <br> Beaverton, Ore | Argonaut |  |  |  |  |  |  | 13 |
| B \& K Instruments, Inc 5111 W. 164th St Cleveland, Ohio | $B \& K$ | * |  | $\star$ |  |  |  |  |
| Babcock Electronics Corp 3501 Harbor Blvd Costa Mesa, Calif | Babcock |  | 14 |  |  |  |  |  |
| Barker \& Williamson, Inc Canal St \& Beaver Dam Rd Bristol, Pa | B \& W | 15 |  |  |  |  |  |  |


| Manufacturer |  | Oscillator | Signal | Noise | Pulse | Sweep | Squarewave | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Address | Abbreviation |  |  |  |  |  |  |  |
| Beckman Instruments, Inc Computer Operations 2200 Wright Ave Richmond, Calif | Beckman |  |  | $\star$ |  |  |  |  |
| Berkeley Nucleonics Beckman Instruments, Inc 1429 Oregon Street Berkeley, Calif | Berkeley |  |  |  | $\star$ |  |  |  |
| Blonder-Tongue Labs, Inc 9 Alling St <br> Newark, NJ | Blonder <br> Tongue |  |  |  |  | ไ |  |  |
| Canoga Electronic Products 1805 Colorado Ave Santa Monica, Calif | Canoga |  |  |  |  |  |  | $\star$ |
| Century Electronics \& Instruments 6540 E. Apache <br> Tulsa, Okla | Century | 16 |  |  |  |  | 17 |  |
| Chesapeake Instrument Corp Shadyside, Md | Chesapeake |  |  |  | 18 |  |  |  |
| Clough-Brengle Co 6014 Broadway Chicago, III | Clough- <br> Brengle | 19 | 20 |  |  | 21 |  |  |
| Datapulse, Inc 509 Hindry Ave Inglewood, Calif | Datapulse |  |  |  | 22 |  |  |  |
| De Mornay-Bonardi Corp 1313 N. Lincoln Ave Pasadena, Calif | D-B |  |  | 23 |  |  |  |  |
| Digital Electronics Ames Court, Engineers Hill Plainview, NY | Digital Elect |  |  |  | 24 |  |  |  |
| Dymec Division Hewlett-Packard Co 395 Page Mill Rd Palo Alto, Calif | Dymec |  | 25 |  |  |  |  |  |
| Dynatronics <br> P.O. Box 2566 <br> Orlando, Fla | Dynatronics |  | 26 |  |  |  |  |  |
| E-H Research Laboratories, Inc 163 Adeline St Oakland, Calif | E-H |  |  |  | 27 | 28 |  |  |
| ENSCO, Inc 3100 Eldridge St Salt Lake City, Utah | ENSCO |  |  |  | 33 |  | 34 |  |
| EPSCO, Inc 411 Providence Highway Westwood, Mass | EPSCO |  | $\star$ |  |  | $\star$ |  |  |
| Electro Design, Inc 8141 Engineer Rd San Diego, Calif | Electro Design |  |  |  | $\star$ |  |  |  |
| Electronic Instrument Co, Inc 131-01 39th Ave Flushing, NY | EICO | 29 | 30 |  |  | 31 | 32 |  |
| Electronic Measurements Corp 625 Broadway <br> New York, NY | EMC |  | $\star$ |  |  |  |  |  |


| Manufacturer |  | Oscillator | Signal | Noise | Pulse | Sweep | Squarewave | Function |
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| Address | Abbreviation |  |  |  |  |  |  |  |
| Elgenco, Inc 1550 Euclid St Santa Monica, Calif | Elgenco |  |  | 35 |  |  |  |  |
| Empire Products Singer Metrics Division 915 Pembroke St Bridgeport, Conn | Empire |  |  | 36 |  |  |  |  |
| Exact Electronics, Inc 455 S.E. Second Ave Hillsboro, Ore | Exact |  |  |  |  |  |  | 37 |
| Fairchild Instrumentation 750 Bloomfield Ave Clifton, NJ | Fairchild |  |  |  | 38 |  | 39 |  |
| Frequency Engineering Lab P.O. Box 527 <br> Farmingdale, NJ | FEL | 40 |  |  |  |  |  |  |
| General Applied Science Labs Merrick \& Stewart Aves Westbury, NY | GASL |  |  |  | $\star$ |  |  |  |
| General Electric Co 40 Federal St <br> West Lynn, Mass | GE |  |  |  |  | $\star$ |  |  |
| General Microwave Corp 155 Marine St Farmingdale, NY | Gen Micro |  |  | 41 |  |  |  |  |
| General Radio Co 22 Baker St Concord, Mass | Gen Radio | 42 | 43 | $44^{\circ}$ | 45 | 46 | 47 |  |
| Gertsch Products Singer-Metrics Div 3211 La Cienega Blvd Los Angeles, Calif | Gertsch |  | 48 |  |  |  |  |  |
| Grundig 150 Nassau St New York, NY | Grundig | $\star$ | $\star$ |  |  | $\star$ |  |  |
| Hallicrafters Co 4401 W. 5th Ave Chicago, III | Hallicrafters | * |  |  |  |  |  |  |
| Hathaway Instruments, Inc 5250 E. Evans Ave Denver, Colo | Hathaway | 158 |  |  |  |  |  |  |
| Heath Co <br> Hilltop Rd <br> Benton Harbor, Mich | Heath | 49 | 50 |  |  | 51 | 52 |  |
| Hewlett-Packard Co 1501 Page Mill Rd Palo Alto, Calif | H-P | 53 | 54 | 55 | 56 | 57 | 58 | 59 |
| Hickok Electrical Instrument Co 10514 Dupont Ave Cleveland, Ohio | Hickok |  | 60 |  |  | 61 | 62 |  |
| Holt Instrument Labs P.O. Box 230 Oconto, Wis | Holt | 63 |  |  |  |  |  |  |


| Manufacturer |  | Oscillator | Signal | Noise | Pulse | Sweep | Squarewave | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Address | Abbreviation |  |  |  |  |  |  |  |
| Houston Omnigraphic Corp 4950 Terminal Ave Bellaire, Texas | Houston |  |  |  |  |  |  | 64. |
| Huggins Laboratories, Inc 999 E. Argues Ave Sunnyvale, Calif | Huggins |  |  |  | 65 |  |  |  |
| ITT Industrial Products Division 15151 Bledsoe St San Fernando, Calif | ITT | $\star$ |  | * |  | $\star$ |  |  |
| Industrial Components, Inc 1675 S.E. Allen Ave Beaverton, Ore | Ind Comp |  |  |  |  |  | 66 |  |
| Industrial Test <br> Equipment Co 20 Beechwood Ave Port Washington, NY | Ind Test Equip | 67 |  |  |  |  |  |  |
| Intercontinental Instruments, Inc 500 Nuber Ave <br> Mount Vernon, NY | Intercontinental |  |  |  | 68 |  |  |  |
| International Electronic Research Corp 135 Magnolia Blvd Burbank, Calif | IERC | $\star$ |  |  |  |  |  |  |
| Jerrold Electronics Corp 15th \& Lehigh Philadelphia, Pa | Jerrold | $\star$ |  |  |  | * |  |  |
| Kay Electric Co Maple Ave Pine Brook, NJ | Kay | 69 | 70 | 71 | 72 | 73 |  |  |
| Krohn-Hite Corp 580 Massachusetts Ave Cambridge, Mass | Krohn-Hite | 74 |  |  |  |  | 75 | 76 |
| Kruse-Storke Electronics 790 Hemmeter Lane Mountain View, Calif | KruseStorke | 155 |  |  |  | 156 |  |  |
| LTV Ling Electronics Div Ling-Temco-Vought 1515 S. Manchester Ave Anaheim, Calif | LTV Ling |  |  |  |  | 77 |  |  |
| Laboratory For Electronics, Inc 1075 Commonwealth Ave Boston, Mass | LFE | 78 |  |  |  | 79 |  |  |
| MSI Electronics, Inc 116-06 Myrtle Ave Richmond Hill, NY | MSI |  |  |  |  | 7 |  |  |
| Marconi Instruments 111 Cedar Lane Englewood, NJ | Marconi | 80 | 81 | 82 |  | 83 | 84 |  |
| Measurements P.O. Box 180 Boonton, NJ | Measurements | 85 | 86 |  | 88 |  |  |  |
| Microdot, Inc 220 Pasadena Ave <br> S. Pasadena, Calif | Microdot | 89 | 90 |  |  |  |  |  |
| Micro-Power, Inc 25-14 Broadway Long Island City, NY | Micro-Power |  |  |  |  | 91 |  |  |


| Manufacturer |  | Oscillator | Signal | Noise | Pulse | Sweep | Squarewave | Function |
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| Address | Abbreviation |  |  |  |  |  |  |  |
| Monsanto Electronics Department 800 N. Lindbergh Blvd St. Louis, Missouri | Monsanto |  |  |  | 92 |  |  |  |
| Motorola Comm \& Elect, Inc 4501 W. Augusta Rd Chicago, III | Motorola |  | 93 |  |  |  |  |  |
| Muirhead Instruments, Inc 111 Bristol Rd Mountainside, NJ | Muirhead | 94 |  |  |  |  |  |  |
| Narda Microwave Corp Commercial St Plainview, NY | Narda | 95 |  |  |  | 96 |  |  |
| Navigation Computer Corp Valley Forge Indl Park Norristown, Pa | Nav Comp | 97 |  |  |  |  |  |  |
| Northeast Electronics Corp Airport Rd Concord, NH | Northeast |  |  | $\star$ |  |  |  |  |
| Optimation, Inc 7243 Atoll Ave <br> N. Hollywood, Calif | Optimation | 98 |  |  |  |  |  |  |
| PRD Electronics, Inc 1200 Prospect Ave Westbury, NY | PRD | 99 |  | 100 |  |  |  |  |
| Piezo Technology 2400 Diversified Way Orlando, Fla | Piezo |  | $\star$ |  |  | \% |  |  |
| Polarad Electronic Instruments 34-02 Queens Blyd Long Island City, NY | Polarad | 101 | 102 | 103 | 104 | 105 |  |  |
| Precise Electronics \& Development Corp 76 E. 2nd St <br> Mineola, NY | Precise |  | 106 |  |  |  | 107 |  |
| Precision Apparatus Co, Inc 80-00 Cooper Ave Glendale, NY | Prec Apparatus | 108 |  |  |  | 109 | 110 |  |
| Probescope Co 211 Robbins Lane Syosset, NY | Probescope | $\star$ |  |  |  | * |  |  |
| RCA, Electronic Components \& Devices 415 S. 5th St Harrison, NJ | RCA | 112 | 113 |  |  | 114 | 115 |  |
| RFD, Inc 1501 W. Cass St Tampa, Fla | RFD | $\star$ |  |  |  |  |  |  |
| RS Electronics Corp 795 Kifer Rd Sunnyvale, Calif | RS |  | $\star$ |  |  |  |  |  |
| Radar Engineers 4719 Brooklyn Ave N.E. Seattle, Wash | Radar Engr |  |  |  | 116 |  |  |  |
| Radiometer Electronics The London Co 811 Sharon Drive Westlake, Ohio | Radiometer | 117 | 118 |  |  |  |  |  |


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| Address | Abbreviation |  |  |  |  |  |  |  |
| Rohde \& Schwarz Sales Co, Inc 111 Lexington Ave Passaic, NJ | R \& S | 119 | 120 | 121 |  | 122 |  |  |
| Rutherford Electronics Co 8944 Lindblade St Culver City, Calif | Rutherford |  |  |  | $\star$ |  |  |  |
| Schlumberger c/o E.F. Associates 100 Quimby St Westfield, NJ | Schlumberger | $\star$ |  |  |  |  |  |  |
| Scientific-Atlanta, Inc P.O. Box 13654 Atlanta, Ga | S-A | 123 |  |  |  |  | 124 |  |
| H. H. Scott 121 Powdermill Rd Maynard, Mass | HH Scott |  |  | 157 |  |  |  |  |
| Servo Corp of America 111 New South Rd Hicksville, NY | Servo |  |  |  | $\star$ | $\star$ |  | $\star$ |
| Siemens America, Inc 350 Fifth Ave New York, NY | Siemens | 125 |  |  |  |  |  |  |
| Sierra Electronic Div Philco Corp 3885 Bohannon Dr Menlo Park, Calif | Sierra | 126 | 127 |  |  |  |  |  |
| Signalite, Inc 1933 Heck Ave Neptune, NJ | Signalite |  |  | 128 |  |  |  |  |
| Smyth Research Assoc 3555 Aero Court San Diego, Calif | Smyth |  | 129 |  |  |  |  |  |
| Spectral Dynamics Corp 8159 Engineers Rd San Diego, Calif | Spectral Dynamics |  |  |  |  | 130 |  |  |
| Spencer-Kennedy Labs, Inc 1360 Soldiers Field Rd Boston 35, Mass | S-K |  |  |  | $\star$ |  |  |  |
| Stewart Bros Division Instrument Laboratories Corp 315 W. Walton Place Chicago, III | Stewart | 131 |  |  |  |  |  |  |
| Stoddart Electro Systems Div Tamar Electronics 2045 W. Rosecrans Ave Gardena, Calif | Stoddard |  |  | 132 |  |  |  |  |
| Strand Laboratories, Inc 143 Main St Cambridge, Mass | Strand | 133 |  |  |  |  |  |  |
| Technical Materiel Corp 700 Fenimore Rd Mamaroneck, NY | Tech Materiel | 153 |  |  |  |  |  |  |
| Tektronix, Inc <br> P.O. Box 500 <br> Beaverton, Ore | Tektronix | 134 |  |  | 135 |  | 136 |  |
| Tel-Instrument Electronics Corp 728 Garden St <br> Carlstadt, NJ | Tel-Inst |  | 137 |  |  | 138 |  |  |


| Manufacturer |  | Oscillator | Signal | Noise | Pulse | Sweep | Squarewave | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Address | Abbreviation |  |  |  |  |  |  |  |
| Telonic Industries, Inc 60 N. First Ave Beech Grove, Ind | Telonic |  |  |  |  | 139 |  |  |
| Texas Instruments, Inc 3609 Buffalo Speedway Houston, Texas | Texas Inst |  |  |  | 140 |  |  |  |
| Texscan Corp 51 S. Koweba Lane Indianapolis, Ind | Texscan |  |  |  |  | 141 |  |  |
| Triplett Electrical Instruments 286 Harmon Rd Bluffton, Ohio | Triplett |  | 142 |  |  |  |  |  |
| Velonex Instrument Div Pulse Engineering, Inc 560 Robert Ave Santa Clara, Calif | Velonex |  |  |  | 111 |  |  |  |
| Walkirt <br> 10321 S. La Cienega Blvd Los Angeles, Calif | Walkirt |  |  |  | 4 |  |  |  |
| Wang Laboratories, Inc 836 North St Tewksbury, Mass | Wang |  |  |  | 143 |  |  |  |
| Waveforms, Inc 333 6th Ave New York, NY | Waveforms | 144 |  |  |  | 145 |  |  |
| Waveline, Inc P.O. Box 718 W. Caldwell, NJ | Waveline |  |  | 146 |  |  |  |  |
| Wavetek, Inc 8133 Engineer Rd San Diego, Calif | Wavetek |  |  |  |  |  |  | 154 |
| Wayne-Kerr Corp 18-22 Frink St Montclair, NJ | Wayne-Kerr | $\star$ |  |  |  |  |  |  |
| Weinschel Engineering Co, Inc P.O. Box 577 <br> Gaithersburg, Md | Weinschel | 147 |  |  | 148 | 149 | 150 |  |
| Weston, Boonshaft \& Fuchs Hatboro Industrial Park Hatboro, Pa | Weston | 151 |  |  |  |  |  |  |
| Wiltron Co 930 Meadow Drive Palo Alto, Calif | Wiltron |  |  |  |  | 152 |  |  |



What's the charge?

CHFTN1 ALKYD
the better molding compound for electricalelectronic products

Here's why GLASKYD glass-reinforced alkyd compounds in continuous rope and cut slug form gain wider acceptance every day: - excellent dielectric strength dimensional stability ${ }^{\text {• resistance to }}$ heat, flame and moisture - wide choice of colors.
GLASKYD offers economy through new, automated cold plunger molding - with fast cure, short cycles, high production rates. This alkyd also can be molded by compression or transfer techniques.
Widely used in such applications as electrical housings, connectors, coil bobbins and strips, switches and collector rings, GLASKYD also is ideal for arc-less switches, phase barriers, brush holders and tuner strips.
Rope in new markets, new product quality - with GLASKYD.
For details, write:


# Buying a pulse generator? These systematic guidelines will take the guesswork out of selecting. 

As a prospective buyer of a pulse generator, you are confronted by more than 100 different models, some of which emphasize some features at the expense of others. If you want the best pulse generator and the best set of trade-offs for your dollar, use a systematic approach to selection. Three basic elements are involved:

- Specifying the characteristics the job calls for.
- Selecting a generator with these characteristics.
- Worst-case testing of a loan instrument.

But before you can begin specifying the pulse generator, you must know your applications.

## Performance, cost and function must be balanced

At times all that is required is a repetitive trigger with a few adjustable characteristics. A low-cost pulser may fill the bill here. When the pulse generator is needed as a general signal source for circuit development, cleanliness of waveshape may be the most important attribute. However, features such as variable dc baseline offset, variable rise and fall times, and pretrigger output might all be considered. For use in triggering multivibrators, pulse shape is not important within wide limits, but period may well be. In the calibration of other instruments, accuracy and cleanliness may both be important. For repetitive testing requiring more than one type of pulse, one might consider a pulse generator with programing. Programing can eliminate the need for two or more pulse generators, by permitting quick selection of various types of preadjusted pulses. In general, variable rise and fall times make it possible to test circuits more nearly under actual operating conditions, or to check response to trigger variations. This feature is becoming more generally available.

Other features that are useful in some applications include trigger input, delayed pulse, double

[^1]pulse, pulse bursts, simultaneous positive and negative polarity pulses and calibrated controls. Some generators have a control calibrated for period, which may be a more convenient reading than repetition rate. Period is easily related to pulse width and may be determined directly from an oscilloscope. Repetition rate is more conveniently related to a frequency counter.

When buying one particular feature, be aware of the other specs that may suffer. For example, before specifying more amplitude than required, consider which trade-offs accompany high voltage and fast rise time in the same instrument. These generators are usually high-power units meant for driving $50-\Omega$ loads. An instrument with a clean $50-\mathrm{V}$ output will often produce a very degraded pulse at lower amplitude. It may be impossible to get a clean low-voltage pulse even with an attenuator. Clean, high-frequency, $50-\Omega$ attenuators are simply not available at power ratings of greater than 2 to 5 W . This means that even moderate duty cycles from a $50-\mathrm{V}$ generator cannot be attenuated cleanly for lower voltage applications. However, you can easily attenuate a $10-\mathrm{V}$ pulse at high duty cycles with the low-power attenuators.

## A look beyond the spec sheet is necessary

Some specifications of pulse-generator characteristics are straightforward and easy to understand. Other specifications are often incomplete or misleading, and, in some instances, some characteristics are not even mentioned. Two categories cover most of the parameters that define the pulse output: (1) The range of adjustment, and (2) How the pulse deviates from ideal.

Adjustment ranges: This category may include maximum and minimum limits in adjusting pulse amplitude, pulse width, pulse period (or repetition rate) and rise time, fall time, or delay time. Expect a specification in this category to be straightforward, but not always-for example, maximum pulse amplitude. A spec that states $10-\mathrm{V}$ peak from a $50-\Omega$ source might imply a $5-\mathrm{V}$ pulse when the


1. Waveform distortions do exist, no matter how ideally the pulse is specified.
output is terminated in $50 \Omega$. Specifying the amplitude into a $50-\Omega$ load, and also specifying the opencircuit amplitude, is clearer. At times the spec sheet may be clear enough, but the buyer may not stop to relate one spec to another. For example, if a certain period (or repetition rate) is required, it is important to check whether a maximum duty cycle limitation of the pulse generator will limit operation to too short a pulse width.

Waveform: No matter how ideally the pulse output is specified, distortions do exist (Fig. 1). They include:

- Preshoot-the initial excursion of the waveform which precedes the leading or trailing edge. It may be of the same or opposite polarity.
- Rise time-the interval between the instances at which the instantaneous pulse amplitude first reaches specified lower and upper limit. Unless otherwise stated, these limits are $10 \%$ and $90 \%$ of the pulse's amplitude. Fall time is analogously defined (Fig. 2). Although not distortions, rise and fall times are limitations to be considered in specifying.
- Overshoot-the initial excursion beyond the limiting final value. It occurs simultaneously with the leading or trailing edge.
- Rounding-the lack of a sharp corner of a waveform, or a smooth transition from leading or trailing edge to the limiting final value.
- Ringing-periodic bumps in the waveform that occur after the overshoot. When specified, it may be peak-to-peak, flat top-to-peak or rms. The latter two produce smaller numbers but not less ringing.
- Tilt-an up or down slope to the otherwise flat top, also called top slope or, more commonly, droop. Other flat-top aberrations do exist, but usually they are not specified or even mentioned individually. They are sometimes called "other aberrations" and ideally should be expressed as a percentage of flat-top amplitude. Sometimes they are collected into a single aberrations spec and included with overshoot, ringing and tilt. One such "other aberration" could be called "dribble


2. Rise and fall times are measured at $90 \%$ and $10 \%$ points.
up." This is a gradual creep up to the flat-top amplitude, too slow to be considered rounding. On shorter pulse widths it will look like tilt or up slope, while on very long widths it will look like a rounded corner.

- Dc baseline shift-the change in the dc level of the baseline.
- Baseline aberrations-almost never mentioned. They are spurious signals or noise on the baseline and, if large enough, may cause false triggering or other complications.
- Jitter in pulse period, in pulse width and between a trigger and a pulse output-the time uncertainty of these quantities, usually expressed as a percentage of the time interval.

These waveform anomalies are often unclearly specified or not mentioned. When something is not specified, it may have been overlooked or been deemed not important enough to clutter up the spec sheet. On the other hand, it may be too costly to spec, or even too embarrassing to mention.

Sometimes a waveform photograph will be displayed in place of, or in addition to, some of the specifications. However, you can be fairly certain that a worst-case setup was not made for the photograph. When something is specified as "negligible" or even given as a vague percentage, it may just as well have been omitted.

The only sure way to determine the cleanliness of waveform is to test the pulse generator. In deciding what generators to evaluate, consider future needs and the possibility of including some additional flexibility. Considerations other than cost should be kept in mind.

## Put the pulser through its paces

Testing a pulse generator in your own laboratory is the surest way to determine whether it meets your needs. Examine the construction techniques and estimate maintainability. Look for components that seem to be running excessively hot, as they may signal possible early failure or a reliability problem. The controls of the instrument should


Hundreds of pulsers do hundreds of jobs. Balance performance, cost and function with your application.
be easily interpreted and easy to adjust to the desired waveform. An overlap of ranges is helpful, as is a reasonably linear continuous control. If the control is too nonlinear, there may be too much change in adjustment in some very small knob rotation.

When obtaining an evaluation instrument, check whether there are ways in which it may be unintentionally damaged. For example, the output transistor can often be destroyed by an inductive load, and unless there is built-in protection, a generator may be damaged by shorting the output. A front panel adjustment can wreck some generators by allowing for too high a duty factor at high amplitude. Study the instruction manual, and list those precautions that must be observed for each of the generators being tested.

The most difficult parameters to verify will be the ones involving waveform aberrations. Difficulties arise because of a lack of industry standards in nomeclature, and, in the case of some very clean pulse generators, aberrations in the measuring oscilloscope itself. Know the type and magnitude of aberrations in the scope, so that meaningful results can be obtained.

## Zero in on choice with worst-case tests

Quick verification of the manufacturer's specifications with the use of a scope, clean $50-\Omega$ cables, terminating resistors and attenuators pads should be followed by setting up worst-case conditions for a more critical look. Here, additional care must be taken in choosing the hardware for testing. Mismatched load, cables and connectors can destroy a clean pulse. The following procedure will turn up waveform aberrations under worstcase conditions:

1. Look at the longest-duration (maximumwidth) pulse at maximum amplitude and low-duty cycle. Check for tilt, usually caused by poor design of ac-coupled circuits, and for dribble-up, often caused by thermal time constants. Note any low-


Worst-case testing will turn up waveform aberrations and provide a critical look at the manufacturer's specs.
frequency ( $1-$ to $10-\mu \mathrm{s}$ period) ringing, usually caused by poor decoupling of the power supply feeding high-current switches.
2. Increase the repetition rate to give a $90 \%$ duty cycle (or the generator's specified duty cycle limit). Under some conditions, this limit may be exceeded, but be sure the specifications clearly state that no damage will occur. Check for a baseline shift from the low-duty-cycle dc level. Thermal dribble-up may decrease, since the junction temperature is more constant (constantly higher) at high-duty cycles. Over-all behavior can become erratic due to increased power supply loading for marginally designed power supplies. Finally, watch carefully for any pulse amplitude reduction. Specification of this condition is often circumvented by specification of a maximum-duty-cycle limitation on the instrument. Some generators have no duty cycle limitation, and when pulse width exceeds the selected period, the pulse generator usually counts down (period doubles). The transition interval from normal operation to countdown may be a clean change in mode, or the waveform may become unstable at this point. (Be careful with higher power generators at high duty cycle into low-power terminating resistors or attenuators. Unfortunately most clean attenuators are low-power ( $1 / 2$ to 2 watts). Clean, high-power attenuators are as rare as ideal pulses).
3. At maximum-duty cyle, check and record the faster aberrations and characteristics at appropriately higher sweep speeds. Record such things as rise time, overshoot and ringing at both leading and trailing edges.
4. Reduce the amplitude. Most generators are far cleaner at maximum amplitude. Thus, at a lower amplitude, check carefully for aberrations of the pulse when it is reduced by the variable amplitude controls or by the internal passive attenuators, which are usually switched controls. Also note any baseline shift due to amplitude variation.

## Rutherford

RUTHERFORD HIGH VOLTAGE PULSE GENERATORS ARE THE STANDARD OF THE INDUSTRY

The B-7 series of vacuum tube pulse generators have earned a reputation for high performance precision and reliability. They have the accuracy and versatility to meet today's rigid standards of testing, research and development. They have testing, research and development. They have
proven their capabilities as systems components proven their capabilities as
as well as in field operation.


Model B-7B features rep rates to 2 MHz and out puts of 50 volts into 50 ohms. Printed circuit boards. Variable rise time control. Trouble-free single unit construction. Overload protection. Sta bilized noise-free repetition rate schedule. Rack mountable.


Model B-7D incorporates all of the time-proven spe cifications of the popular Model B.7B with several extra features. Simultaneous positive and negative output pulses are available at front panel connectors. The rise and fall time of each pulse is sepators. The rise and fall time of each pulse is sepa-
rate and independent, and may be degraded withrate and independent, and may be degraded withmay be set to zero by front panel control, or may be offset.


Model B-7F adds the following features to the basic specs of Model B.7B: (1) repetition rate is continuously variable from 2 Hz to 2 MHz ; (2) output pulse rise or fall time may be independently degraded to approx. $1 \mu \mathrm{sec}$; (3) either single or double pulse output available by front panel control.

## NEW-REMOTELY PROGRAMMABLE PULSE GENERATOR



Model PPG3 is the only solid-state, digitally con trolled programmable pulse generator of its type. No other automatic pulse generator offers the degree of accuracy, stability, reliability, or range of easy operation. It exceeds requirements of today's most sophisticated automatic checkout systems. All major parameters may be programmed, sequentially or in parallel, with digital information from tape or card readers. Remotely programs to control six to eight information bits. Internal rep rate is $2 \mu \mathrm{sec}-999 \mathrm{sec}$ in 8 ranges. Pulse delay of 0 to 999 sec . Pulse width at $50 \%$ amplitude points is $0.1 \mu \mathrm{sec}-999 \mathrm{sec}$. Pulse amplitude is 0.25 volt Rise and fall time $\leq 20 \mathrm{nsec}$.

SOLID-STATE PULSE GENERATORS


Model B-14 is a low cost, highly versatile, compact and portable general purpose pulse generator. It features repetition rate of 20 Hz to 2 MHz . Delay is 0 to $10,000 \mu \mathrm{sec}$. Amplitude is 15 v into 1,000 ohms, 8 v into 50 ohms. Pulse width of .06 to $10,000 \mu \mathrm{sec}$. Rise and fall time is less than 10 nanosec, fixed. Rechargeable battery pack available for completely portable operation

Model B-15 has the same fast rise and fall time, delay and pulse width as Model B-14. In addition, B-15 offers a repetition rate of 5 Hz to 5 MHz . Also, its amplitude is 10 v into 50 ohms. Both units are only $12^{\prime \prime}$ wide $\times 5^{\prime \prime}$ high $\times 11^{1 / 2^{\prime \prime}}$ deep. Recharge able battery pack available


Model B-16 all transistorized pulse generator offers a rep rate of $20 \mathrm{~Hz} \cdot 20 \mathrm{MHz}$. Variable rise and fall times of less than 5 nsec to greater than 200 nsec . Pulse width is $0.015 \cdot 10,000 \mu \mathrm{sec}$. Amplitude is 0 to 10 volts, peak. Single or pulse pair operation. Rack mount available.

## SOLID STATE DIGITAL TIME DELAY GENERATORS

These three time delay generators are designed with solid-state circuitry for reliability and main tenance free performance. Their high accuracy with very low delay jitter lets you calibrate synchroscope sweeps, produce accurately spaced pulses for bio logical investigations, measure waveform timing measure pulse width, use with pulse generator for more accurate delay, etc
All three models below have these specifications: Delay range of 0.0 to $999,999.9 \mu \mathrm{sec}$ in increments of 100 nsec. Delay accuracy of $\pm(0.001 \%$ of set delay +2 nsec.) Delay jitter less than 1 nsec.


Model A10 provides 3 delayed pulses. Also offers amplitude of 10 volts, peak, min., into $>50$ ohms Approx. 15 nanosec rise time. Approx. 50 nsec width. Instrument is $8^{3 / 4} 4^{\prime \prime}$ high $\times 19^{\prime \prime}$ wide $\times 12^{\prime \prime}$ deep.


Model A11
offers single delayed pulse with same basic delayed pulse specs as A10 except amplitude is 6 volts, peak, min., into $>50$ ohms. And rise time is approx 10 nsec . Unit is half-rack size ( $5^{1 / 4^{\prime \prime}}$ high $\times 9^{1 / 22^{\prime \prime}}$ wide $\times 14^{1 / 2^{\prime \prime}}$ deep). Rack mounting unit is available.


Model A12 produces three delayed pulses, and has same basic delayed pulse specs as A10 except amplitude is 70 volts, peak, min., into $>50$ ohms Width is $3 \mu \mathrm{sec} \mathrm{min}$. Rise time is approx. $0.1 \mu \mathrm{sec}$ Repetitive and manual reset operation. Manual offers fail-safe triggering to protect against loss of information.


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## Pulse generators $60 \mathrm{~Hz}-5 \mathrm{MHz}$

For information on how to use these tables, turn to page 2

|  |  |  | FREQ | UENCY |  | MAIN | PULSE |  |  | OUTPU |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Manufacturer | Model | Min. Hz | Max. <br> MHz | Width Min. $\mu \mathrm{S}$ | Width Max. ms | Rise <br> ns | Fall ns | Min. Volts | Max. <br> -Volts | Imp. ohms | Type | Price \$ | Notes |
| $\begin{gathered} \text { PG- } \\ 1 \end{gathered}$ | Huggins S-K GASL Tektronix Weinschel | 961D 503A $2303-C$ 109 PG-1A | 50 50 10 275 20 | 60 Hz 120 Hz 260 Hz 700 Hz .002 | .002 .0006 ina .0005 1 | 20 ns 100 ns ina 300 ns .005 | 0.5 0.5 0.3 0.25 ina | 0.5 ina ina 0.3 ina | 0 ina 0 0 0 | 2000 ina $\pm 100$ 50 -1000 | 51 50 5 50 50 | C C C C R | $\begin{array}{r} 900 \\ 495 \\ 485 \\ 360 \\ 1250 \end{array}$ | c d c,d d |
|  | Ka | 5070-B | 50 | . 005 | 0.1 | 0.1 | 10 | 10 | 0.5 | 0.5 | 50 | R | 875 | e |
|  | $\mathrm{H}-\mathrm{P}$ | 212A | 50 | . 005 | . 07 | . 01 | 20 | 20 | 0 | $\pm 50$ | 50 | C, R | 600 |  |
|  | Servo | 9350 | 0.2 | . 005 | 100 | 1000 | 5 | 5 | $\pm 7$ | $\pm 10$ | 93 | $C, R$ | 660 | $a, b, e$ |
|  | Digital Elect | 1554 | . 05 | . 005 | 80 | 13 sec | 1000 | $1-15 \mu \mathrm{~s}$ | 5 | 15 | 150 | C | 130 |  |
|  | Chesapeake | U-100 | 50 | . 007 | 1 | . 006 | 500 | ina | ina | ina | 100 | C | 795 |  |
| $\begin{gathered} \text { PG- } \\ 2 \end{gathered}$ | Polarad | MP-1A | 10 | $.01{ }^{6}$ | 0.2 | . 002 | 10 | ina | 15 | 15 | 100 | C | 2575 | c |
|  | Ensco | PG214 | 10 | . 01 | 1 | 1 | 100 | 200 | 0 | 50 | 200 | C | 1075 | b |
|  | Ensco | PG114 | 10 | . 01 | 1 | 1 | 100 | 200 | 0 | 50 | 200 | C | 375 |  |
|  | Alfred | 5-6826P | 10 | . 01 | 1 | . 012 | 500 | 500 | 300 | 450 | ina | R | 490 |  |
|  | Tektronix | 160A/162 | 0 | . 01 | 100 | 10 sec | 1000 | ina | 50 | 50 | 1000 | R | 320 |  |
|  | H-P | 218AR/219A | 0 | . 01 | ina | ina |  | ina | 50 | 50 | 50 | R | 2125 | b |
|  | AEL | $155$ | 0.1 | . 01 | 10 | 1000 | 3000 | 3 | . 01 | 250 | ina | C | 675 |  |
|  | H-P | 218AR/219B | 0 | . 01 | 0.2 | . 005 | 60 | ina | 0 | 50 | 50 | R | 2490 | b |
|  |  | 218AR/219C | 0 | . 01 | 1 | 10 | 30 | $30$ | 0 | $\pm 15, \pm 90$ | 90,500 | R | 2375 | a |
|  | Berkeley | RP-2 | 60 | . 05 | ina | ina | note 10 |  | ina | ina | ina | C | 890 |  |
| $\begin{gathered} \text { PG- } \\ 3 \end{gathered}$ | Berkeley | RP-1 | 1 | . 05 | ina | ina | 50-500 | 2-100 $\mu \mathrm{s}$ | 0.1 | 2.2 | 100 | C | 960 |  |
|  | Tektronix | 160A/161 | 0 | . 05 | 10 | 100 | 500 | ina | 0 | $\pm 5$ | 1800 | R | 320 |  |
|  | Measurements | 179 | 60 | 0.1 | 0.5 | . 06 | 100 | 150 | -150 | $\pm 200$ | 250,1000 | C | 365 | d |
|  | Texas Inst | 6710 | 30 | 0.1 | 0.1 | . 001 | 0.35 | 30 | $\pm 8$ | $\pm 12$ | 50 | C | 1500 | a,e |
|  | Tektronix | R293 | 10,000 | 0.1 | . 002 | $0.25 \mu \mathrm{~s}$ | 1 | 1 | 6 | 12 | ina | R | 1000 | d |
|  | E-H | 131 | 10 | 0.1 | 0.1 | 0.5 | 10 | 10 | 50 | 50 | 50 | R | 575 | c |
|  | GASL | 2305-C | 10 | 0.1 | . 002 | $0.2 \mu \mathrm{~s}$ | 1 | 1 | 0 | $\pm 20$ | 50 | C | 595 |  |
|  | Servo | 2140A | 10 | 0.1 | 0.1 | 1 | 20 | 40 | 0 | $\pm 80$ | 93 | C | 1195 | $b, d, f, h$ |
|  | Servo | 2120A | 10 | 0.1 | 0.1 | 1 | 20 | 40 | 0 | $\pm 80$ | 93 | C | 895 | d,f,h |
|  | Velonex | 570 | 3 | 0.1 | 0.3 | 0.2 | 50 | 70 | 0 | -2000 | 200 | C | 5390 |  |
| $\begin{gathered} \text { PG- } \\ 4 \end{gathered}$ | Velonex | 350 | 3 | 0.1 | 0.1 | 0.2 | 50 | 70 | 0 | -2000 | 200 | C. | 3990 |  |
|  | Tektronix | 111 | 0 | 0.1 | . 002 | . 0015 | 500 | 1 | 5 | 5 | 50 | C | 365 | d |
|  | H-P | 1105A/1106A | 0 | 0.1 | 3 | ina | . 02 | ina | 0.2 | ina | 50 | C | 750 |  |
|  | H-P | 213B | 0 | 0.1 | 2 | . 002 | 0.1 | ina | 0.35 | 0.35 | 50 | C | 215 |  |
|  | Fairchild | 404-B | 10 | 0.25 | . 05 | 0.105 | 15 | 15 | -60 | $+60$ | 50 | $C, R$ | 760 | d |
|  | Datapulse | 100 | 5 | 0.5 | 0.1 | 100 | 30 | 40 | 1 | 150 | 50 | C,R | 345 |  |
|  | Digital Elect | 521 | 5 | 0.5 | 0.8 | 120 | 50-100 | 100 | 0 | 15 | 150 | C | 95 | c,d,e |
|  | Wang | 5SP | 0.5 | 0.5 | 0.5 | 500 | ina | ina | 0 | -12 | ina | C | 150 |  |
|  | Tektronix | 160A/163 | 0 | 0.5 | 1 | 10 | 200 | 200-500 | 0 | 25 | 500 | R | 320 |  |
|  | Digital Elect | 522 | 0 | 0.5 | 0.5 | 1 sec | 200 | 200 | 0 | 15 | 100 | C | 98 | c,d,e |
| $\begin{gathered} \text { PG- } \\ 5 \end{gathered}$ | Texas Inst | 6701 | 100 | 1 | . 005 | $0.1 \mu \mathrm{~s}$ | 1 | 1 | $\pm 2$ | $\pm 50$ | 50 |  |  | d,e |
|  | H-P | 215A | 100 | 1 | 0 | $0.1 \mu \mathrm{~s}$ | 1 | 1 | -10 | +10 | 50 | $C, R$ | 1875 |  |
|  | H-P | 214A | 10 | 1 | . 05 | 10 | 13 | 13 | 0.2 | 100 | 50 | C,R | 875 |  |
|  | E-H | 125 | 10 | 1 | . 001 | 0.1 | 0.2 | 0.5 | -10 | -10 | 50 | $C, R$ | 2275 | c |
|  | Berkeley | PB-2 | 1 | 1 | 0.3 | 0.1 | . $05-2 \mu \mathrm{~s}$ | .06-32 $\mu \mathrm{s}$ | . 001 | 10.1 | 100 | C | 790 |  |
|  | GASL | PSG-1 | 1 | 1 | 0.1 | $0.3 \mu \mathrm{~s}$ | 100 | 100 | 0.2 | 50 | 50 | C | 745 |  |
|  | Datapulse | 103M/P906 | 0 | 1 | . 002 | $0.2 \mu \mathrm{~s}$ | 1 | 1 | $\pm 3$ | $\pm 3$ | 50 | C,R | 1860 |  |
|  | Gen Radio | 1395A | 2.5 | 1.2 | 0.1 | 1 sec | note 1 | note 1 | 0 | $\pm 20$ | 1000 | C,R | 1992 |  |
|  | Gen Radio | 1398A | 2.5 | 1.2 | 0.1 | 1.1 sec | 5 | 5 | -60 | +60 | 1000 | C,R | 535 |  |
|  | Servo | 9450 | 100 | 2 | 100 | 1 | 5 | 5 | $\pm 7$ | $\pm 10$ | 93 | C, R | 835 | $a, b, e$ |
| PG-6 | Rutherford | B-7B | 20 | 2 | . 05 | 10 | 15 | 15 | 0 | $\pm 50$ | 50 | C,R | 720 | d |
|  | Rutherford | B-7D | 20 | 2 | . 05 | 10 | 15 | 15 | 0 | $\pm 50$ | 50 | C,R | 1200 | a |
|  | Rutherford | B-14 | 20 | 2 | . 06 | 10 | 10 | 10 | 0 | 15 | 10-1000 | C,R | 385 | d,e,g |
|  | Rutherford | B-7F | 2 | 2 | . 05 | 10 | 15 | 15 | 0 | 50 | 50 | $C, R$ | 920 |  |
|  | Tektronix | 114 | 0 | 2 | 0.1 | 1 | 10 | 10 | -1 | +10 | 50 | C | 350 | d |
|  | Gen Radio | 1217C/1201B | 0 | 2.4 | 0.1 | 1 sec | 15 | 15 | -40 | +40 | 1000 | C | 370 |  |
|  | Datapulse | 102 | 2 | 3 | . 05 | . $01 \mu \mathrm{~s}$ | .10-500 | 10 | 0 | $\pm 50$ | 50 | $C, R$ | 720 | c,d |
|  | E-H | 132A | 5 | 3.5 | 0.1 | . $01 \mu \mathrm{~s}$ | 12-100 | ina | -50 | +50 | $50$ | R | 715 |  |
|  | E-H | $130$ | 10 | 4 | 0.1 | . $05 \mu \mathrm{~s}$ | $10$ | ina | 0 | $\pm 50$ | 50-200 | R | 1175 | d |
|  | E-H | 133A | 1 | 5 | 0.5 | 0.3 | . $01-10 \mu \mathrm{~s}$ | . $02-10 \mu \mathrm{~s}$ | $\pm 0.2$ | $\pm 50$ | 50 | $C, R$ | 2275 | c |

Notes, abbreviations and manufacturers' index at end of this section.

Pulse generators $5 \mathrm{MHz}-200 \mathrm{MHz}$

|  | Manufacturer | Model | FREQUENCY |  | MAIN PULSE |  |  |  | OUTPUT |  |  | Type | Price \$ | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. Hz . | Max. <br> MHz | Width Min. $\mu \mathrm{s}$ | Width Max. ms | Rise ns | $\begin{aligned} & \text { Fall } \\ & \mathrm{ns} \end{aligned}$ | Min. Volts | Max. <br> Volts | Imp. ohms |  |  |  |
| $\begin{gathered} \text { PG- } \\ 7 \end{gathered}$ | Datapulse <br> Rutherford <br> Datapulse <br> Datapulse <br> Datapulse <br> Radar Engr <br> Walkirt <br> E-H <br> E-H <br> Servo | $\begin{aligned} & 103 \mathrm{M} / \mathrm{P905} \\ & \mathrm{~B}-15 \\ & 103 \mathrm{M} / \mathrm{P901} \\ & 103 \mathrm{M} / \mathrm{P902} \\ & 103 \mathrm{M} / \mathrm{P} 903 \\ & 760 \\ & \text { SWG-101 } \\ & 138 \\ & 120 \mathrm{D} \\ & 9455 \end{aligned}$ | 5 <br> 5 <br> 5 <br> 5 <br> 5 $\begin{aligned} & 5 \mathrm{MHz} \\ & 3000 \\ & 300 \\ & 100 \\ & 100 \end{aligned}$ | $\begin{aligned} & 5 \\ & 5 \\ & 5 \\ & 5 \\ & 5 \\ & \\ & 6 \\ & 10 \\ & 10 \\ & 10 \\ & 10 \end{aligned}$ | .05 <br> .06 <br> .05 <br> 2 <br> .05 <br> 20 ms <br> ina <br> . 05 <br> . 01 <br> .025 | 0.5 <br> 10 <br> 2 <br> 50 <br> 2 <br> 20 <br> ina <br> 1 <br> $0.1 \mu \mathrm{~s}$ <br> .001 | $\begin{aligned} & 20 \\ & 10 \\ & 20-300 \\ & 100 \\ & 5 \\ & 8 \\ & 8 \\ & 20-200 \\ & 10 \\ & 0.85 \\ & 5 \end{aligned}$ | $\begin{aligned} & 1000 \\ & 10 \\ & 20-200 \\ & 100 \\ & 5 \\ & 8 \\ & 8 \\ & 20-200 \\ & 10 \\ & 1 \\ & 5 \end{aligned}$ | $\begin{array}{\|l\|} \hline 1 \\ 0 \\ -15 \\ \pm 1 \\ 2.5 \\ 0 \\ 0.5 \\ 7.5 \\ -2 \\ \pm 7 \end{array}$ | $\begin{aligned} & 30 \\ & 10 \\ & +13 \\ & \pm 15 \\ & 5 \\ & 2 \\ & 12 \\ & 12 \\ & 15 \\ & -20 \\ & \pm 10 \end{aligned}$ | 50 <br> 50 <br> 50 <br> 600 <br> 50 <br> 5 <br> note 7 <br> 50 <br> 50 <br> 93 | C,R <br> C,R <br> C,R <br> C,R <br> C,R <br> C <br> C <br> C,R <br> C,R <br> C,R | $\begin{array}{r} 1490 \\ 525 \\ 1450 \\ 1350 \\ 1150 \\ \\ 88 \\ 345 \\ 990 \\ 1375 \\ 975 \end{array}$ | d,e <br> b,d,e,g <br> d,e <br> d,e <br> d,e <br> $g$ <br> $a, b, e$ |
| $\begin{gathered} \text { PG- } \\ 8 \end{gathered}$ | E-H <br> Fairchild <br> Digital Elect <br> E-H <br> Datapulse <br> Datapulse <br> Datapulse $\mathrm{H}-\mathrm{P}$ <br> Monsanto Intercontinental | $\begin{aligned} & 120 \mathrm{E} \\ & 792 \mathrm{~A} \\ & 721 \\ & 121 \\ & 108 \\ & \\ & 101 \\ & 108 \mathrm{~L} \\ & 222 \mathrm{~A} \\ & 3000 \\ & \text { PG-1 } \end{aligned}$ | $\begin{aligned} & 100 \\ & 50 \\ & 50 \\ & 10 \\ & 10 \\ & 10 \\ & 10 \\ & 10 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & 10 \\ & 10 \\ & 10 \\ & 10 \\ & 10 \\ & 10 \\ & 10 \\ & 10 \\ & 10 \\ & 10 \end{aligned}$ | .01 <br> 50 <br> .04 <br> .01 <br> . 02 <br> .03 <br> .03 <br> .03 <br> 1 <br> .03 | $\begin{aligned} & 0.1 \mu \mathrm{~s} \\ & 500 \\ & 50 \\ & 0.25 \\ & 5 \\ & 10 \\ & .005 \mu \mathrm{~s} \\ & 5 \\ & 100 \\ & 200 \end{aligned}$ | 0.85 <br> 8 <br> 20 <br> 10 <br> 7 <br> 5 <br> 12 <br> 4 <br> note 8 <br> 10 | $\begin{aligned} & 1 \\ & 8 \\ & 8 \\ & 20 \\ & 10 \\ & 7 \\ & 7 \\ & 7 \\ & 12.5 \mu \mathrm{~s} \\ & 4 \\ & \text { note } 8 \\ & 10 \end{aligned}$ | $\begin{aligned} & -.07 \\ & 0 \\ & 0 \\ & 10 \\ & 0.2 \\ & \\ & 0.5 \\ & 0.2 \\ & .05 \\ & 0.5 \\ & \pm 15 \end{aligned}$ | $\begin{aligned} & -20 \\ & 10 \\ & 10 \\ & 74 \\ & 50 \\ & \\ & 10 \\ & 50 \\ & 10 \\ & 10 \\ & \pm 15 \end{aligned}$ | 50 <br> 50 <br> 150 <br> 50 <br> 50 <br> 50 <br> 50 <br> 50 <br> 50 <br> 50 | $\begin{aligned} & C, R \\ & C, R \\ & C \\ & R \\ & C, R \\ & C, R \\ & C, R \\ & C, R \\ & C, R \\ & C, R \end{aligned}$ | $\begin{array}{r} 1675 \\ 520 \\ 220 \\ 1675 \\ 1480 \\ \\ 345 \\ 1980 \\ 690 \\ \text { request } \\ 585 \end{array}$ | d,e <br> c,d,e <br> d <br> d,e <br> $a, b, c, e, f$ <br> $b, c, d, e$ <br> d,e |
| $\begin{gathered} \text { PG- } \\ 9 \end{gathered}$ | Intercontinental <br> Tektronix <br> Datapulse <br> Texas Inst <br> Intercontinental <br> GASL <br> E-H <br> Rutherford Electro Design Intercontinental | $\begin{aligned} & \text { PU-2 } \\ & \text { R116 } \\ & 106 A \\ & 6613 \\ & \text { PG-2 } \\ & \\ & \text { PG-10 } \\ & 123-A \\ & \text { B-16 } \\ & \text { PG-20 } \\ & \text { PG-32 } \end{aligned}$ | $\begin{aligned} & \hline 0 \\ & 0 \\ & 10 \\ & 15 \\ & 1 \\ & 1 \mathrm{MHz} \\ & 1000 \\ & 20 \\ & 10 \\ & 0.1 \end{aligned}$ | $\begin{aligned} & 10 \\ & 10 \\ & 12 \\ & 15 \\ & 16 \\ & 20 \\ & 20 \\ & 20 \\ & 20 \\ & 20 \end{aligned}$ | $\begin{aligned} & .03 \\ & .05 \\ & .025 \\ & .03 \\ & .03 \\ & \\ & .02 \\ & .02 \\ & 0.15 \\ & .03 \\ & .03 \end{aligned}$ | $\begin{aligned} & 200 \\ & 0.55 \\ & 5 \\ & .03 \mu \mathrm{~s} \\ & 200 \\ & \\ & 0.3 \mathrm{~ns} \\ & 10 \\ & 10 \\ & 10 \\ & 1000 \end{aligned}$ | 10 note 5 $10 \mathrm{~ns}-1 \mathrm{~ms}$ note 2 note 11 5 5 7 $5-200$ 5 $10 \mathrm{~ns}-1 \mathrm{~s}$ | 10 <br> note 5 <br> $10 \mathrm{~ns}-1 \mathrm{~ms}$ <br> note 2 <br> note 11 $\left\|\begin{array}{l} 5 \\ 7 \\ 5-200 \\ 5 \\ 10 n s-1 s \end{array}\right\|$ | $\pm 15$ 0.4 .01 0 0 note 9 0 0 0 $\pm .01$ | $\pm 15$ <br> 10 <br> $\pm 12$ <br> 10 <br> $\pm 20$ <br> note 9 <br> 50 <br> 10 <br> 20 <br> $\pm 20$ | 50 <br> 50 <br> 50 <br> 50 <br> 50 <br> ina <br> 50 <br> 50 <br> 50 <br> 50,500 | C, R <br> R <br> C,R <br> C <br> C, R <br> C <br> C <br> C, R <br> C <br> C,R | $\begin{array}{r} 425 \\ 1550 \\ 950 \\ 950 \\ 925 \\ 960 \\ 1775 \\ 875 \\ 775 \\ 1385 \end{array}$ | d,e <br> d <br> $a, b, c, e$ <br> $a, c, e$ <br> d <br> d <br> d <br> $a, b, c, d, e$ |
| $\begin{aligned} & \text { PG- } \\ & 10 \end{aligned}$ | Intercontinental <br> Intercontinental <br> Texas Inst <br> Texas Inst <br> Texas Inst <br> Servo <br> Datapulse <br> Datapulse <br> Datapulse <br> Texas Inst | $\begin{aligned} & \text { PG-31 } \\ & \text { PG-33 } \\ & 6601 \\ & 6605 \\ & 6303 \\ & \\ & 9550 \\ & 110 A \\ & 109 \\ & 111 \\ & 6650 \end{aligned}$ | 0.1 <br> 0.1 <br> 60 <br> 60 <br> 60 $\begin{aligned} & 2 \mathrm{MHz} \\ & 4 \\ & 4 \\ & 4 \\ & 10 \end{aligned}$ | 20 <br> 20 <br> 25 <br> 25 <br> 25 <br> 40 <br> 40 <br> 40 <br> 40 <br> 50 | $\begin{aligned} & .03 \\ & .03 \\ & .02 \\ & .03 \\ & .02 \\ & \\ & .025 \\ & .01 \\ & .01 \\ & .005 \\ & .01 \end{aligned}$ | $\begin{aligned} & 1000 \\ & 1000 \\ & .001 \\ & 10 \\ & .001 \\ & \\ & .001 \\ & 5 \\ & 50 \\ & 500 \\ & 10 \end{aligned}$ | 10 $5 \mathrm{~ns}-1$ sec 6 note 3 6 5 4.5 5 2 note 4 | 10 <br> $5 \mathrm{~ns}-1 \mathrm{sec}$ <br> 6 <br> note 3 <br> 6 <br> 5 <br> 6 <br> 5 <br> 2 <br> note 4 | $\begin{array}{\|l} \hline \pm .01 \\ \pm .01 \\ 0 \\ 0 \\ 0 \\ \pm 7 \\ .01 \\ 1 \\ 0.15 \\ .01 \end{array}$ | $\begin{aligned} & \pm 20 \\ & \pm 20 \\ & 5 \\ & 10 \\ & 5 \\ & \pm 10 \\ & 10 \\ & 10 \\ & 5 \\ & 10 \end{aligned}$ | $\begin{aligned} & 50,500 \\ & 50,500 \\ & 93 \\ & 50 \\ & 93 \\ & 93 \\ & 93 \\ & 50 \\ & 50 \\ & 50 \\ & 50 \end{aligned}$ | $\begin{aligned} & C, R \\ & C, R \\ & C \\ & C \\ & C \\ & C, R \\ & C, R \\ & C, R \\ & C, R \\ & R \end{aligned}$ | $\begin{array}{r} 1225 \\ 1350 \\ 1300 \\ 1450 \\ 2280 \\ \\ 1390 \\ 1250 \\ 690 \\ 1480 \\ 1000 \end{array}$ | $a, b, c, d, e$ <br> $a, b, c, d, e$ <br> b,e <br> a,c,e <br> $a, c, e$ <br> $a, b, e$ <br> $a, b, d, e$ <br> $a, b, d, e$ <br> $a, b, c, e$ <br> d,e |
| $\begin{gathered} \text { PG- } \\ 11 \end{gathered}$ | E-H <br> Gen Radio <br> Texas Inst H-P <br> E-H | $\begin{aligned} & 139 \mathrm{~B} \\ & 1394 \mathrm{~A} \\ & 6901 \\ & 216 \mathrm{~A} \\ & 122 \end{aligned}$ | $\begin{aligned} & 10 \\ & 1 \mathrm{MHz} \\ & 1000 \\ & 0 \\ & 1000 \end{aligned}$ | $\begin{aligned} & 50 \\ & 100 \\ & 100 \\ & 100 \\ & 200 \end{aligned}$ | $\begin{aligned} & .01 \\ & .004 \\ & .002 \\ & .005 \\ & .002 \end{aligned}$ | 10 <br> 99 ns <br> 2 <br> 25 ns <br> 0.1 | $\begin{aligned} & 6 \mathrm{~ns}-3 \mathrm{~ms} \\ & 2 \\ & 1 \\ & 2.5 \\ & 1 \end{aligned}$ | $\begin{aligned} & 6 \mathrm{~ns}-3 \mathrm{~ms} \\ & 2 \\ & 1 \\ & 2.5 \\ & 1 \end{aligned}$ | $\begin{aligned} & \pm .03 \\ & 0 \\ & .005 \\ & 0.4 \\ & \pm 0.15 \end{aligned}$ | $\begin{aligned} & \pm 10 \\ & \pm 4 \\ & 5 \\ & 10 \\ & \pm 5 \end{aligned}$ | $\begin{aligned} & 50 \\ & 50 \\ & 50 \\ & 50 \\ & 50 \end{aligned}$ | $\begin{aligned} & C, R \\ & C, R \\ & R \\ & C, R \\ & C, R \end{aligned}$ | $\begin{array}{r} 1275 \\ 995 \\ 1800 \\ 1775 \\ 2875 \end{array}$ |  |

## Pulse generators Late arrivals

| PG- <br> 12 | Adar | SQ-260 | 1000 | 10 | .05 | .01 | ina | ina | 0 | $\pm 7$ | 51 | $C, R$ | 5600 |  |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

Notes, abbreviations and manufacturers' index at end of this section.


Compare this new Model SQ-260 Multiple Pulse Generator with any other and you'll see that it provides the most for the least cost! Featuring all solid-state integrated logic, the Model SQ-260 also offers: 10 megacycle stepping rate, 12 output channels, 16 time steps, convenient plugboard programming, program repeat capability, step-andrepeat capability, 51 ohm output impedance (change resistor to alter impedance), 12 variable output pulse durations, and 12 variable pulse start delays! All this and more for $\$ 5600$. Call or write for descriptive literature today!

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- bridging or non-bridging wipers
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PULSE GENERATORS

NOTES:
a. Both polarities available simultaneously from separate connectors.
b. This unit is a double-pulse generator. These pulses have the same over-all specifications.
c. Rise and Fall time taken between $10 \%$ and $90 \%$ points.
d. Either polarity available by means of a switch.
e. Solid state.
f. One or more extra sync pulses are available which occur after the first sync pulse in time.
. Battery operated.
h. Has extra sync pulse available coincident with leading edge of main pulse.

1. Rise and Fall time variable $100 \mathrm{~ns}-10 \mathrm{~ms}$
2. Rise and Fall time variable $10 \mathrm{~ns}-10 \mathrm{~ms}$
. Rise and Fall time variable $10 \mathrm{~ns}-3 \mu \mathrm{~s}$.
3. Rise and Fall time variable $5 \mathrm{~ns}-5 \mathrm{~ms}$.
4. Rise and Fall time variable $10 \mathrm{~ns}-110 \mu$ s.
5. Five independent pulse channels.
6. The output may be terminated in 43,50 or 600 ohms.
7. Rise and Fall time variable $100 \mathrm{~ns}-10 \mathrm{~ms}$.
8. +20 V or -36 V at low duty cycle; +15 V or -24 V at high duty cycle.
9. Rise time variable $.05-5 \mu$; Fall time variable $2-100 \mu \mathrm{~s}$.
10. Rise and Fall time variable $.01-200 \mu$.

## ABBREVIATIONS

Cabinet.
R Rackmount.
ina Information not available.

# Index of Manufacturers and Model Numbers 

(keyed to table locator symbols)

| Adar Associates | RP-2 | (PG-2) |
| :---: | :---: | :---: |
| SQ-260 (PG-12) | Chesapeake Instrument Corp. |  |
| Alfred Electronics | U-100 | (PG-1) |
| 5-6826P (PG-2) | Datapulse, Inc |  |
| American Electronic Laboratories, Inc (AEL) | 100 | (PG-4) |
|  | 101 | (PG-8) |
|  | 102 | (PG-6) |
| 155 (PG-2) | 103M/P901 | (PG-7) |
|  | 103M/P902 | (PG-7) |
| Berkeley Nucleonics | 103M/P903 | (PG-7) |
|  | 103M/P905 | (PG-7) |
| PB-2 (PG-5) | 103M/P906 | (PG-5) |
| RP-1 (PG-3) | 106A | (PG-9) |


| 108 | $(P G-8)$ |
| :--- | :--- |
| 108 L | $(P G-8)$ |
| 109 | $(P G-10)$ |
| 110 A | $(P G-10)$ |
| 111 | $(P G-10)$ |

Digital Electronics (Digital Elect)

| 521 | $(P G-4)$ |
| :--- | :--- |
| 522 | $(P G-4)$ |
| 721 | $(P G-8)$ |
| 1554 | $(P G-1)$ |

E-H Research Laboratories, Inc

| 120 D | (PG-7) |
| :--- | :--- |
| 120 E | (PG-8) |
| 121 | (PG-8) |
| 122 | (PG-11) |
| $123-\mathrm{A}$ | (PG-9) |
| 125 | (PG-5) |
| 130 | (PG-6) |
| 131 | (PG-3) |
| 132 A | (PG-6) |
| 133 A | (PG-6) |
| 138 | $(\mathrm{PG}-7$ |
| 1398 | $(\mathrm{PG}-11)$ |

Electro Design, Inc

| PG-20 | (PG-9) |
| :--- | ---: |
| ENSCO, Inc |  |
| PG114 | (PG-2) |
| PG214 | (PG-2) |
| Fairchild Instrumentation |  |
| 404-B | (PG-4) |
| 792A | (PG-8) |

General Applied Science Laboratories (GASL)

| $2303-C$ | $(P G-1)$ |
| :--- | :--- |
| $2305-C$ | $(P G-3)$ |
| PG-10 | (PG-9) |
| PSG-1 | (PG-5) |

General Radio Co (Gen Radio)

| $1217 \mathrm{C} / 1201 \mathrm{~B}$ | $($ PG-6) |
| :--- | :--- |
| 1394 A | $($ PG-11) |
| 1395 A | $($ PG-5 |
| 1398 A | (PG-5) |

Hewlett-Packard Co (H-P)


Manufacturers' addresses and literature offerings in master cross index at front of issue.

Kay Electric Co
5070-B (PG-1)
Measurements
179 (PG-3)

Monsanto
3000 (PG-8)
Polarad Electronic Instruments

MP-1A (PG-2)
Radar Engineers (Radar Engr)
760
(PG-7)
Rutherford Electronics Co

| B-7B | (PG-6) |
| :--- | :--- |
| B-7D | (PG-6) |
| B-7F | (PG-6) |
| B-14 | (PG-6) |
| B-15 | (PG-7) |
| B-16 | (PG-9) |

Servo Corp of America

| 2120A | (PG-3) |
| :--- | :--- |
| $2140 A$ | (PG-3) |
| 9350 | (PG-1) |
| 9450 | (PG-5) |
| 9455 | (PG-7) |
| 9550 | (PG-10) |

Spencer-Kennedy Labs, Inc (S-K)
503A (PG-1)
Tektronix, Inc

| 109 | $(P G-1)$ |
| :--- | :---: |
| 111 | $(P G-4)$ |
| 114 | $(P G-6)$ |
| $160 A / 161$ | $(P G-3)$ |
| $160 A / 162$ | $(P G-2)$ |
| $160 A / 163$ | $(P G-4)$ |
| R116 | $(P G-9)$ |
| R293 | $(P G-3)$ |

Texas Instruments, Inc (Texas Inst)

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# What's missing in generator specs? <br> Here are seven secondary parameters to consider and some pitfalls to avoid when buying. 

Until the day when all manufacturers agree on one method of specifying signal generators, the prospective buyer will find it difficult to compare competitive models on a point-by-point basis. He will find it especially frustrating when he looks for complete specifications on secondary parameters, such as harmonic content and stability, which are often either hedged or omitted entirely. Here are some of the more important of these secondary parameters that he should bear in mind.

- Output level—an apparently straightforward parameter-must be interpreted carefully. Is the specified level into an open circuit or a load? The user must know this or he cannot be sure of output level. Some signal generators are calibrated in microvolts across a standard termination, some in open-circuit microvolts. Mistaking one for the other can easily lead to a 2 -to-1 error in interpreting the output level indication. It should be obvious that a properly matched load cannot be provided unless the value to match it to is known.
- Harmonics in the output of the signal generator can be especially troublesome when the signal generator is being used to measure a receiver's ability to reject signals outside its pass band. If the rejection ratio to be measured is on the order of 60 to 100 dB and harmonics are lurking only 30 or 40 dB down in the pass band, the measurement will yield inaccurate results.
- Stability statements are often missing and, when they are given, often misleading. Optimum conditions (a constant level, constant frequency, constant load, etc.) may be assumed without a statement to that effect. Also, the phrase "after warm-up" (as in "drift after warm-up") in a stability or drift specification is useless, unless it is accompanied by the warm-up period. Similarly, the terms "short-term stability" and "long-term stability" are meaningless without further qualification; there are no standard definitions of "short term" and "long term."
- Retuning drift-a rarely stated specification

[^2]-is the generator's stability when the bandswitch is rotated to another range and returned. The chief problem here is that, when a tank coil is switched into a circuit and starts passing current, it warms up. Switch it out of the circuit and it cools off. Thus, although the instrument might have completed its specified warm-up period, bandswitching initiates a new coil thermal cycle.

- Load changes on frequency and on waveform, which are often characterized by pulling and distortion, respectively, are among the most neglected specifications. Distortion, which can be produced by a number of causes, is especially critical when tests are being conducted on highfidelity audio equipment.
- RF shielding effectiveness is important. The signal generator should deliver its output through the output connector only. RF escaping through other routes can lead to considerable error in sensitivity measurements, and the leakage specification should therefore be noted carefully.
- Meter indications are often assumed to offer the accuracy that the specification states. But there is usually more to be said, including, for example, the frequency characteristic. Also, the percent-modulation meter may be specified as accurate to " $\pm 10 \%$ ", but, unless it is known whether this is $10 \%$ of full scale or of indicated value, meter accuracy still cannot be assessed.

Incidental FM or AM, modulation envelope symmetry, modulation distortion at various modu-


Comparing competitive units point-by-point is difficult. Considering secondary parameters removes the blindfold.
lation levels, intermodulation in the output meter rectifier, the frequency characteristic of modula-tion-these specifications and many others must be given if the capability of a signal generator is to be known completely. But the coin has another side-one that explains why the completely specified generator will never be made.

## Full specification too costly

Specifications cost money. Checking each instrument for the effects of line voltage, temperature, retuning, waveform, etc. could easily add several hundred dollars to the price. No one could afford a completely specified instrument. The manufacturer has to decide how much specification his customers are willing to pay for and proceed accordingly. Thus, from a particular customer's point of view, an instrument may be overspecified or underspecified.

Overspecification is also the fault of the customer who buys more performance than he needs. Many signal generator buyers are probably guilty of overspecification, particularly of output level. A single instrument that tries to be all things to all men is rarely the most economical approach to signal generators, largely because certain features can be bought only at the expense of others. A high power level, for example, works against a generator's stability and leakage characteristics.

Specifying a signal generator may someday be simple and straightforward. The IEEE's Instrumentation and Measurement Group's Technical Committee on High-Frequency Instrumentation and Measurements has a subcommittee working on the problem, and some standards on specifications are sure to result. Meanwhile, as with any product, the best way to ensure that a signal generator is honestly specified is to deal with a reputable manufacturer. You may then be confident that the specifications that are given are accurate. If you need specifications that are not given, a letter to the manufacturer should ordinarily bring information on typical performance to be expected.


Spec sheets are often incomplete. A letter to the manufacturer should turn up the missing specifications.

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# Look beyond the listed specs of microwave signal generators to find out about their modulation performance, compatibility and versatility. 

A number of factors other than the specifications should be borne in mind whenever you are selecting a microwave signal instrument. The listed specifications are easy-to-measure, welldefined parameters that may tell precious little about the instrument. Often more important than these are two groups of characteristics that are difficult, even impossible, to measure precisely:

- Signal impurities.
- Unmeasurable characteristics.

Signal impurities. Their measurement is possible, but they are so interrelated with other parameters, so hedged about with qualifications, or so dependent on the mode or range of operation, that no simple numerical statement can be made about them. Hence they are seldom published, though the manufacturer is usually able (or should be able) to produce useful data about them.

Unmeasurable characteristics. They are either qualitive considerations like convenience or flexibility, or properties that cannot be measured because no yardstick exists, such as durability.

## Certain parameters are usually specified

Altogether there are about 22 criteria that must or should be taken into account when selecting microwave signal instruments. We shall divide them into three groups: usually published parameters, frequently unspecified parameters, and unmeasurable parameters. First, a list of the parameters that are handed to the engineer:

Frequency range-It is the basic specification, arbitrarily determined by the manufacturer. Even though the instrument may perform well beyond the limits of this range, the manufacturer is prepared to guarantee his other specifications only within these specified limits.
Frequency accuracy-It includes all the factors that contribute to the maximum observable difference between any dial setting within the specified frequency range and the actual, absolute value of the output frequency (referred to NBS

[^3]standards) after stabilization and under standard conditions of ambient temperature, line-voltage level modulation setting. Frequently used standard conditions are 115 volts, 60 Hz unmodulated (cw) line voltage, and 0.0 dBm output.

Frequency stability vs time-When measured after 30 minutes warm-up under standard conditions, a typical figure for a quality instrument is $0.005 \%$ per hour, with a maximum drift that keeps the unit within the frequency-accuracy specification.

Frequency stability vs temperature-It is usually specified as a per-cent frequency change per ${ }^{\circ} \mathrm{C}$ over a specified temperature range. Typical values for a commercial instrument are $0.0005 \% /{ }^{\circ} \mathrm{C}$ from $0^{\circ}$ to $50^{\circ} \mathrm{C}$.

Frequency stability vs line voltage-It is usually specified as a per-cent frequency change per one-volt change. A typical microwave signal generator is rated at $0.0003 \%$ per one-volt change over a range of $\pm 10 \%$ of nominal line voltage.

Accuracy of power-level setting (full scale)—It must include only the energy at the fundamental frequency and exclude harmonics or spurious energy. The result is comparable to absolute NBS standards. The measurement must be performed on an unmodulated signal. The operating conditions should include the lowest-rated line voltage and the highest-rated ambient temperature.

Accuracy of power attenuation-It describes the linearity of the attenuator, i.e., its maximum contribution to the error under the worst combination of setting, frequency and ambient temperature, and with the operating conditions described.

## How to check impurities of the output

The next group of parameters, those frequently unspecified, includes a variety of signal impurities and their effects on the modulation envelope. The cw output of a practical, commercial signal instrument is not ideal; it does not have the singlefrequency (coherent) waveform that is desirable. However, the degree of deviation from ideal purity in a particular design is rarely stated, except in some general form like "minimum inci-
dental AM and FM." The impurities can be measured, but their complex relationships and the fact that they are not uniformly present over the entire rated frequency range make statements of their measurement complex and difficult.

To cope with these difficulties, a conscientious manufacturer, though he may not publish ratings, maintains "design limits," which should be available to assist the engineer in evaluating the instrument. Here is a list of causes of signal impurities and suggested tolerances:

Hum modulation, AM and FM-Inadequate filtering of the power supplies feeding the oscillator is the prime cause, although magnetic pickup and even electrostatic ac coupling can be significant. In a typical X-band design, the internal design limit might read: "Maximum incidental FM shall not exceed 20 kHz p-p due to power supply ripple and coupling. Maximum AM shall not exceed $0.01 \%$ measured under cw conditions."

Noise modulation, AM and FM-This is due primarily to noise generated in the microwave oscillator tube or transistor; more specifically, beam noise in klystron or other velocity-type tube is the culprit. A typical design-limit statement might read: "Maximum integrated noise sideband power shall not exceed -60 dB referred to the unmodulated carrier."

Harmonic Content-Invariably generated by the oscillator, this is never completely attenuated by the $Q$ of the cavity, high though that may be. A typical design limit may be stated as: "Total harmonic content shall not exceed -40 dBm ."

Flicker-Several sources contribute to this: line transients and spikes, imperfect joints (e.g., sliding contacts) in RF plumbing, and erratic "pulling" (or intermittent "moding") in a marginal oscillator circuit. In a well-designed signal instrument, this should not be a measurable parameter. Typically, flicker modulation should not exceed -60 dB over more than $1 \%$ of operating time, or -50 dB over $0.01 \%$ of the time.

Modulation characteristics and anomalies are often as hard to determine from a written specification as are cw characteristics and behavior. The following points should not be overlooked:

Splatter-It results from an inadequate dynamic modulation range and should never be present when a device is operated under a specified range of modulation conditions. Attempts to operate an instrument at a higher than the specified modulation percentage may result in serious splatter.

Anomalous sidebands-Distortion in the modulation process can generate dozens of large, confusing, and sometimes intolerable spurious sidebands. In a good general-purpose design, the total energy of all such sidebands should not exceed $1 \%$ of the total sideband energy.
Spectral assymetry-This is usually due to
some combination of factors, including limited modulation range, high and nonlinear power supply impedance, marginal fidelity in the modulation circuit, and non-ideal modulating signals.

Any one of the above departures from absolute signal purity can cause expensive, time-wasting, and perhaps even destructive malfunctioning in a system. For example, large signal impurity can throw off level reading by several decibels, produce strange "detuning" effects and generate unrecognizable modulation envelopes. Only by assuring himself that the instrument designer has anticipated and minimized signal anomalies can the engineer avoid such problems.

Imperfections in the modulating signal are difficult to define with precision. However, it is necessary to check that each of the following has been standardized to acceptable limits:

Pulse-modulation fidelity of envelope-Typical design-limit specifications are: Rise and decay time shall not exceed $0.15 \mu \mathrm{~s}$. Neither overshoot nor undershoot should be more than $5 \%$. Flatness of pulse top should be $1 \%$ on narrow pulses, $5 \%$ on wide pulses.

Sawtooth modulation fidelity of envelope-Typical design-limit specifications are: RF output should track modulating waveform within $3 \%$ for all modulation levels between 10 and $90 \%$.

Sine-wave modulation fidelity of envelopeTypical design-limit specifications are: Modulation envelope distortion should not exceed 5\% total over a range of 0 to $50 \%$.

## Indefinable qualities can be quite definitive

Even though the instrument passes all the previous tests with flying colors, there are still some hurdles left. The last group of criteria are those unmeasurable qualities that make or break a line. These usually fall into two main categories: One we may call "functional reliability" or "design longevity," and the other, simply, "convenience and flexibility."

Functional reliability is a measure of the probability that an instrument, purchased today, will function in accordance with its specifications at a given time in the future. Failure to do so need not be catastrophic or even apparent. A manufacturer should be able to assure you, by showing life-test or field-experience data, that his instrument will,


Estimate design longevity of the instrument. The manufacturer should provide life-test or field experience data.


HOURS OF SERVICE (LOG. SCALE)

1. Typical cost factors associated with the operation of a signal generator are shown in terms of initial cost and routine maintenance expenses through the life of the instrument.

2. In a sound instrument, true functional failure, $F_{2}$, must occur later than the end of useful life. The functional failure analysis has been prepared for power output in this graph. $F_{1}$ represents a renewable point in the life of the instrument.


Pick your purchase from a modular family. Future compatibility and functional modularity are important.
in all probability, provide full, functional reliability for a period of years.

Note that "functional failure" exists whenever the instrument is capable of operating outside the specified limits, even if the user never actually happens to apply a combination of stresses that would force it beyond them.

Anomalous behavior is a kind of functional failure, even if it is within the specified limits. For instance, an instrument's level calibration error may manifest itself as a drift upward and then suddenly change to a downward drift. This uncharacteristic behavior may paralyze an experiment, or at least delay it while the reason for it is hunted down, even though the drift remains within the permitted range.

Renewability-A common shortcoming of inferior instruments is that they are based on marginal designs that have very narrow tolerances. When a component fails, the unit cannot always be repaired such that it will again perform according to all of its original specifications, even when factory-supplied standard parts are used. To guard against this type of design, the engineer should make sure that the manufacturer has observed adequate margins to guarantee renewability. A typical set of curves used by Polarad to establish design margins is shown in Fig. 1. The cost of maintaining an instrument is compared with the cost of replacement in Fig. 2.
Versatility-In how many different ways can it be used in addition to that for which it is originally purchased? How much of the time will it be in use? Will it be compatible with most associated equipment, and in how many combinations? These and similar questions become important when selecting an instrument for laboratory use on a specific project with the expectation that it will later be available for other work. The manufacturer should be able to show features that demonstrate the wide applicability of his instrument.

Functional modularity-Look beyond the specific instrument to the other members of its family. When a line of instruments is considered as an integrated set (of measuring facilities, for example), each unit by itself should be suited to a sizeable range of applications without wasteful duplication, overlap or compromise in performance. You have a right to ask: "Can the same doubler be driven by each of a family of generators? Will the modulator module drive every one of the sources and generators in the line?"

Future compatibility-When purchasing one or more designs in a line of instrument modules, engineers should ask: "Can we be sure that our future needs for this kind of instrumentation can be met by adding one or more compatible existing modules from the same family?" Once again, it is necessary to look beyond the specifications. - -

## another series of



618C Signal Generator


620B Signal Generator

# Improved 

## 3.8-7.6 GHz



## $\mathbf{7 - 1 1 ~ G H z}$

## Generators

Very low residual FM; cleaner signals mean more accurate measurement results
High level auxiliary rf output; can phase-lock or count frequency
New power monitor without "zero set"; simplified operation
High performance, lighter weight power supplies
These improved signal generators from HewlettPackard offer new standards of highly accurate and stable test signals. The new power supplies result in the lower residual FM ( $10 \mathrm{kHz} \mathrm{p}-\mathrm{p}$ max.) and decrease the weight of the instruments. The auxiliary rf output allows you to phase-lock the signal generators with the Dymec 2650A Oscillator Synchronizer to provide crystal oscillator stability at microwave frequencies. It also can be used with an electronic counter for utmost precision in monitoring frequency.

Ultra-fine tuning capability is assured with the addition of a $\Delta \mathrm{F}$ frequency vernier control. A new crystal detector type power monitor eliminates zero setting; operation is simplified with less chance for operator error.

Brief specs are listed here. Call your HewlettPackard field engineer for complete information or write Palo Alto, California 94304, Tel. (415) 326-7000; Europe: 54 Route des Acacias, Geneva.

## SPECIFICATIONS hp 618C, 620B Signal Generators

Frequency range: $\mathrm{hp} 618 \mathrm{C}, 3.8$ to $7.6 \mathrm{GHz} ; \mathrm{hp} 620 \mathrm{~B}, 7$ to 11 GHz
Frequency calibration: Direct reading, accuracy better than $\pm 1 \%$ Calibrated RF into $50 \Omega$
Output accuracy: Within $\pm 2 \mathrm{db}$ from -7 dbm to -127 dbm
Aux. RF output: Fixed level of at least 0.3 mw

Weight: Net $63 \mathrm{lbs}(29 \mathrm{~kg})$

Prices f.o.b. factory.

## HEWLETT

Frequency stability: $<0.006 \% /{ }^{\circ} \mathrm{C}$ change in ambient temp.; $<0.02 \%$ change for $\pm 10 \%$ line voltage variation
Residual FM: $\mathrm{hp} 618 \mathrm{C}, \leq 8 \mathrm{kHz} \mathrm{p}$-p; hp $620 \mathrm{~B}, \leq 10 \mathrm{kHz} \mathrm{p}$-p output range: 1 mw or 0.224 v to $0.1 \mu \mathrm{v}(0 \mathrm{dbm}$ to $-127 \mathrm{dbm})$

Modulation: Pulse, square wave, $F M$; internal or external

Price: hp 618C, hp 620B, $\$ 2250$; rack mount add $\$ 20$.
Data subject to change without notice.

## Signal generators $\quad 1.62-420 \mathrm{MHz}$

For information on how to use these tables, turn to page 2

|  | Manufacturer | Model | FREQUENCY |  |  |  | \# of ranges | OUTPUT |  | Modulation | Type | Price \$ | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. MHz | Max. <br> MHz | Acc. \% | Stab. ppm |  | Min. $\mu \mathrm{V}$ | Max. V |  |  |  |  |
| $\begin{gathered} \text { SG- } \\ 1 \end{gathered}$ | Sierra | 350A | . 005 | 1.62 | $\pm 2 \mathrm{kHz}$ | ina | 2 | -90 dBm | $+10 \mathrm{dBm}$ | ina | C | 895 |  |
|  | Tel-Inst | 1902A | 4.5 | 4.5 | ina | xtal | 1 | ina | 0.75 | AM,FM | C | 480 |  |
|  | H-P | 618C | 3.8 | 7.6 | 1 | 60 | 1 | 0.1 | 0.224 | AM,FM, Pulse | C,R | 2250 |  |
|  | H-P | 620B | 7 | 11 | 1 | 60 | 1 | 0.1 | 0.224 | AM,FM, Pulse | C, R | 2250 |  |
|  | Grundig | AS2 | 0.1 | 11.2 | ina | ina | 12 | $-130 \mathrm{~dB}$ | 0.5 | AM | C | 275 |  |
|  | Sierra | 351A | . 01 | 15 | $\pm 10 \mathrm{ppm}$ | ina | 1 | -90 dBm | 0 dBm | ina | C,R | 2950 |  |
|  | R \& S | SMLR | 0.1 | 30 | $\pm 1$ | 50 | 5 | 1 | 10 | AM,FM | C | 1490 |  |
|  | Measurements | 65B | . 075 | 30 | 0.5 | ina | 6 | 0.1 | 2.2 | AM | C | 875 |  |
|  | Heath | IG-42 | 0.1 | 31 | $\pm 3$ | ina | 5 | ina | 0.1 | AM | C | 56 kit |  |
|  | R \& S | SMAR | 29 Hz | 31 | $\pm 0.5$ | 30 | 6 | . 01 | 10 | AM,FM | C | 5995 |  |
| $\begin{gathered} \text { SG- } \\ 2 \end{gathered}$ | Clough-Brengle | 299A |  | 32 | 0.5 | ina | 5 | 0.5 | 0.1 |  |  |  |  |
|  | RCA | WR-50B | $.085$ | 40 | $\pm 2$ | ina | 6 | 50 mV | ina | AM | C | 65 |  |
|  | Measurements | 82 | . 08 | 50 | 1 | ina | 7 | 0.1 | 1 | AM | C | 660 |  |
|  | Gen Radio | 1001A | . 005 | 50 | $\pm 1$ | 2500 | 8 | 0.1 | 0.282 | AM | C | 1195 |  |
|  | $R$ \& S | SMDH | 0 | 50 | . 002 ppm | . 001 ppm | 2 | 0.1 | 2.5 | FM | $C, R$ | 11,600 |  |
|  | Measurements | 210 S | 24 | 52 | 0.5 | ina | 1 | 0.1 | 0.1 | FM | C | 475 |  |
|  | H-P | 606B | . 05 | 65 | 1 | 50 | 6 | 0.1 | 3 | AM,FM | $C, R$ | 1550 |  |
|  | Gertsch | SG-8 | . 05 | 65 | $\pm 1$ | . $005 \%$ | 6 | 0.1 | 3 | AM | R | 1345 | b |
|  | H-P | 606A | . 05 | 65 | 1 | 50 | 6 | 0.1 | 3 | AM,FM | C,R | 1350 | b |
|  | Marconi | 2002 | . 01 | 72 | $\pm 1$ | 10 | 8 | 0.1 | . 08 | AM | $C, R$ |  |  |
| $\begin{gathered} \text { SG- } \\ 3 \end{gathered}$ | Measurements | 210 R |  | 80 | 0.5 | ina |  | 0.1 |  | FM |  |  |  |
|  | AMI | 304 | 5 | 100 | $\pm 0.5$ | $\pm .005 \%$ | 1 | 0.1 | 0.1 | FM | $C, R$ | $1785$ | b |
|  | Piezo | SG-12A/U | 1.4 | 102 | 0.5 | ina | 14 | . 05 | 1 | FM | C | 2500 |  |
|  | EICO | 320 | 0.15 | 102 | ina | ina | 7 | ina | . 07 | AM | C | 30 |  |
|  | Measurements | 88 | 86 | 108 | 0.5 | ina | 1 | 0.1 | 0.1 | FM | C | 585 |  |
|  | Measurements | 210A | 86 | 108 | 0.5 | ina | 1 | 0.1 | 0.1 | FM | C | 450 |  |
|  | Heath | IG-102 | 100 | 110 | 2 | ina | 6 | ina | 0.1 | AM | C | 30 kit |  |
|  | EMC | 502 | 0.115 | 110 | $\pm 1.5$ | ina | 6 | ina | 0.1 | AM | C | 27 |  |
|  | Radiometer | MS111 | . 01 | 110 | 1.5 | 0.2\% | 12 | 0.2 | 0.2 | AM,FM | ${ }_{C}$ | $1008$ |  |
|  | Kay | 5070 | 10 | 120 | $\pm 1$ | ina | 5 | 107 dB | 3 | Pulse | $C, R$ |  |  |
| $\begin{gathered} \text { SG- } \\ 4 \end{gathered}$ | Aircraft Radio | H-14-A | 108 | 132 | . 005 | ina | 2 | 1 | 100 |  | C |  |  |
|  | H-P | 211 A | 88 | 140 | 0.1 | 50 | 1 | 0.1 | 0.2 | AM,FM | R | $2190$ |  |
|  | EICO | 315 | 75 | 150 | 1 | ina | 7 | ina | 0.1 | AM | C | 60 |  |
|  | Microdot | 440/167RF | 1 | 150 | . 0008 | .0005\% | 1 | 0.1 | 1 | AM, FM, Pulse | R | request |  |
|  | Measurements | 210B | 148 | 174 | 0.5 | ina | 1 | 0.1 | 0.1 | FM | C | 450 |  |
|  | Motorola | T-1036-A | 25 | 175 | 0.5 | ina | 6 | 0.1 | 0.1 | FM | C | 793 |  |
|  | Hickok | 295X | 0.125 | 175 | 1 | ina | 8 | 0.1 | 0.1 | AM | C,R | 655 |  |
|  | AMI | 302 | 20 | 200 | $\pm 0.5$ | $\pm .005 \%$ | 1 | 0.1 | 0.1 | FM | C,R | 1950 |  |
|  |  | 202H |  | 216 | $\pm 0.5$ | 100 | 2 | 0.1 | 0.2 | AM,FM,Pulse | C,R | $1475$ |  |
|  | Radiometer | MS26 |  | 216 | 0.5 | ina | 2 | . 05 | 0.2 | AM,FM | C |  |  |
| $\begin{gathered} \text { SG- } \\ 5 \end{gathered}$ | Marconi | 995A/2 | 1.5 | 220 | 1 | 25 | 5 | 1 | 0.1 | AM,FM | C | 1145 |  |
|  | Triplett | 3432A | 0.16 | 220 | 2 | ina | 8 | ina | ina | AM | C | 130 |  |
|  | Precise | 612 | 0.1 | 220 | 1 | ina | 6 | 20 | 0.1 | AM,FM | C | 80 |  |
|  | Radiometer | MS27 | 0.3 | 240 | 0.5 | ina | 5 | 0.2 | 0.2 | AM,FM | C | 1270 |  |
|  | Gen Radio | 1021-AV | 40 | 250 | 1 | ina | 2 | 0.5 | 1 | AM | C | 895 |  |
|  | RS | 1021 VHF |  | 260 | ina | $\pm .01 \%$ | 1 | 0.1 | . 07 |  | C |  | a |
|  | RS | 5036-3 | 2161 | 260 | ina | . $015 \%$ | 1 | 0.1 | 0.1 | FM | C,R | request |  |
|  | RS | 1003 | 216 | 260 | $\pm 0.5$ | . $015 \%$ | 1 | 0.1 | 0.1 | FM | C,R | 2925 |  |
|  | H-P | 202J | $195$ | 270 | $\pm 0.5$ | $200$ | 1 | 0.1 | 0.2 | AM,FM,Pulse | $C, R$ | $1595$ |  |
|  | Microdot | 440/140-4RF | 200 | 275 | . 0008 | .0006\% | 1 | 0.1 |  |  |  | request |  |
| $\begin{gathered} \text { SG- } \\ 6 \end{gathered}$ | $R$ \& S | ASV | 30 | 300 | $\pm 2$ | ina | 1 | 30 mV | 3 | AM,FM | C | 850 |  |
|  | $R$ \& S | SMLM | 30 | 300 | $\pm 1$ | 30 | 6 | 3 mV | 3 | AM,FM | C | 1395 |  |
|  | $R \& S$ | SMAF | 4 | 300 | $\pm 1$ | 50 | 8 | . 05 | 50 | AM,FM | C | 2995 |  |
|  | H-P | 232A | 329.3 | 335 | . 0065 | ina | 2 | 1 | 0.2 | AM | C | 1920 |  |
|  | Measurements | 95 | 50 | 400 | 0.5 | ina | 3 | 0.1 | 0.1 | FM | C | 1800 |  |
|  | EPSCO | SG-132A | 15 | 400 | 0.5 | 50 | 6 | 0.1 | 0.15 | AM,FM | C,R | 2400 |  |
|  | Measurements | 80 | 2 | 400 | 0.5 | ina | 6 | 0.1 | 0.1 | AM,Pulse | C | 590 |  |
|  | AMI | 303A | 215 | 420 | $\pm 0.5$ | $\pm .005 \%$ | 1 | 0.1 | 0.1 | FM | C,R | 1900 |  |
|  | H-P | 608D | 10 | 420 | 0.5 | 10 | 5 | 0.1 | 0.5 | AM,FM,Pulse | C,R | 1300 | b |
|  | Gertsch | SG-9 | 10 | 420 | $\pm 0.5$ | .005\% | 5 | 0.1 | 0.5 | AM | R | 1295 | b |

Notes, abbreviations and manufacturers' index at end of this section.

## Signal generators $435-7600 \mathrm{MHz}$

|  |  |  |  | FREQ | ENCY |  |  | OUT |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Manufacturer | Model | Min. MHz | Max. <br> MHz | Acc. \% | Stab. ppm | \# of ranges | Min. $\mu \mathrm{V}$ | Max. V | Modulation | Type | Price \$ | Notes |
| $\begin{gathered} \text { SG- } \\ 7 \end{gathered}$ | EICO | 324 | 0.15 | 435 | 1.5 | ina | 7 | ina | 0.1 | AM | C | 40 |  |
|  | H-P | 608F | 10 | 455 | 1 | 50 | 5 | 0.1 | 0.5 | AM,FM,Pulse | $C, R$ | 1600 |  |
|  | Marconi | 1064B/2 | 30 | 470 | 0.5 | 25 | 3 | 0.25 | . 01 | FM | C | 795 |  |
|  | Motorola | T1035-A | 25 | 470 | 0.5 | ina | 6 | 0.1 | 0.1 | FM | C | 793 |  |
|  | Measurements | M-673 | 25 | 470 | 0.5 | ina | 6 | 0.1 | 0.1 | FM | C | 698 |  |
|  | Marconi | 1066B/6 | 10 | 470 | $\pm 1$ | 0.15\% | 5 | 0.1 | 0.1 | AM,FM | C,R | 1895 |  |
|  | Marconi | 1066B/1 | 10 | 470 | 1 | 25 | 5 | 0.2 | 0.1 | AM,FM | C,R | 1650 |  |
|  | Marconi | $801 \mathrm{D} / 1$ | 10 | 470 | 0.2 | 50 | 5 | 0.1 | 0.5 | AM,FM,Pulse | C | 1615 |  |
|  | Measurements | 80R | 5 | 475 | 0.5 | ina | 6 | 0.1 | 0.1 | AM,Pulse | C | 625 |  |
|  | R \& S | SLSV | 25 | 480 | $\pm 1$ | 50 | 7 | ina | 3.5 | AM | C | 1695 |  |
| $\begin{gathered} \text { SG- } \\ 8 \end{gathered}$ | H-P | 608E | 10 | 480 | 0.5 | 100 | 5 | 0.1 | 1 | AM, FM, Pulse | C, R | 1450 |  |
|  | H-P | 608C | 10 | 480 | 1 | 50 | 5 | 0.1 | 1 | AM,FM, Pulse | C,R | 1200 | b |
|  | Gertsch | FM-9 | 150 | 486 | $\pm .0002$ | ina | 2 | 0.5 | . 05 | FM | C | 1495 |  |
|  | Clough-Brengle | 555 | 10 | 490 | 0.5 | 250 | 8 | 0.2 | 0.2 | AM | C | 485 |  |
|  | H-P | 3200B | 10 | 500 | $\pm 2$ | 20 | 6 | 1 | 3.1 | AM | $C, R$ | 475 |  |
|  | Gertsch | SSG-1 | 5 Hz | 500 | $\pm .00001$ | .00001\% | 12 | -130 dBm | 0 dBm | AM | C | 12,500 |  |
|  | R \& S | SMFA | 1.39 | 510 | $\pm 0.5$ | ina | 12 | . 03 |  | AM,FM | C | 7920 |  |
|  | AMI | 303H | 380 | 520 | $\pm 0.5$ | $\pm .005 \%$ | 1 | 0.1 | 0.3 | FM | C, R | 2800 |  |
|  |  | 1021UHF | 406 | 549 |  | $\pm .005 \%$ | 1 | 0.1 | . 07 | FM | C | 2950 | a |
|  | Babcock | BSG-17D |  |  |  |  | 1 |  |  | FM |  | 5600 |  |
| $\begin{gathered} \text { SG- } \\ 9 \end{gathered}$ | AMI | 303B | 400 | 550 | $\pm 0.5$ | .0025\% | 1 | 0.1 | 0.1 | FM | C,R | 1950 |  |
|  | RS | 1001 | 400 | 550 | $\pm 0.5$ | . $015 \%$ | 1 | 0.1 | 0.1 | FM | $C, R$ | 2925 |  |
|  | Microdot | 440/143-4RF | 400 | 550 | . 0003 | .0006\% | 1 | 0.1 | 1 | FM | $\mathrm{R}$ | request |  |
|  | RS | 5036-1 | $400{ }^{1}$ | 550 | ina | . $015 \%$ | 1 | 0.1 | 0.1 | FM | C,R | request |  |
|  | Microdot | 412A | 400 | 550 | . 0003 | .0005\% | 1 | 0.1 | 1 | FM | C | 9950 |  |
|  | Smyth | 606 | 38 | 600 | $\pm .005$ | $\pm .002 \%$ | 1 | -30 dBm | -160 dBm | AM,FM | R | 1295 |  |
|  | AMI | 303 | 225 | 800 | $\pm 0.5$ | $\pm .05 \%$ | 1 | 0.1 | $0.1$ | FM | C, R | 3600 | $b$ |
|  | Gen Radio | 1021-AU | 250 | 940 | 1 | ina | 1 | 0.5 | $1$ | AM | C | 895 |  |
|  | R \& S | SDAF | 170 | 940 | $\pm 1$ | 50 | 9 | 0.5 |  | AM,FM, Pulse |  | 4090 |  |
|  | Marconi | 1060/3 | 470 | 960 | $\pm 1$ | 50 | 1 |  | 0.223 | AM,FM | $C, R$ | 1895 |  |
| $\begin{aligned} & \text { SG- } \\ & 10 \end{aligned}$ | Motorola | T1034-C | 25 | 960 | 0.5 | ina |  | 0.1 | 0.1 | FM | C | 728 |  |
|  | Measurements | 560FM | 25 | 960 | 0.5 | ina | 6 | 0.1 | 0.1 | FM | C | 648 |  |
|  | Measurements | 84TVR | 400 | 1000 | 0.5 | ina | 1 | 0.1 | 0.3 | AM,FM | C | 785 |  |
|  | $R$ \& S | SDR | 300 | 1000 | $\pm 1$ | 50 | 8 | 1 | 3.5 | AM, Pulse | C | 2520 |  |
|  | Gertsch | FM-7 | 20 | 1000 | $\pm .0002$ | $\pm 1$ | 1 | note 6 | note 6 | AM,FM | $C, R$ | 1625 |  |
|  | Gertsch | SG-10 | 400 | 1200 | $\pm 1$ | ina | 1 | 0.1 | 0.5 | AM | R | 1395 | b |
|  | H-P | 8925A | 962 | 1213 | note 5 | ina | 1 | -100 dBm | -10 dBm | Pulse | C | 12,090 |  |
|  | $\mathrm{H}-\mathrm{P}$ | 612A | 450 | 1230 | $1$ | ina | 1 | $0.1$ | 0.5 | AM,FM, Pulse | C, R | 1400 | $b$ |
|  | RS | $1041 \mathrm{~L}$ | 1435 | 1535 | ina | $.0005 \%$ | 1 | $-20 \mathrm{dBm}$ | $-120 \mathrm{dBm}$ | FM | $C, R$ | 2950 |  |
|  | Microdot | 440/145-4RF | 1435 | 1555 |  | .0006\% | 1 |  |  | FM | R | request |  |
| SG-11 | R \& S | SCR | 1000 |  | $\pm 1$ | 50 | 4 | 1 | 2.7 | AM | C | 2190 |  |
|  | EPSCO | SG-161 | 900 | 2100 | $\pm 1$ | . $005 \%$ | 1 | 0.2 | 0.223 | Pulse | C,R | $1700$ |  |
|  | H-P | 614 A | 800 | 2100 | 1 | 50 | 1 | 0.1 | 0.224 | FM, Pulse | C,R | $1950$ | b |
|  | Gertsch | SG-11 | 900 | 2200 | $\pm 0.5$ | ina | 1 | 0.1 | 0.223 | FM, Pulse | $C^{\prime}$ | request |  |
|  | RS | 1041S | 2200 | 2300 | ina | .0005\% | 1 | $-20 \mathrm{dBm}$ | -120 dBm | FM | $C, R$ | 2950 |  |
|  | H-P | 8614A | 800 | 2400 | $\pm 0.5$ |  | 1 | -127 dBm | $+10 \mathrm{dBm}$ |  | C,R | 2100 |  |
|  | H-P | 8614 B | 800 | 2400 | $\pm 0.5$ | 50 | 1 | note 2 | 15 mW | AM,FM,Pulse | $C, R$ | 1450 | b |
|  | $R$ \& S | SBR | 1700 | 2700 | $\pm 1$ | 50 | 1 |  | 2 | AM | C | 2320 |  |
|  | R \& S | SLRD | 275 | 2750 | 2 | 50 | 2 | $-80 \mathrm{~dB}$ | ina | AM | C | 3995 |  |
|  | Polarad | $\begin{gathered} \text { MSG-IR/2R- } \\ \text { G24P } \end{gathered}$ | 2400 | 4000 | 1 | 50 | 1 | $-127 \mathrm{dBm}$ | $+10 \mathrm{dBm}$ | AM,FM,Pulse | C, R | 2250 | b, c |
| $\begin{gathered} \text { SG- } \\ 12 \end{gathered}$ | R \& S | SAR | 2700 | 4200 | $\pm 1$ | 20 | 1 | 5 | 3.4 | AM | C | 2930 |  |
|  | H-P | 616B | 1800 | 4200 | 1 | 50 | 1 | 0.1 | 0.223 | AM,FM,Pulse | C,R | 1950 | b |
|  | EPSCO | SG-153A | 1800 | 4200 | $\pm 1$ | .005\% | 1 | $0.1$ | 0.233 | FM,Pulse | C,R | 1750 |  |
|  | Gertsch | SG-12 | 1800 | 4400 | $\pm 0.5$ |  | 1 | $0.1$ | $0.223$ | FM,Pulse | $C^{\prime}$ | request |  |
|  | H-P | 8616A | 1800 | 4500 | $\pm 10 \mathrm{MHz}$ | 50 | 1 | -127 dBm | $\pm 10 \mathrm{dBm}$ | AM,FM,Pulse | C,R | $2100$ | b |
|  | H-P | 8616B | 1800 | 4500 | $\pm 10 \mathrm{MHz}$ | 50 | 1 | note 2 | 15 mW | AM,FM,Pulse | C,R | 1450 | b |
|  | Polarad | $\begin{aligned} & \text { MSG-IR/2R- } \\ & \text { G24 } \end{aligned}$ | 2000 | 4600 |  | 50 | 1 | -127 dBm | 0 dBm | AM, FM, Pulse | C,R | 1950 | $b, c$ |
|  | R \& S | SLRC | 2300 | 7000 | $\pm 1.5$ | 50 | 1 | 100 mW | 3 W | FM, Pulse | C | 6600 |  |
|  | Gertsch | SG-13 | 3800 | 7600 | $\pm 0.5$ | ina | 1 | 0.1 | 0.223 | FM, Pulse | C | request |  |
|  | EPSCO | SG-152 | 3800 | 7600 | 1 | .006\% | 1 | 0.1 | 0.223 | AM,FM, Pulse | C,R | 2025 |  |

Notes, abbreviations and manufacturers' index at end of this section.

## Signal generators $7780-39,700 \mathrm{MHz}$

|  | Manufacturer | Model | FREQUENCY |  |  |  | $\begin{aligned} & \text { \# of } \\ & \text { ranges } \end{aligned}$ | OUTPUT |  | Modulation | Type | Price \$ | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. MHz | Max. <br> MHz | Acc. \% | Stab. ppm |  | Min. $\mu V$ | Max. V |  |  |  |  |
| $\begin{gathered} \text { SG- } \\ 13 \end{gathered}$ | Dymec | 623B | 5820 | 7780 | . 03 | ina | 1 | 70 | 0.223 | AM,FM | C | 2250 |  |
|  | Polarad | 1107 | 3800 | 8200 | $\pm 0.5$ | 50 | 1 | $-127 \mathrm{dBm}$ | $+3 \mathrm{dBm}$ | AM,FM | R | 1900 | b |
|  | Polarad | 1207 | 3800 | 8200 | $\pm 0.5$ | ina | 1 | 50 mW | ina | AM,FM | R | 1425 | b |
|  | Dymec | DY-5636 | 7100 | 8500 | $\pm .03$ | ina | 1 | $+15 \mathrm{dBm}$ | -85 dBm | AM,FM, Pulse | C | 3800 |  |
|  | Dymec | 624C | 8500 | 10,000 | . 03 | ina | 1 | 2.23 | 0.223 | AM,FM, Pulse | $C, R$ | 2265 |  |
|  | Smyth | 608 | 600 | 10,000 | $\pm .005$ | $\pm .002 \%$ | 1 | -30 dBm | $-160 \mathrm{dBm}$ | AM,FM | R | 2-3000 ${ }^{(3)}$ |  |
|  | Gertsch | SG-14 | 7000 | 11,000 | $\pm 0.5$ | ina | 1 | 0.1 | 0.223 | FM, Pulse | C | request |  |
|  | EPSCO | SG-184 | 7000 | 11,000 | 1 | .006\% | 1 | 0.1 | 0.223 | AM,FM, Pulse | C, R | 2050 |  |
|  | Polarad | 1108 | 6950 | 11,000 | $\pm 0.5$ | ina | 1 | $-127 \mathrm{dBm}$ | $+3 \mathrm{dBm}$ | AM, FM, Pulse | R | 1900 | b |
|  | Polarad | 1208 | 6950 | 11,000 | $\pm 0.5$ | 50 | 1 | 25 mW | ina | AM,FM, Pulse | R | 1425 | b |
| $\begin{gathered} \text { SG- } \\ 14 \end{gathered}$ | Polarad | MSG-34 | 4200 | 11,000 | 1 | 100 | 1 | 0.1 | 0.223 | AM, FM, Pulse | C | 3680 |  |
|  | R \& S | SMCK | 1700 | 11,400 | $\pm 1$ | 10 | note 5 | 3 mW | 120 mW | AM,FM | C | note 5 |  |
|  | H-P | 626A | 10,000 | 15,500 | 1 | ina | 1 | $-90 \mathrm{dBm}$ | $+10 \mathrm{dBm}$ | AM,FM,Pulse | C,R | 3400 | b |
|  | H-P | 628A | 15,000 | 21,000 | 1 | ina | 1 | -90 dBm | $+10 \mathrm{dBm}$ | AM,FM, Pulse | $C, R$ | 3400 | b |
|  | Polarad | EHF-G1822 | 18,000 | 22,000 | 0.1 | ina | 1 | -90 dBm | $-10 \mathrm{dBm}$ | AM,FM,Pulse | C | 3315 | c |
|  | Polarad | EHF-G2225 | 22,000 | 25,000 | 0.1 | ina | 1 | -90 dBm | $-10 \mathrm{dBm}$ | AM,FM,Pulse | C | 3315 | c |
|  | Polarad | EHF-G2427 | 24,700 | 27,500 | 0.1 | ina | 1 | -90 dBm | $-10 \mathrm{dBm}$ | AM, FM, Pulse | C | 3315 | c |
|  | Polarad | EHF-G2730 | 27,270 | 30,000 | 0.1 | ina | 1 | -90 dBm | $-10 \mathrm{dBm}$ | AM,FM, Pulse | C | 3340 | c |
|  | Polarad | EHF-G3033 | 29,700 | 33,520 | 0.1 | ina | 1 | $-90 \mathrm{dBm}$ | $-10 \mathrm{dBm}$ | AM, FM, Pulse | C | 3340 | c |
|  | Polarad | EHF-G3336 | 33,530 | 36,250 | 0.1 | ina | 1 | -90 dBm | $-10 \mathrm{dBm}$ | AM,FM, Pulse | C | 3340 | c |
|  | Polarad | EHF-G3540 | 35,100 | 39,700 | 0.1 | ina | 1 | -90 dBm | $-10 \mathrm{dBm}$ | AM,FM,Pulse | C | 3340 | c |

## Signal generators Late arrivals



Notes, abbreviations and manufacturers' index at end of this section.

## NOTES

a. Battery operated.
b. Input voltage, 115 or $230 \mathrm{~V}, \pm 10 \%, 50-60 \mathrm{~Hz}, 1$ phase.
c. Prices shown are for tuning unit and basic power supply. The basic power supply can be used with any of this series of tuning heads.

1. Monitored by built-in frequency counter.
2. Attenuator range 130 dB .
3. Depending on RF unit desired.
4. Three separate oscillator units available, $1.7-5 \mathrm{GHz}$, $\$ 4110 ; 4.4-8.3 \mathrm{GHz}, \$ 4150$; $8-11.4 \mathrm{GHz}, \$ 4400$.
5. Determined by frequency counter setting.
6. Fundamental range $20-40 \mathrm{MHz}$, output 0.4 V across 50 ohms; harmonics, $40-100 \mathrm{MHz}$, output .002 V minimum across 50 ohms.

## ABBREVIATIONS

C Cabinet.
R Rack mount.
ina Information not available.
xtal Crystal.

# Tektronix oscilloscope displays both time-bases separately or alternately 

## TYPE 547 and 1A1 UNIT

DUAL TRACE DC-to- 50 MHz $50 \mathrm{MV} / \mathrm{CM}$ DC.TO-28 MHz, $5 \mathrm{MV} / \mathrm{CM}$

## SINGLE TRACE

## 2 Hz -to- 15 MHz $500 \mu \mathrm{~V} / \mathrm{CM}$ (Channels I AND 2 Cascaded)

## With automatic display switching, the

 Type 547 provides two independent oscilloscope systems in one cabinet, time-sharing a single-beam crt.
## Type 547 also uses



## Some Type 547/1A1 Unit Features

CRT (with internal graticule and controllable illumination) provides bright "no-parallax" displays of small spot size and uniform focus over the full $6 . \mathrm{cm}$ by $10 . \mathrm{cm}$ viewing area.

Calibrated Sweep Delay extends continuously from 0.1 microsecond to 50 seconds.
2 Independent Sweep Systems provide 24 calibrated time-base rates from $5 \mathrm{sec} / \mathrm{cm}$ to $0.1 \mu \mathrm{sec} / \mathrm{cm}$. Three magnified positions of $2 \mathrm{X}, 5 \mathrm{X}$, and 10 X , are common to both sweeps-with the 10 X magnifier increasing the maximum calibrated sweep rates to $10 \mathrm{nsec} / \mathrm{cm}$.

Single Sweep Operation enables oneshot displays for photography of either normal or delayed sweeps, including alternate presentations.

2 Independent Triggering Systems simplify set-up procedures, provide stable displays over the full passband and to beyond 50 MHz , and include brightline automatic modes for convenience.

Type 547 Oscilloscope (without plug-in unit)
Type 1A1 Dual-Trace Unit . . . . . . \$600
Rack-Mount Model Type RM547 . . . $\$ 1975$
U.S. Sales Prices f.o.b. Beaverton, Oregon
$\$ 1875$

## Tektronix, Inc.



For complete information, contact your
nearby Tektronix field engineer or write:
Tektronix, Inc., P.O. Box 500, Beaverton, Oregon 97005

## 2 signals - portions of each magnified

Trace 1 is Channel 2/B sweep, $10 \mu \mathrm{sec} / \mathrm{cm}$.
Trace 2 (brightened portion of Trace 1) is Channel 2/A sweep, $0.5 \mu \mathrm{sec} / \mathrm{cm}$.
Trace 3 is Channel $1 / B$ sweep, $10 \mu \mathrm{sec} / \mathrm{cm}$.
Trace 4 (brightened portion of Trace 3) is
Channel 1/A sweep, $0.5 \mu \mathrm{sec} / \mathrm{cm}$.
Using sweep delay technique-plus automatic alternate switching of the time bases-permits displaying both signals with a selected brightened portion and the brightened portions expanded to a full 10 centimeters.
B sweep triggering internally from Channel 1 (plugin) assures a stable time-related display without using external trigger probe.

## same signal - different sweeps

Upper trace is Channel 1/A sweep, $0.1 \mu \mathrm{sec} / \mathrm{cm}$.
Lower trace is Channel $1 / B$ sweep, $1 \mu \mathrm{sec} / \mathrm{cm}$.
Using different sweep rates to alternately display the same signal permits close analysis of waveform aberrations in different time domains.

(keyed to table locator symbols)
Advanced Measurement
Instruments, Inc (AMI)

| 302 | $(S G-4)$ |
| :--- | :--- |
| 303 | $(S G-9)$ |
| $303 A$ | $(S G-6)$ |
| $303 B$ | $(S G-9)$ |
| $303 H$ | $(S G-8)$ |
| 304 | $(S G-3)$ |

Aircraft Radio Corp
H-14A (SG-4)

Babcock Electronics Corp
BSG-17D (SG-8)

Clough-Brengle Co

| $299 A$ $(S G-2)$ <br> 555 $(S G-8)$ |  |
| :--- | :--- |
|  |  |
| Dymec |  |
|  |  |
| DY-5636 | (SG-13) |
| 623B | (SG-13) |
| $624 C$ | $(S G-13)$ |

Dynatronics

| DFS-23 | $(S G-15)$ |
| :--- | :--- |
| DFS-23A | $(\mathrm{SG}-15)$ |
| DFS-22 | $(\mathrm{SG}-15)$ |
| DFS-22A | $(\mathrm{SG}-15)$ |
| DFS-21A | $(\mathrm{SG}-15)$ |

Electronic Instrument Co, Inc (EICO)

| 315 | (SG-4) |
| :--- | :--- |
| 320 | (SG-3) |
| 324 | (SG-7) |

Electronic Measurements
Corp (EMC)
502 (SG-3)

- Conservatively rated for dependability.
- Simple to operate.
- Reasonably priced.

Other MEASUREMENTS products include: Frequency Meters, Deviation Meters, Megacycle (grid-dip) Meters, Pulse and Square Wave Generators, Crystal Calibrators, Vacuum Tube Voltmeters and Intermodulation Meters, made with the same painstaking care. For more information, drop us a line.


EPSCO, Inc

| SG-132A | (SG-6) |
| :--- | :--- |
| SG-152 | (SG-12) |
| SG-153A | (SG-12) |
| SG-161 | (SG-11) |
| SG-184 | (SG-13) |

General Radio Co
(Gen Radio)

| 1001A | $(\mathrm{SG}-2)$ |
| :--- | ---: |
| $1021-\mathrm{AU}$ | $(\mathrm{SG}-9)$ |
| $1021-\mathrm{AV}$ | $(\mathrm{SG}-5)$ |
| Grundig |  |
| AS2 | $(\mathrm{SG}-1)$ |
|  |  |
| Heath Co |  |
| IG-42 <br> IG-102 | (SG-1) |
|  | (SG-3) |
| Hewlett-Packard Co | (H-P) |
| 202H | (SG-4) |
| 202J | (SG-5) |

# The Standard Reference For Electronic Test Instruments <br> DIRECTORY OF TECHNICAL SPECIFICATIONS 

## 5

FREQUENCY METERS
upper frequency limit 1.15 Mc



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# Designed for <br> Adaptation 

## \$255.



Here is the practical oscilloscope for special applications-Data Instruments S51. This scope is designed for modification both physically and electrically and has a history of success in large volume OEM equipments as well as single installations. Versions of the S51 are currently performing with unusual success in medical applications for which new sensitivities were installed and controls were tailored to the habits of the personnel using them. The S51 is also used as original equipment in consoles of standard data handling and process control systems and has gained wide acceptance for use on assembly line testing and for educational purposes. The features that make the S51 particularly suitable for adaptation are: (a) The low initial cost of the instru-ment-\$255. (b) The large sophisticated CRT, which is capable of handling a broad range of requirements without additional circuitry. (c) The open construction which simplifies the physical problems of modification. (d) Its extremely light weight ( 16 lbs ). And (e) the high quality and performance of the basic instrument. Its specifications are:

| VERTICAL AMPLIFIER |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| BANDWIDTH | SENSITIVITY/CM | ATTENUATOR | IMPEDANCE | ACCURACY |  |  |  |  |
| DC- 3 MHz | 100 mv to 50 v | 9 position |  |  |  |  | $1 \mathrm{M} \Omega+30 \mathrm{pf}$ | $\pm 5 \%$ |
| TIME BASE |  | CRT |  |  |  |  |  |  |
| SPEED/CM |  <br> HOR. AMP. | DIA. | PHOSPHOR | VOLTS | DIM. \& WT. |  |  |  |
| $1 \mu \mathrm{~s}-0.1 \mathrm{sec}$. <br> $(6$ ranges) | Exp. $\times 2$ <br> $5 \mathrm{~Hz}-200 \mathrm{KHz}$ | $5^{\prime \prime}$ PDA | P1, P7 | 3.5 kv | $151 / 2^{\prime \prime} \times 8^{\prime \prime} \times 7^{\prime \prime}$ <br> 16 lbs |  |  |  |

Data Instruments maintains a staff of engineers experienced in special installations. If you have an unusual requirement for an oscilloscope, the chances are the S 51 can be modified to do the job.
Data Instruments Division - 7300 Crescent Blvd. - Pennsauken, N.J. 08110

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6. $\pm \mathbf{0 . 5} \%$ Accurate Digital Frequency Readout-programmable by rear tuning shaft extension, too.
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## 9. Full Phase-Lock Compatibility-all

 models designed to accept phase-lock frequency stabilization from the Polarad Model 3815-the highest-performance master-crystal stabilizer you can buy.10. In-Stock Availability-in small quantities, we ship from continually-replenished stock; larger quantities are scheduled on a 15-45 day cycle, currently. (Demos? Overnight by air!)

## Yes,

 IT'S TRUE-more engineers standardize on POLARAD Modular Microwave Signal Instrumentation every year ... won't use any other kind, in fact. The card below will bring you all the reasons for PEl's popularity-by return mail!
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My application is
The frequency range of interest to me is $\qquad$
$\qquad$
$\qquad$
Company $\qquad$
Address
City
$\qquad$
State
ip
Use this card for Fast, Direct Action.
(If card is missing, see back of this stub.)

| MSG－34 | $($ SG－14） |
| :--- | :--- |
| 1107 | $(S G-13)$ |
| 1108 | $(S G-13)$ |
| 1207 | $(S G-13)$ |
| 1208 | $(S G-13)$ |

$\left.\begin{array}{ll}\begin{array}{l}\text { Precise Electronics \＆} \\ \text { Development }\end{array} \\ \text { Corp }\end{array}\right)$（SG－5）

RCA，Electronic Components \＆Devices
WR－50B（SG－2）
Radiometer Electronics

| MS26 | （SG－4） |
| :--- | :--- |
| MS27 | （SG－5） |
| MS111 | （SG－3） |

Rohde \＆Schwarz Sales Co，Inc （ $\mathrm{R} \& \mathrm{~S}$ ）

| ASV | （SG－6） |
| :---: | :---: |
| SAR | （SG－12） |
| SBR | （SG－11） |
| SCR | （SG－11） |
| SDAF | （SG－9） |
| SDR | （SG－10） |
| SLRC | （SG－12） |
| SLRD | （SG－11） |
| SLSV | （SG－7） |
| SMAF | （SG－6） |
| SMAR | （SG－1） |
| SMCK | （SG－14） |
| SMDH | （SG－2） |
| SMFA | （SG－8） |
| SMLM | （SG－6） |
| SMLR | （SG－1） |

Sierra Electronic Div

| 350A | （SG－1） |
| :--- | :--- |
| 35IA | （SG－1） |
|  |  |
| Gertsch Products |  |
| Singer－Merrics Div |  |
| FM－7 | （SG－10） |
| FM－9 | （SG－8） |
| SG－8 | （SG－2） |
| SG－9 | （SG－6） |
| SG－10 | （SG－10） |
| SG－11 | （SG－11） |
| SG－12 | （SG－12） |
| SG－13 | （SG－12） |
| SG－14 | （SG－13） |
| SSG－1 | （SG－8） |

Smyth Research Associates

| 606 | $(S G-9)$ |
| :--- | :--- |
| 608 | $(S G-13)$ |

Tel－Instrument Electronics Corp（Tel－Inst）
1902A
（SG－1）
Triplett Electrical Instrument Co
3432A
（SG－5）
Manufacturers＇addresses and literature offerings in master cross index at front of issue．


## NEW OPERATIONAL AMPLIFIER COMPACT ELECTROMETER，TOO！

## Keithley Model 300

This economical little package is a true electrometer operational amplifier．It combines more than $10^{14}$ ohms input resistance， less than $5 \times 10^{-14}$ ampere offset curreht and ultra－low current drift of $10^{-15}$ ampere per day into a precise single－ended output design that meets demands in conditioning signals as low as $10^{-14}$ ampere． $\mathbb{E}$ Completely shielded，the 300 is a simple－to－use，easy mounting plug－in module．An output voltage of 11 volts at 11 ma is provided．Works to specs on unregulated supplies from $\pm 16$ to $\pm 25$ volts，at +25 ma or -8 ma ． ．For experiments or systems requiring extraordinary conditioning of small current signals，the Model 300 is the finest operational amplifier on the commercial market． Particularly for researchers in automated R \＆D，designers and producers of process or production control equipment．Ask your Keithley engineer for a demonstration．But read our technical engineering note first．It＇s yours by dropping us a line．

## CHARACTERISTICS

| Voltage Gain <br> dc open loop： | $>20,000$ | Voltage Offset | adjustable to <br> zero |
| :---: | :--- | :--- | :--- |
| Input |  | Voltage Drift | $<500 \mathrm{uv} / \mathrm{hr}$. |
| Resistance： | $>10^{14}$ ohms | Overload Limit | $\pm 400 \mathrm{~V}$ |
| Capacitance： | $<10 \mathrm{pf}$ | Output |  |
| Current Offset： | $<5 \times 10^{-14} \mathrm{amp}$ | Voltage： | $\pm 11 \mathrm{~V}$ |
| Current Drift： | $<10^{-15} \mathrm{amp} /$ day | Current： | $\pm 11 \mathrm{ma}$ |

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K曰エTエエIEエ INSTRUMENTS

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# Sweep away drift problems in narrow-band receiver tests. Use a sweep generator and scope for sensitivity and signal-to-noise measurement. 

Drift problems in a narrow-band communications receiver are relatively easy to overcomejust use a crystal oscillator rather than LC circuits. But what's the answer to drift in the signal generator testing the receiver? Variable tuning for a generator is a necessity to accomplish such basic tasks as out-of-band rejection tests. Frequency synthesizers can be used as a master oscillator, but, this is an expensive solution.
A more economical solution is found simply by varying the measuring technique. Use a frequen-cy-swept signal with the receiver's output displayed on a scope. Benefits are threefold:

- The test set-up is basically the same for all receivers. (Fig. 1).
- The test sequence is simple, quick and without calculation.
- Generator frequency drift is no longer a consideration.

In addition to the often-used bandwidth and selectivity measurements, sweep frequency techniques may be applied to determine sensitivity and signal-to-noise ratio for single sideband (SSB) and telegraphy receivers-both AM and FM.

## SSB and telegraphy receivers are simplest

Despite often exacting specs, SSB and telegraphy receivers are, in one respect, the easiest to test. Their general performance can be measured by using an unmodulated cw signal to simulate the wanted sideband. Since the test signal does not have to be modulated, noise-limited sensitivity can be read from a single display.

Receiver sensitivity is usually stated in terms of that input level necessary to obtain a specified signal-to-noise ratio (noise-limited sensitivity). In the case of an SSB receiver, it is simply given as an input voltage without specifying the amount of modulation. Using a signal generator, signal-tonoise ratio is determined by measuring the receiver's output power level with and without an input signal. Output power with zero input is, of course,

[^4]noise alone. Output power with a finite input signal is equal to the sum of the noise and the signal. Signal-to-noise ratio is then given by:
\[

$$
\begin{equation*}
\mathrm{S} / \mathrm{N}=\left[10 \log \left(P_{s} / P_{n}\right)-1\right] \mathrm{dB} \tag{1}
\end{equation*}
$$

\]

Where: $P_{s}$ is the output power with signal applied and $P_{n}$ is the output power with zero input.
For sensitivity measurements, noise is measured first, the required output signal level $P_{s}$ is calculated, and the generator is adjusted to produce this output power. Sensitivity voltage is then read directly from the attenuator setting.

Using sweep frequency, noise level and signal plus noise are displayed simultaneously since the baseline of the response display corresponds not to zero output but to the noise level. At the comparatively high input voltages used for bandwidth measurement, the difference is negligible. However, if the input voltage is reduced to the specified sensitivity level, it is necessary to turn up the effective gain of the scope's vertical amplifier to obtain a display. At this gain setting, the height of the displayed baseline is easily measured.
It is necessary to first establish the position of zero vertical input deflection on the baseline of the scope's graticule. This is done by disconnecting the vertical input and bringing the trace to the graticule baseline with the position control. Noise level, when the scope is reconnected, is simply the distance between the graticule and display baselines. The distance between the graticule baseline and the peak of the displayed response is proportional to signal-plus-noise voltage.

One minor point-signal-to-noise is essentially a power ratio, while scope deflection is proportional to peak voltage. This is true with the high levels used for frequency response measurement, but not necessarily true at the lower noise measurement signal levels. The answer lies in the detector used. Most diodes have transfer characteristics which are linear above 500 mV and approximate squarelaw responses below. Realizing this, it is easy to construct a detector with a voltage output nearly proportional to the mean power in its input circuit (See Fig. 2). The complete test set up for sensitivity measurement is shown in Fig. 3.

1. The generator is tuned and the sweep width adjusted to obtain a suitable display. The switch is

2. Conventional sweep generator-scope setup for dynamic display of receiver frequency response.
set to position 1 so that the scope has no vertical input and the trace then brought to the baseline.
3. The switch is then reset to position 2 and the AF gain of the receiver adjusted to bring the display baseline to the line on the dB scale corresponding to the specified signal-to-noise ratio.
4. The peak of the curve is brought to the $0-\mathrm{dB}$ line with the generator's attenuator controls, which then indicate sensitivity.

This sequence is simpler and the possibility of the generator drifting out of tune is negligible.

## Same set-up for AM receivers

If the generator has provisions for applying AM and frequency sweep simultaneously, the test setup to Fig. 3 is equally suitable for a conventional double sideband AM receiver. The usual method of displaying the response characteristic using a sweep generator is by connecting the scope's vertical input directly to the receiver's detector. However, for audio bandwidths, the application of a frequency-swept amplitude-modulated test signal gives accurate results. The AM frequency must be low (about $10 \%$ ) compared to the bandwidth, and the modulation depth should be restricted to about $20 \%$. Then the displayed response using the basic swept set-up is the same as that obtained by dc coupling the scope to the receiver's detector.

Maximum sensitivity is the term usually applied to what is virtually a receiver gain measurement expressed in terms of RF input voltage for a given AF output power. The bandwidth of receivers normally measured is seldom a small enough fraction of the tuning frequency to warrant any precaution against generator frequency drift. Here, the case for sweep frequency rests upon the ability to conduct a number of tests with the same basic set-up. In order to give an absolute measure of output power, the detector must be calibrated with a monitored AF signal. Having established the scope deflection for the required AF power, the measurement is a simple matter of adjusting the input signal level to produce this deflection at the center frequency of the display. Maximum sensitivity measurements are normally made with $30 \%$ modulation at 400 Hz . Application

2. Full-wave detector gives voltage output proportional to mean power applied to its input. With switch in position 1 , the unit is a peak voltage detector; a flip of the switch converts it to a square-law device. The $15-\Omega$ resistor is used only when necessary to terminate the receiver's AF output circuit.

3. Sensitivity measurement setup parallels basic frequency response setup with detector acting as a squarelaw device.
of this modulation may cause slight deformation of the skirts of display, but there is negligible amplitude error in the region of the peak.

Aside from the fact that the noise-limited sensitivity of an AM receiver is usually measured with $30 \%$ modulation applied to the carrier, the method of measurement is very similar to that used for SSB and telegraphy receivers. There is one important difference.

The noise level of a SSB receiver remains constant with or without the input signal. If an AM receiver is tuned to an unmodulated RF signal which is below the age threshold, the noise level rises noticeably as compared with the noise for zero input. Without an input signal, internally generated noise is not sufficient to drive the receiver's detector to the linear part of its characteristic. But, when an external carrier is applied, the noise voltages add to it and effectively produce random modulation which is linearly detected.

Signal-to-noise ratio is therefore always measured with the carrier applied throughout the test, at a level close to the specified sensitivity. Noise output power is first measured with the carrier unmodulated. Modulation is then applied and a second measurement made, giving the signal plus noise sum. The ratio is then calculated by the formula given for SSB receivers (Eq. 1).

Using sweep irequency, the sensitivity measure-
ment can again be made in three simple steps, without calculation and with complete independence from frequency drift. The set-up is again that of Fig. 3.

1. Vertical deflection with zero input is first set to the graticule baseline as before.
2. The switch is then set to position 2 and a response curve displayed by sweeping the unmodulated RF signal through the receiver's IF passband. This curve is due to the noise output of the receiver; therefore the receiver's AF gain is set to bring its peak to the line on the dB graticule corresponding to the required signal-to-noise.
$3.30 \%$ AM is applied to the carrier at the specified AF and the generator's attenuator is adjusted to bring the peak of the displayed curve to the $0-\mathrm{dB}$ line on the graticule. The attenuator reading is then the noise-limited sensitivity.

## Narrow-band FM receivers tax generator stability

Vhf or uhf narrow-band FM receivers probably tax the frequency stability of the generator more than any other type. In fixed and mobile point-topoint systems, channel spacings of 25 kHz are quite common, maximum rated deviation being 15 kHz . Noise-limited sensitivity measurements are usually made at peak deviation of $30 \%$ of maximum ( 5 kHz ) so that the signal generator needs to drift only about 6 kHz from center frequency before the outer significant sidebands fall outside the receiver's passband. At a tuning frequency of the order of 470 MHz this calls for a stability of about $0.00125 \%$ over the time necessary to make the measurement.

Because of the ready adaptability of many FM generators to sweep frequency methods, their use for the dynamic display of FM receiver characteristics is quite common. Display of the IF amplifier response requires a separate detector fed directly from the last IF stage, but otherwise, the method is similar to that used for any other type of receiver. The main application of the sweep generator to FM receivers, however, is for examination of demodulator characteristics. The dynamic display of demodulator response can be produced on a scope using any FM generator suitable for general receiver tests. However, maximum frequency deviation of the generator must be large enough to accommodate the entire demodulator response. Of receivers in common use, broadcast receivers, designed for $75-\mathrm{kHz}$ maximum deviation, require the widest sweep (about $\pm 100 \mathrm{kHz}$ ). To check the demodulator realistically, the test signal should be applied at full limiter voltage and it should also be derived from the correct source impedance. To obtain these conditions, use the IF amplifier of the receiver as the connecting network between the generator and the demodulator.

Then, the generator output is fed into the receiver's IF amplifier input or, into the antenna socket if this is more convenient. Care should be taken that the displayed demodulator characteristic is not modified by the frequency response characteristic of the receiver's tuned amplifiers. To do so, modulating frequency should be kept as low as conveniently possible ( 50 Hz under normal circumstances). The bandwidth of the receiver normally accommodates the multiple FM sidebands at much higher modulation frequencies, so all significant sidebands at $50-\mathrm{Hz}$ spacing are easily handled.

This usually necessitates modulating the generator from an external source, and, in this case, a sinewave is more convenient than a sawtooth. With sinewave modulation, the generator's modulation meter indicates the frequency deviation, which is half the sweep width. The horizontal deflection on the scope is obtained by also feeding the output of the modulating oscillator to the external time base terminal of the scope, and the total length of the trace then corresponds to twice the FM deviation as indicated on the modulation meter. Horizontal amplifier gain can then be adjusted so that the horizontal calibration of the scope's graticule becomes a frequency scale. The scope's vertical input is connected directly to the audio output terminal of the receiver's demodulator. The high input impedance of the scope is unlikely to affect demodulator operation. With the signal generator tuned to the IF (or RF) center frequency, sufficient output is applied to operate the limiter of the receiver. The familiar " S " shaped demodulator response will be displayed.

If the FM generator is suitable, a much more useful display can be produced using two superimposed modulating frequencies. When the object of the display is measurement of true demodulator linearity over the nominally linear part of its characteristic, more information can be gained from a display of the derivative of the demodulation curve. This is a display in which the instantaneous vertical position of the spot is proportional to the instantaneous slope of the demodulation curve. Such a display gives far better discrimination than the direct response curve (see Fig. 4).

The test set-up is shown in Fig. 5. A slow sawtooth voltage or low-frequency sinewave (about $60-\mathrm{Hz}$ ) is simultaneously applied to the generator's external modulation terminals and the horizontal deflection system of the scope. The amplitude of this sweep voltage should be such as to give a frequency sweep which completely accommodates the demodulator characteristic. Its frequency should be below the low-frequency response of the receiver's audio amplifier. Superimposed upon this voltage, by means of the transformer, is an AF voltage (say 1 kHz ) of sufficient

4. Derivative of FM demodulator response (bottom curve) shows changes in slope much more markedly than direct response (upper curve).
amplitude to give about $1 \%$ of maximum rated deviation. The vertical input terminal of the scope is connected via a detector to the AF output of the receiver. Thus, both the gain and the low-frequency output of the audio amplifier are utilized. The instantaneous $1-\mathrm{kHz}$ receiver output is then directly proportional to the slope of the demodulation curve at the instantaneous input carrier frequency , so that the spot traces out the derivative curve. Any nonlinearity is easily detected by aligning the curve with one of the horizontal graticule lines on the scope. Also, the relative magnitude of the nonlinearity can be measured by comparing the amplitude of the departure from this line with the mean height of the display from the zero points.

The procedure for making signal-to-noise measurements using sweep frequency parallels the static method. With true zero established at the graticule baseline, a modulated signal is applied to the receiver (the low-voltage AF modulating voltage is superimposed on the sweep voltage). Most specs quote noise-limited sensitivity with FM applied at $30 \%$ of the maximum rated deviation. This FM level naturally distorts the edges of the derivative curve, but this is unimportant because the height of the displayed curve at the center frequency remains proportional to the intune output of the receiver. Then, with the modulated RF input level approximately at the specified sensitivity level, the AF gain of the receiver is adjusted to bring the peak of the "modulation on" curve to the $0-\mathrm{dB}$ line on the graticule. The modulation voltage is then switched off so that the scope displays a curve representing noise level as a function of RF input frequency. Because the application of an RF input reduces the receiver noise output, this second curve is inverted as shown in Fig. 6 with the trough indicating the in-tune noise level. The RF output of the generator is adjusted to bring the lowest point on the displayed curve into coincidence with the $d B$ graticule line corre-

5. Test setup for demodulator derivative curve. For sensitivity measurement, the generator's RF output is applied to the receiver's antenna input.


AM RECEIVER DISPLAY
FM RECEIVER DISPLAY
6. Modulation on/modulation off displays for AM (left) and FM (right) receiver noise-limited sensitivity. Trough in FM display indicates in-tune noise level.
sponding to the specified signal-to-noise ratio. Noise-limited sensitivity is then read from the generator's attenuator dials.

Accurate tuning is essential for signal-to-noise measurement on an FM receiver because part of the AM rejection takes place in the demodulator itself. When the measurement is made with sweep frequency, this aspect is dealt with automatically.

## Consider the effect of sweep speed

For all of the tests, the most important general rule to be remembered is the relation between sweep speed and bandwidth. For measurements which are not concerned with the true shape of the frequency response characteristic, it is tempting to increase sweep speed and ignore the effects of ringing in the receiver's amplifier. This can lead to amplitude error and should be avoided. As a rule of thumb to establish maximum permissible sweep speed, there is no significant deformation if the highest frequency component of the displayed response is less than $1 \%$ of the receiver's $3-\mathrm{dB}$ bandwidth. - -

For information on how to use these tables, turn to page 2

|  | Manufacturer | Model | FREQUENCY |  | SWEEP WIDTH |  |  | OUTPUT |  | Type | $\begin{gathered} \text { Price } \\ \$ \end{gathered}$ | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\underset{\mathrm{kHz}}{\mathrm{Min} .}$ | Max. <br> MHz | Min. kHz | Max. <br> MHz | $\begin{aligned} & \text { Rate } \\ & \mathrm{Hz} \end{aligned}$ | Volts | Imp. Ohms |  |  |  |
| SW- 1 | ITT <br> AMI <br> LTV Ling <br> Probescope <br> Spectral Dynamics <br> LTV Ling <br> Spectral Dynamics <br> Clough-Brengle <br> Waveforms <br> Telonic | $\begin{aligned} & \hline 74217-A \\ & 321 \\ & \text { CO-10-A } \\ & 5 \\ & \text { SD-104-5 } \\ & \text { CO-10-B } \\ & \text { SD-104-1 } \\ & 182-A \\ & 610 B \\ & \text { LA-1M/SM-2000 } \end{aligned}$ | $\begin{array}{\|l} \hline .03 \\ 1 \\ .005 \\ 0 \\ .005 \mathrm{~Hz} \\ .01 \\ .01 \mathrm{~Hz} \\ .025 \\ .02 \\ .02 \end{array}$ | .004 .005 .005 .005 .05 .01 .01 .015 .02 .02 | ina . 05 note 8 . 02 .005 Hz note 8 . 01 Hz 0 ina .05 | ina <br> 0.2 kHz <br> note 8 <br> 0.6 <br> .05 <br> note 8 <br> .01 <br> full rng <br> ina <br> .02 | $\begin{aligned} & \text { ina } \\ & .03-1 \text { sec } \\ & \text { note } 9 \\ & 1-30 \text { sec } \\ & 0-1000 \\ & \\ & \text { note } 9 \\ & 0-200 \\ & 5 \\ & 6-60 \mathrm{sec} \\ & .01-100 \end{aligned}$ | $\begin{aligned} & -20 \mathrm{dBm} \\ & 1 \\ & 0.1-1 \\ & 1 \\ & 1 \\ & 0.1-1 \\ & 1 \\ & 0.1 \mathrm{~W} \\ & 2.5 \\ & 17 \end{aligned}$ | 600 <br> 600 <br> ina <br> ina <br> 600 <br> ina <br> 600 <br> 600,20k <br> 600 <br> 600 | $\begin{aligned} & C \\ & C \\ & R \\ & R \\ & R \\ & R \\ & R \\ & R \\ & R \\ & C, R \\ & C, R \\ & C, R \end{aligned}$ | $\begin{array}{r} 2550 \\ 2975 \\ 1360 \\ 475 \\ 1965 \\ \\ 1360 \\ 1975 \\ 185 \\ 1000 \\ 1770 \end{array}$ | $\begin{aligned} & a \\ & a, f \end{aligned}$ |
| SW- 2 | H-P <br> Spectral Dynamics <br> Clough-Brengle <br> Clough-Brengle <br> Probescope <br> Kay <br> Kay <br> Probescope <br> Kay <br> Telonic | 207A <br> SD-104-2 <br> 282-A <br> 610-A <br> 100 <br> 141 <br> P141A <br> 500 <br> P142 <br> L-1/SM-2000 | $\begin{aligned} & .02 \\ & .02 \mathrm{~Hz} \\ & .025 \\ & .025 \\ & 0 \\ & .02 \\ & .02 \\ & 0 \\ & .035 \\ & 400 \end{aligned}$ | $\begin{aligned} & .02 \\ & .02 \\ & .032 \\ & .046 \\ & 0.1 \\ & 0.2 \\ & 0.2 \\ & 0.5 \\ & 0.5 \\ & 1.8 \end{aligned}$ | note 18 <br> .02 Hz <br> 0.5 . <br> 0 <br> 0.2 <br> 0 <br> 2 <br> 0 $0.1 \%$ | note 18 <br> .02 <br> .01 <br> . 02 <br> . 02 <br> full rng <br> .02 <br> 0.2 <br> .04 <br> 40\% | $\begin{aligned} & \text { note } 18 \\ & 0-1000 \\ & 2-10 \\ & 2-10 \mathrm{sec} \\ & 1 \mathrm{sec} \\ & 0.2-30 \\ & 0.3-30 \\ & 0.33 \mathrm{sec} \\ & 0.2-30 \\ & .01-100 \end{aligned}$ | $\begin{aligned} & 10 \\ & 1 \\ & 0.1 \mathrm{w} \\ & 0.1 \mathrm{w} \\ & 10 \\ & \\ & 5 \\ & 1 \\ & 10 \\ & 1 \\ & 1 \end{aligned}$ | 600 600 $600,4 \mathrm{k}$ 4000 ina 600 50 ina 50 50 | $\begin{aligned} & C, R \\ & R \\ & C, R \\ & C, R \\ & C, R \\ & R \\ & C, R \\ & C, R \\ & R \\ & C, R \\ & C, R \\ & C, R \end{aligned}$ | $\begin{array}{r} 425 \\ 1965 \\ 485 \\ 485 \\ 425 \\ 1295 \\ 475(12) \\ 450 \\ 475(12) \\ 1075 \end{array}$ | $\begin{aligned} & a, e \\ & a, e \\ & a, e \\ & a, f \end{aligned}$ |
| SW- 3 | Kay <br> Telonic <br> Tel-Inst <br> Tel-Inst <br> Telonic <br> Telonic <br> R \& S <br> Telonic <br> Jerrold <br> Telonic | $\begin{aligned} & \text { P130 } \\ & \text { L-2/SM-2000 } \\ & 1902 \mathrm{~A} \\ & 1105 \\ & \text { HD-4 } \\ & \text { SV-14 } \\ & \text { SWH } \\ & \text { VR-2M/SM-2000 } \\ & 1015 \\ & \text { L-3/SM-2000 } \end{aligned}$ | $\begin{aligned} & 0.1 \\ & 1000 \\ & 4500 \\ & 50 \\ & 10 \\ & 10,200 \\ & 100 \\ & 50 \\ & 0.2 \\ & 1 \\ & 4000 \end{aligned}$ | $\begin{array}{\|l\|} \hline 2 \\ 4 \\ 4.5 \\ 10 \\ 10 \\ \\ 11.2 \\ 12 \\ 12 \\ 15 \\ 16 \end{array}$ | $\begin{aligned} & 0 \\ & 0.1 \% \\ & \text { note } 7 \\ & 0 \\ & 25 \\ & 150 \\ & 150 \\ & .05 \% \\ & 0.1 \\ & 0 \\ & 0.1 \% \end{aligned}$ | full rng full rng note 7 full rng 10 <br> full rng 5\% 10 full rng 75\% | $0.2-30$ $.01-100$ 2000 60 $50 / 60$ $50 / 60$ 20 $.01-100$ $.007-60$ $.01-100$ | $\begin{aligned} & 1 \\ & 1 \\ & 0.75 \\ & 2 \\ & 1 \\ & 3.5 \mu \mathrm{~V}-1 \\ & 50 \mu \mathrm{~V}-2 \\ & 1 \\ & 2.236 \\ & 1 \end{aligned}$ | 50 <br> 50 <br> 75 <br> 75 <br> 50,75 <br> 75 <br> 60 <br> 50 <br> 50,75 <br> 50 | $\begin{aligned} & C, R \\ & C, R \\ & C \\ & C, R \\ & C, R \\ & C, R \\ & C \\ & C \\ & C, R \\ & C, R \\ & C, R \end{aligned}$ | $\begin{gathered} 375(12) \\ 1075 \\ 480 \\ 880 \\ 745 \\ 850 \\ 1440 \\ 1725 \\ 2540 \\ 1075 \end{gathered}$ | a, e $a, f$ b $a, d$ <br> $a, f$ <br> $a, f$ |
| SW- | Telonic <br> Marconi <br> Kay <br> R \& S <br> Kay <br> Texscan <br> Kay <br> Telonic <br> Kay <br> Jerrold | 1001 <br> TF-1099 <br> 150B <br> SWOF <br> P152 <br> VS-20 <br> P855 <br> L-4/SM-2000 <br> 370A <br> H-73/707C | $\begin{aligned} & 100 \\ & 100 \\ & 50 \\ & 20 \\ & 10 \\ & 0 \\ & 0.2 \\ & 2000 \\ & 10,000 \\ & 20,000 \\ & 2000 \end{aligned}$ | $\begin{aligned} & 20 \\ & 20 \\ & 20 \\ & 20 \\ & 20 \\ & 25 \\ & 32 \\ & 40 \\ & 50 \\ & 50 \end{aligned}$ | 10 0 0 1000 0.5 0 0 $0.1 \%$ ina $\pm 0.5 \%$ | 20 full rng full rng 16 20 <br> full rng 2\% 80\% note 13 $\pm 60 \%$ | $\begin{aligned} & .01-60 \\ & 50-60 \\ & 60 \\ & 0.2-20 \\ & 0.2-30 \\ & 5-60 \\ & 0.2-30 \\ & .01-100 \\ & 60 \\ & .007-60 \end{aligned}$ | $\begin{aligned} & 1 \\ & 0.3-3 \\ & 0.2 \\ & .001-1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 0.25 \\ & 20 \mathrm{dBm} \end{aligned}$ | $\begin{aligned} & 50 \\ & 75 \\ & 70 \\ & 75 \\ & 50 \\ & 50 \\ & 50 \\ & 50 \\ & 70 \\ & 50 \end{aligned}$ | $C, R$ $C, R$ $C, R$ $C, R$ $C, R$ $C, R$ $C, R$ $C, R$ $C, R$ $C$ | $\begin{array}{r} \text { request } \\ 1265 \\ 595 \\ 5600 \\ 375(12) \\ 850 \\ 850 \\ 1075 \\ 595(12) \\ 495 \\ 840 \end{array}$ | $\begin{aligned} & e \\ & a, e \\ & a, e \\ & c \\ & a, e \\ & a, f \\ & a, e \\ & e, f \end{aligned}$ |
| $\begin{gathered} 5 W- \\ 5 \end{gathered}$ | RCA <br> Kay <br> Clough-Brengle <br> Tel-Inst <br> Telonic <br> Telonic <br> Telonic <br> Telonic <br> Kay <br> Texscan | $\begin{aligned} & \text { WR-69A } \\ & 380 A \\ & 603 \\ & 1500 B \\ & \text { L-5/SM-2000 } \\ & \\ & \text { LD-5 } \\ & \text { SSX-2 } \\ & \text { HD-7 } \\ & 386 A R \\ & \text { HS-70 } \end{aligned}$ | $\begin{aligned} & 50 \\ & 20,000 \\ & 20,000 \\ & 400 \\ & 20,000 \\ & 20,000 \\ & 20,000 \\ & 100 \\ & 455 \\ & 20,000 \end{aligned}$ | $\begin{aligned} & \hline 50 \\ & 60 \\ & 60 \\ & 70 \\ & 75 \\ & 75 \\ & 75 \\ & 75 \\ & 98 \\ & 100 \end{aligned}$ | $\begin{aligned} & 0 \\ & 3000 \\ & 0 \\ & 0 \\ & 0.1 \% \\ & .05 \% \\ & 0.1 \% \\ & 100 \\ & 60 \\ & 0.1 \% \end{aligned}$ | 20 <br> 20 <br> 12 full rng 40\% <br> 40\% <br> 40\% <br> 50 <br> 24 <br> 15\% | 60 60 60 ina $.01-100$ $50 / 60$ 60 $50 / 60$ ina $50 / 60$ | 0.1 <br> 0.25 <br> 0.1 <br> 1 <br> 1 <br> $1 \mu \mathrm{~V}-1$ <br> 1 <br> 0.2 <br> 4 W | $\begin{aligned} & 100 \\ & 70 \\ & 75 \\ & 75 \\ & 50 \\ & \\ & 50 \\ & 50 \\ & 50,75 \\ & 50 \\ & \text { ina } \end{aligned}$ | $C$ $C, R$ $C$ $C$ $C$ $C, R$ $C, R$ $C, R$ $C, R$ $C, R$ $C, R$ | $\begin{array}{r} 295 \\ 450 \\ 250 \\ 595 \\ 1075 \\ \hline 695 \\ 1695 \\ 695 \\ 1250 \\ 2500 \end{array}$ | a,e <br> $a, b$ <br> a,f <br> a <br> d <br> c |
| $\begin{gathered} \text { SW- } \\ 6 \end{gathered}$ | Telonic <br> Jerrold <br> Texscan <br> Wiltron <br> Kay <br> Heath <br> Telonic <br> Telonic <br> H-P <br> Jerrold | $\begin{aligned} & \text { PD-2 } \\ & \text { H-71/707C } \\ & \text { VS-30 } \\ & \text { 610 } \\ & \text { 154A } \\ & \text { FMO-1 } \\ & \text { SV-14 } \\ & \text { LH-2/SM-2000 } \\ & 3211 \mathrm{~A} \\ & 602-5 B \end{aligned}$ | $\begin{aligned} & 20,000 \\ & 10,000 \\ & 100 \\ & 100 \\ & 50 \\ & 90,000 \\ & 84,000 \\ & 400 \\ & 100 \\ & 4000 \end{aligned}$ | 100 100 100 100 100 107 110 110 110 112 | $\begin{aligned} & 0.2 \% \\ & \pm 0.5 \% \\ & 0 \\ & 0 \\ & 0 \\ & 200 \\ & 4000 \\ & 40 \\ & 0 \\ & \pm 1 \% \end{aligned}$ | 10\% $\pm 60 \%$ full rng full rng full rng 1 full rng 40 full rng $\pm 60 \%$ | $\begin{aligned} & 50 / 60 \\ & .007-60 \\ & 5-60 \\ & .01-10 \mathrm{sec} \\ & 5-60 \\ & 60 \\ & 50 / 60 \\ & .01-100 \\ & 10-100 \\ & 50-60 \end{aligned}$ | $\begin{aligned} & 14 \\ & 20 \mathrm{dBm} \\ & 1 \\ & 1 \\ & 1 \\ & 0.5 \\ & 0.5 \mathrm{~V}-1 \\ & 3.5 \mathrm{~V}-1 \\ & 0.25 \\ & 0.7 \\ & 2.5 \end{aligned}$ | 50 <br> 50 <br> 50 <br> 50 <br> 50 <br> 50 <br> 75 <br> 50 <br> 50 <br> 50,75 | $C, R$ $C, R$ $C, R$ $C, R$ $C, R$ $C$ $C$ $C$ $C, R$ $C, R$ $C, R$ | $\begin{array}{r} 2500 \\ 840 \\ 850 \\ 1975 \\ 895 \\ \\ 35 \mathrm{kit} \\ 850 \\ 1275 \\ 1000 \\ 475 \end{array}$ |  |

Notes, abbreviations and manufacturers' index at end of this section.

## Sweep generators $115-950 \mathrm{MHz}$

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \& \multirow[b]{2}{*}{Manufacturer} \& \multirow[b]{2}{*}{Model} \& \multicolumn{2}{|l|}{FREQUENCY} \& \multicolumn{3}{|c|}{SWEEP WIDTH} \& \multicolumn{2}{|c|}{OUTPUT} \& \multirow[b]{2}{*}{Type} \& \multirow[b]{2}{*}{Price \$} \& \multirow[b]{2}{*}{Notes} \\
\hline \& \& \& Min. kHz \& \begin{tabular}{l}
Max. \\
MHz
\end{tabular} \& Min. kHz \& Max. MHz \& \[
\begin{aligned}
\& \text { Rate } \\
\& \mathrm{Hz}
\end{aligned}
\] \& Volts \& Imp. Ohms \& \& \& \\
\hline \[
\begin{gathered}
S W- \\
7
\end{gathered}
\] \& \begin{tabular}{l}
Kay \\
Kay \\
AMI \\
Telonic \\
Kay \\
Kay \\
Hickok \\
Jerrold \\
Telonic \\
Telonic
\end{tabular} \& \begin{tabular}{l}
P154 \\
866A \\
301 \\
L-6/SM-2000 \\
865A \\
932B \\
288AX \\
H-72/707C \\
HD-3 \\
L-7/SM-2000
\end{tabular} \& \[
\begin{aligned}
\& .05 \\
\& 4 \\
\& .01 \\
\& 50 \\
\& 10 \\
\& 0.1 \\
\& .035 \\
\& 20 \\
\& 1 \\
\& 100
\end{aligned}
\] \& \[
\begin{aligned}
\& 115 \\
\& 120 \\
\& 120 \\
\& 125 \\
\& 135 \\
\& 150 \\
\& 160 \\
\& 200 \\
\& 200 \\
\& 210
\end{aligned}
\] \& 0 ina 0 0.1\% ina note 14 0 \(\pm 0.5 \%\) 200 0.1\% \& \[
\begin{array}{|l|}
\hline 100 \\
30 \\
3 \\
30 \% \\
30 \\
\\
\text { note } 14 \\
0.45 \\
\pm 60 \% \\
\text { full rng } \\
25 \%
\end{array}
\] \& \begin{tabular}{l}
0-30 \\
60 \\
ina .01-100 \\
60 \\
60 \\
60 \\
.007-60 \\
50/60 \\
.01-100
\end{tabular} \& \[
\begin{array}{|l|}
\hline 1 \\
1 \\
\text { ina } \\
1 \\
1 \\
\\
0.25,1 \\
\text { ina } \\
13 \mathrm{dBm} \\
0.25 \\
0.75
\end{array}
\] \& \[
\begin{aligned}
\& 50 \\
\& 70 \\
\& \text { ina } \\
\& 50 \\
\& 70 \\
\& \\
\& 70 \\
\& 100 \\
\& 50 \\
\& 50,75 \\
\& 50
\end{aligned}
\] \& \begin{tabular}{l}
C,R C,R C,R C,R C,R \\
C, R C C,R C,R C,R
\end{tabular} \& \[
\begin{gathered}
\hline 495(12) \\
950 \\
3000 \\
1075 \\
950 \\
825 \\
315 \\
840 \\
835 \\
1075
\end{gathered}
\] \& \(a, e\) \(a, d, e\) \(a, f\) \(a, d, e\) \(a, d, e\) e,f \(a, f\) \\
\hline SW- \& \begin{tabular}{l}
Prec Apparatus \\
Kay \\
Tel-Inst \\
Kay \\
EICO \\
Jerrold \\
AMI \\
Heath \\
EICO \\
Kay
\end{tabular} \& \begin{tabular}{l}
E410C \\
932A \\
1212 \\
361C \\
368 \\
H-75/707C \\
320 \\
IG-52 \\
369 \\
P860
\end{tabular} \& \[
\begin{aligned}
\& 3 \\
\& 0.1 \\
\& 54 \\
\& 43.5 \\
\& 3 \\
\& \\
\& 45 \\
\& 4 \\
\& 3.6 \\
\& 3 \\
\& 2
\end{aligned}
\] \& \[
\begin{aligned}
\& 213 \\
\& 215 \\
\& 216 \\
\& 216 \\
\& 216 \\
\& 220 \\
\& 220 \\
\& 220 \\
\& 220 \\
\& 220
\end{aligned}
\] \& 0
note 15
10,000
15,000
0
\(\pm 0.5 \%\)
0
0
0
10 \& \[
\begin{aligned}
\& 30 \\
\& \text { note } 15 \\
\& 15 \\
\& \text { ina } \\
\& 30 \\
\& \\
\& 460 \% \\
\& 3 \\
\& 42 \\
\& 20 \\
\& 30
\end{aligned}
\] \& \begin{tabular}{l}
60 \\
60 \\
ina \\
60 \\
60
\[
\begin{aligned}
\& .007-60 \\
\& \text { ina } \\
\& 60 \\
\& 60 \\
\& 0.2-30
\end{aligned}
\]
\end{tabular} \& \[
\begin{aligned}
\& 0.1 \\
\& 0.25,1 \\
\& 0.5 \\
\& 1 \\
\& 0.1 \\
\& 13 \mathrm{dBm} \\
\& 1 \mu V-0.1 \\
\& .08-0.23 \\
\& 0.1 \\
\& 1
\end{aligned}
\] \& \[
\begin{aligned}
\& 50 \\
\& 70 \\
\& 75,300 \\
\& 70 \\
\& 50 \\
\& 50 \\
\& 50 \\
\& 50 \\
\& 50 \\
\& 50 \\
\& 50
\end{aligned}
\] \& \[
\begin{aligned}
\& R \\
\& C, R \\
\& C \\
\& C, R \\
\& C, R \\
\& C, R \\
\& C, R \\
\& C \\
\& C \\
\& C, R
\end{aligned}
\] \& \[
\begin{gathered}
160 \\
825 \\
950 \\
845 \\
120 \\
890 \\
485 \\
68 \\
150 \\
445(12)
\end{gathered}
\] \& \[
\begin{aligned}
\& a, e \\
\& a, \\
\& a, e \\
\& a, b \\
\& e, f \\
\& a, b \\
\& a, b \\
\& a, b \\
\& a, b
\end{aligned}
\] \\
\hline SW- \& \begin{tabular}{l}
GE \\
Kay \\
Telonic \\
Jerrold \\
R\& S \\
Hickok \\
EICO \\
Telonic \\
Texscan \\
Gen Radio
\end{tabular} \& \[
\begin{aligned}
\& \text { ST-4A } \\
\& 935 B \\
\& \text { SV-13 } \\
\& 601-5 B \\
\& \text { SWF } \\
\& \\
\& 615 \\
\& 360 \\
\& 3001 / \text { SM }-2000 \\
\& \text { TH-200 } \\
\& 1025-A
\end{aligned}
\] \& \[
\begin{aligned}
\& 0.1 \\
\& 50 \mathrm{~Hz} \\
\& 20 \\
\& 12 \\
\& 5 \\
\& \\
\& 0 \\
\& 0.5 \\
\& 50 \\
\& 1 \\
\& 0.7
\end{aligned}
\] \& 220
220
225
225
225
225
228
230
230
230 \& 500
20
note 3
\(\pm 1 \%\)
.05
0
0
2000
100
0 \& \begin{tabular}{l}
15 60\% \\
note 3 \(\pm 60 \%\) \\
15 \\
15 \\
30 \\
180 \\
230 \\
full rng
\end{tabular} \& \begin{tabular}{l}
ina \\
0.2-30 \\
50/60 \\
50-60 \\
60 \\
60 \\
60 \\
.01-100 \\
50/60 \\
20
\end{tabular} \& \[
\begin{aligned}
\& 0.5 \\
\& 1 \\
\& 1 \\
\& 0.5 \\
\& 0.1 \mathrm{~m} V-0.1 \\
\& \text { ina } \\
\& \text { ina } \\
\& 1 \\
\& 0.25 \\
\& 0.3 \mu \mathrm{~V}-1
\end{aligned}
\] \& \[
\begin{aligned}
\& 20-70 \\
\& 70 \\
\& 50,60,75 \\
\& 50,75 \\
\& 60 \\
\& 90 \\
\& \text { ina } \\
\& 50 \\
\& 50 \\
\& 50
\end{aligned}
\] \& \[
\begin{aligned}
\& C, R \\
\& C, R \\
\& C \\
\& C, R \\
\& C R \\
\& C \\
\& C \\
\& C \\
\& C, R \\
\& C \\
\& C, R
\end{aligned}
\] \& request
1295
833
450
1400
360
50
570
1570
525
3450 \& \[
\begin{aligned}
\& a \\
\& e \\
\& a \\
\& a \\
\& \\
\& b \\
\& b \\
\& f \\
\& c
\end{aligned}
\] \\
\hline \[
\begin{gathered}
\text { SW- } \\
10
\end{gathered}
\] \& \begin{tabular}{l}
Texscan \\
Telonic \\
Kay \\
Kay \\
Jerrold \\
Texscan \\
Kay \\
Kay \\
Telonic \\
Micro-Power
\end{tabular} \& \begin{tabular}{l}
\[
\begin{aligned}
\& \mathrm{HS}-75 \\
\& \mathrm{PD}-3 \\
\& 385 \mathrm{~A} \\
\& 159 \mathrm{~B} \\
\& \mathrm{SS}-300
\end{aligned}
\] \\
VS-40 \\
386AN \\
386 \\
PD-7 \\
H24MD/220
\end{tabular} \& \[
\begin{aligned}
\& 100 \\
\& 100 \\
\& 1 \\
\& 1 \\
\& 0.5 \\
\& 0.5 \\
\& 0.5 \\
\& 6.975 \\
\& 1 \\
\& 200 \\
\& 200
\end{aligned}
\] \& \[
\begin{aligned}
\& 250 \\
\& 250 \\
\& 260 \\
\& 300 \\
\& 300 \\
\& \\
\& 300 \\
\& 332.15 \\
\& 350 \\
\& 375 \\
\& 400
\end{aligned}
\] \& 0.1\%
\(0.2 \%\)
70
50
200

200
note 16
$60 \%$
$0.2 \%$

0 \& $$
\begin{array}{|l|}
15 \% \\
15 \% \\
70 \\
\text { full rng } \\
300 \\
300 \\
\text { note } 16 \\
70 \% \\
10 \% \\
\text { full rng }
\end{array}
$$ \& \[

$$
\begin{aligned}
& 50 / 60 \\
& 50 / 60 \\
& 60 \\
& 5-60 \\
& .003-60 \\
& 5-60 \\
& \text { ina } \\
& 60 \\
& 50 / 60 \\
& .01-100 \mathrm{sec}
\end{aligned}
$$

\] \& | 14 |
| :--- |
| 0.5 |
| 0.5 |
| 0.6 |
| 0.5 |
| 0.5 |
| 0.5 |
| 14 |
| . 02 W | \& \[

$$
\begin{aligned}
& \text { ina } \\
& 50 \\
& 70 \\
& 50 \\
& 50 \\
& 50 \\
& 50 \\
& 70 \\
& 50,70 \\
& 50 \\
& \text { ina }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& C, R \\
& C, R \\
& C, R \\
& C, R \\
& C, R \\
& C, R \\
& C, R \\
& C, R \\
& C, R \\
& C, R \\
& C
\end{aligned}
$$

\] \& \[

$$
\begin{array}{r}
2500 \\
2500 \\
725 \\
895 \\
1095 \\
850 \\
1220 \\
925 \\
2500 \\
3650
\end{array}
$$

\] \& \[

$$
\begin{aligned}
& c \\
& a \\
& a, e \\
& e \\
& e \\
& a, c, e \\
& c \\
& a, d, e \\
& a, e \\
& a, e \\
& a, c \\
& f
\end{aligned}
$$
\] <br>

\hline \[
$$
\begin{gathered}
\text { SW- } \\
11
\end{gathered}
$$

\] \& | EPSCO |
| :--- |
| R \& S |
| Texscan |
| Telonic |
| Kay |
| Kruse-Storke |
| Servo |
| Micro-Power |
| Telonic |
| Micro-Power | \& | SG-132-A |
| :--- |
| SWOB I |
| HS-80 |
| SH-1/SM-2000 |
| P867 |
| 5009/5000 |
| Q880 |
| H25MD/220 |
| S-4/SM-2000 |
| H37MD/220 | \& \[

$$
\begin{aligned}
& 15 \\
& 0.5 \\
& 200 \\
& 0.5 \\
& 220 \\
& 250 \\
& 250 \\
& 250 \\
& 250 \\
& 150 \\
& 350
\end{aligned}
$$
\] \& 400

400
425
460
470
500
500
500
500
700 \& $0.1 \%$
200
$0.1 \%$
200
20
0
0
0
$.02 \%$

0 \& \begin{tabular}{l}
$\pm 20 \%$ <br>
50 <br>
15\% <br>
200 <br>
30 <br>
full rng <br>
full rng <br>
full rng 10\% <br>
full rng

 \& 

25 <br>
60 <br>
50/60 <br>
50/60 <br>
0.2-30 <br>
$.01-100 \mathrm{sec}$ <br>
.01-100 <br>
.01-100 sec <br>
50/60 <br>
$.01-100 \mathrm{sec}$

\end{tabular} \& \[

$$
\begin{aligned}
& 0.15 \\
& 0.4 \\
& 4 \mathrm{~W} \\
& 0.35 \\
& 0.5 \\
& .02 \mathrm{~W} \\
& \\
& 0.4 \mathrm{~W} \\
& .05 \mathrm{~W} \\
& 1 \\
& 0.1 \mathrm{~W}
\end{aligned}
$$

\] \& | 50 |
| :--- |
| 50,75 |
| ina |
| 50 |
| 50 |
| ina |
| ina |
| ina |
| 50 |
| ina | \& $C$

$C$
$C$
$C, R$
$C, R$
$C, R$
$C, R$
$C, R$
$C, R$
$C, R$

$C$ \& | 2440 |
| :--- |
| 3100 |
| 2500 |
| 1175 |
| 200(12) |
| 2740 |
| 3400 |
| 3550 |
| 1125 |
| 3650 | \& \[

\left\{$$
\begin{array}{l}
c \\
a, f \\
a, e \\
a, b, c, f \\
a \\
f \\
f, f \\
f
\end{array}
$$\right.
\] <br>

\hline \[
$$
\begin{aligned}
& \text { SW- } \\
& 12
\end{aligned}
$$

\] \& | Grundig |
| :--- |
| Blonder-Tongue |
| Blonder-Tongue |
| Tel-Inst |
| Telonic |
| Telonic |
| Texscan |
| Texscan |
| Telonic |
| Kay | \& | WS-3 |
| :--- |
| 4122 |
| 4114 |
| 1211 |
| HD-IA $\begin{aligned} & \text { S-5/SM-2000 } \\ & \text { CS-77 } \\ & \text { CS-76A } \\ & \text { SD-3 } \\ & 111 \end{aligned}$ | \& 4

10
5
550
45
1
460
460
460
440

10 \& $$
\begin{aligned}
& 800 \\
& 890 \\
& 890 \\
& 900 \\
& 900 \\
& 920 \\
& 920 \\
& 920 \\
& 920 \\
& 950
\end{aligned}
$$ \& 0

0000
5000
50,000
200

$.02 \%$
460 MHz
100
$.02 \%$

50 \& $$
\begin{array}{|l}
\hline 30 \\
420 \\
420 \\
50 \\
200 \\
10 \% \\
460 \\
45 \\
10 \% \\
40
\end{array}
$$ \& \[

$$
\begin{aligned}
& 50 \\
& 60 \\
& 60 \\
& \text { ina } \\
& 60 \\
& 50 / 60 \\
& 50 / 60 \\
& 50 / 60 \\
& 60 \\
& 60
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.5 \\
& 0.5 \\
& 0.1 \\
& 1 \\
& 0.75 \\
& 1 \\
& 0.5 \\
& 0.5 \\
& 0.75 \\
& 0.15
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 60 \\
& 75 \\
& 75 \\
& 75 \\
& 50 \\
& \\
& 50 \\
& 50 \\
& 50 \\
& 50 \\
& 70
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& C \\
& c \\
& c \\
& c \\
& C, R \\
& C, R \\
& C, R \\
& C \\
& C \\
& C, R \\
& C, R
\end{aligned}
$$
\] \& 595

request
request
1100
995
1125
440
525
745

625 \& $$
\begin{aligned}
& a \\
& a \\
& a \\
& a \\
& a \\
& a, f \\
& c \\
& c \\
& c \\
& a \\
& a, e
\end{aligned}
$$ <br>

\hline
\end{tabular}

Notes, abbreviations and manufacturers' index at end of this section.

## Sweep generators $950-4000 \mathrm{MHz}$

|  | Manufacturer | Model | FREQUENCY |  | SWEEP WIDTH |  |  | OUTPUT |  | Type | Price \$ | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. MHz | Max. <br> MHz | Min. <br> kHz | Max. <br> MHz | Rate <br> Sec | Watts | Imp. <br> Ohms |  |  |  |
| $\begin{gathered} \text { SW- } \\ 13 \end{gathered}$ | Kay | $110$ | . 05 | 950 |  | 40 | 60 Hz | 0.5V | 50 | C,R | 625 |  |
|  | Telonic | 3005/SM-2000 | 460 | 960 | $5000$ | 500 | . $01-100 \mathrm{~Hz}$ | 0.3V | $50$ | C,R | 1525 |  |
|  | Kay | 1483A | 440 | 960 | 5000 | 520 | $10-30 \mathrm{~Hz}$ | 0.5 V | 50 | C,R | 495 |  |
|  | Kruse-Storke | 5010/5000 | 500 | 1000 | 0 | full rng | .01-100 | . 02 | ina | C,R | 2740 | $a, b, c, f$ |
|  | Servo | P880 | 500 | 1000 |  | full rng | . $01-100 \mathrm{~Hz}$ | 0.4 | ina | C,R | 3400 | $a$ |
|  | Micro-Power | H51MD/220 | 500 | 1000 | 0 | full rng | . $01-100$ | 0.1 | ina | C | 3550 | , |
|  | Telonic | VR-50M/SM-2000 | 500 | 1000 | 5000 | 500 | . $01-100 \mathrm{~Hz}$ | 0.3 V | 50 | C,R | 1725 | f |
|  | Texscan | HS-85 | 400 | 1000 | 0.1\% | 15\% | $50 / 60 \mathrm{~Hz}$ | 4 | ina | C,R | 2500 | c |
|  | Telonic | PD-8 | 375 | 1000 | 0.2\% | 15\% | $50 / 60 \mathrm{~Hz}$ | 14 V | 50 | C,R | 2500 |  |
|  | Texscan | VS-70 | 275 | 1000 | 50 | 40\% | $5-60 \mathrm{~Hz}$ | 0.5 V | 50 | C, R |  |  |
| SW-14 | Kay | P123 | 100 | 1000 | 0.2\% | full ring | ina | 0.5 V | 50 | C,R |  |  |
|  | Kay | 100 | . 05 | 1000 | 50 | 40 | 60 Hz | 0.5 V | 50 | C,R | $575$ | a,e |
|  | Kay | P121/121 | 0.5 | 1050 | 50 | 350 | $10-60 \mathrm{~Hz}$ | 0.5V | $50$ | C,R | 1390 | f |
|  | Jerrold | $890$ | 0.5 | 1100 | 100 | 200 | 60 Hz | 0.25 V | $50,75$ | C,R | 845 | $a, b$ |
|  | Telonic | S-6/SM-2000 | 600 | 1200 | .02\% | 8\% | $50 / 60 \mathrm{~Hz}$ | 0.75 V | 50 | C,R | 1125 | $a, f$ |
|  | R \& S | SWLU | 400 | 1200 | 0 | 170 | 60 Hz | 3 V | 50,60 | C | 1690 |  |
|  | Micro-Power | H41MD/220 | 400 | 1200 | 0 | full rng | . $01-100$ | . 02 | ina | C | 4050 | f |
|  | Jerrold | $900-\mathrm{C}$ | 0.5 | 1200 | $10$ |  | 60 Hz | 0.25 V | 50 | C,R | 2180 | $a, b$ |
|  | Jerrold | $900-\mathrm{A}$ | $0.5$ | $1200$ | $500$ | $400$ | $60 \mathrm{~Hz}$ | $0.25 \mathrm{~V}$ | 50 | C,R |  | $a, b$ |
|  | Texscan |  |  |  |  | 300 | $5-60 \mathrm{~Hz}$ | 0.5 V |  | $C, R$ |  |  |
| SW-15 | R \& S | SWOB II | 0.5 | 1200 | 200 | 50 | 60 Hz | 0.4 V | 50,75 | C | 4200 |  |
|  | Kay | P122/121 | 900 | 1300 | 200 | full rng | $10-60 \mathrm{~Hz}$ | 0.5 V | 50 | C,R | 1270 | e,f |
|  | Kay | P124/121 | 1300 | 1700 | 500 | full rng | $10-60 \mathrm{~Hz}$ | 0.5 V | 50 | C,R | 1290 | a,e |
|  | Kay | 121 | 0.5 | 1700 | $50$ | 500 | $10-60 \mathrm{~Hz}$ | $0.5 \mathrm{~V}$ | 50 | C,R | 895 | a,e |
|  | Telonic | E-1/SM-2000 | 460 | 1840 | .02\% | 10\% | $50 / 60 \mathrm{~Hz}$ | 0.25-1V | 50 | $C, R$ | 1575 | a,f |
|  | Alfred |  | $1000$ | $2000$ | 0 | full rng | .01-100 | . $08{ }^{(6)}$ |  | C,R | 3350 |  |
|  | Alfred | $651 \mathrm{~K} / 650$ | $1000$ | $2000$ | 0 | full rng | . $01-100$ | . 07 (6) | $50$ | $C, R$ | 3600 | $c, f$ |
|  | Alfred | 651 AK/650 | $1000$ | $2000$ | 0 | full rng | . $01-100$ | .06(5) | $50$ | C,R | $3850$ | $c, f$ |
|  | Alfred Alfred | $631 \mathrm{~A}$ | $\begin{aligned} & 1000 \\ & 1000 \end{aligned}$ | $\begin{aligned} & 2000 \\ & 2000 \end{aligned}$ | 0 | full rng | . $01-100$ | $.05$ | ina | $C, R$ | $3490$ | c |
|  |  |  |  |  |  | full rng | . $01-100$ |  |  | C,R |  |  |
| SW-16 | Alfred | $641$ $641 \mathrm{~K}$ |  |  |  |  |  |  | 50 50 |  | $3050$ |  |
|  | Alfred | 641K <br> 6021 | $\begin{aligned} & 1000 \\ & 1000 \end{aligned}$ | $\begin{aligned} & 2000 \\ & 2000 \end{aligned}$ | 0 | full rng | . $01-100$ | .07(4) | 50 | C,R | $3325$ | c |
|  | Alfred | $6021$ | 1000 | 2000 | 0 | full rng | .01-100 |  | 50 | C | 6350 | a |
|  | E-H H-P | $\begin{aligned} & 571 \\ & 8691 \mathrm{~A} / 8690 \mathrm{~A} \end{aligned}$ | $\begin{aligned} & 1000 \\ & 1000 \end{aligned}$ | 2000 | 0 | full rng | note 1 | 0.12 | 50 | R | 3660 |  |
|  | H-P | 8691A/8690A | 1000 | 2000 | 0 | full rng | .01-100 | 0.1 | 50 | C, R | 3450 | f |
|  | H-P | 8691B/8690A | 1000 | 2000 | 0 | full rng | .01-100 |  | 50 |  |  |  |
|  | Kruse-Storke | $5011 / 5000$ | 1000 | 2000 | 0 | full rng | . $01-100$ | . 01 | ina | C, R | 3080 | $a, b, c, f$ |
|  | LFE | 832-L-1 | 1000 | 2000 | 1000 | full rng | .01-100 | .08-0.15 | 50 | C, R | request |  |
|  | Micro-Power | H102L/220 |  | $2000$ |  | full rng | . $01-100$ |  | ina | C |  | f |
|  | MSI | N900L |  |  |  | full rng | ina | 0.1 | 50 | R |  |  |
| SW-17 |  |  |  |  |  | full rng | 10 Hz | $25-30 \mathrm{dBm}$ | 50 |  | 9600 |  |
|  | Servo | L880 | 1000 | 2000 | 0 | full rng | . $01-100 \mathrm{~Hz}$ | 0.1 | ina | C, R | 3190 | a |
|  | Texscan | VS-120 | 1000 | 2300 | $50$ | $25 \%$ | $5-60 \mathrm{~Hz}$ | $0.5 \mathrm{~V}$ | 50 | $C, R$ | 1695 | c |
|  | Kruse-Storke | $5012 / 5000$ | 1400 | $2400$ | $0$ | full rng | $.01-100$ | $.005$ | ina | $C, R$ | $3080$ | $a, b, c, f$ |
|  | Telonic | E-2/SM-2000 | 600 | 2400 | .02\% | 10\% | $50 / 60 \mathrm{~Hz}$ | 0.25-1V | 50. | $C, R$ | 1770 | $a, f$ |
|  | Alfred | 631A-51 | 1400 | 2500 | 0 | full rng | . $01-100$ | . 05 | 50 | C,R | 3790 | $a, c$ |
|  | Alfred | $631 \mathrm{D}-\mathrm{S1}$ | 1400 | 2500 | 0 | full rng | . $01-100$ | $.07$ | 50 | C,R | 3990 | $a, c$ |
|  | Alfred | $641 \mathrm{~K}-\mathrm{Sl}$ | 1400 | 2500 | 0 | full rng | $.01-100$ | $.07(4)$ | 50 | C,R | $3600$ |  |
|  | Alfred | $641-S 1$ $651 A-S 1 / 650$ | $1400$ | 2500 | 0 | full rng | $.01-100$ | $.08^{(2)}$ | $50$ | $C, R$ | $3300$ | c |
|  | Alfred | 651A-S1/650 |  |  |  | full rng | .01-100 | . 06 (5) | 50 | C,R |  |  |
| $\begin{gathered} \text { SW- } \\ 18 \end{gathered}$ | Alfred |  |  |  | $0$ |  |  |  | $50$ |  | $4175$ |  |
|  | Alfred | $651 \mathrm{~K}-\mathrm{S} 1 / 650$ | $1400$ | $2500$ | $0$ | full rng | $.01-100$ | $.07(6)$ | $50$ | $C, R$ | $3900$ | $c, f$ |
|  | Alfred | 651-S1/650 | 1400 | 2500 | 0 | full rng | . $01-100$ | $.08(6)$ | 50 | $C, R$ | 3600 | c, f |
|  | Micro-Power | H142L/220 | 1400 | 2500 | $0$ | full rng | .01-100 | $0.1$ | ina | C | $4050$ | f |
|  | Telonic | E-3/SM-2000 | 550 | 3000 | .02\% |  | $50 / 60 \mathrm{~Hz}$ | $0.2-0.75 \mathrm{~V}$ | 50 | $C, R$ | 1770 | $a, f$ |
|  | R \& S | SMC | 1600 | 3200 | 0 | full rng | 10 Hz | $22-30 \mathrm{dBm}$ | 50 |  | $9000$ |  |
|  | Alfred | 632 D | 2000 | 4000 | 0 | full rng | . $01-100$ | $.02$ | 50 | C,R | 3490 | $a, c$ |
|  | Alfred | 632A | 2000 | 4000 | 0 | full rng | . $01-100$ | $.04$ | ina | $C, R$ | 3290 | a |
|  | Alfred | 652AK/650 | 2000 | 4000 | 0 | full rng | . $01-100$ | $.04(5)$ | 50 | $C, R$ | 3680 | $c, f$ |
|  | Alfred | $652 \mathrm{~A} / 650$ | 2000 | 4000 | 0 | full rng | . $01-100$ | .04(5) | 50 | $C, R$ | 3400 | c, f |

Notes, abbreviations and manufacturers' index at end of this section.

Sweep generators $4000-8300 \mathrm{MHz}$

|  | Manufacturer | Model | FREQUENCY |  | SWEEP WIDTH |  |  | OUTPUT |  | Type | Price \$ | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. MHz | Max. MHz | Min. <br> kHz | Max. MHz | Rate Sec | Watts | Imp. Ohms |  |  |  |
| $\begin{gathered} \text { SW- } \\ 19 \end{gathered}$ | Alfred | $652 \mathrm{~K} / 650$ | 2000 | 4000 | 0 | full rng | . $01-100$ | . $05{ }^{(6)}$ | 50 | C,R | 3425 |  |
|  | Alfred | 642 K | 2000 | 4000 | 0 | full rng | . $01-100$ | . $05{ }^{(4)}$ | 50 | C,R | 3140 | c |
|  | Alfred | 642 | 2000 | 4000 | 0 | full rng | . $01-100$ | . 06 (2) | 50 | C,R | 2850 | c |
|  | Alfred | 652/650 | 2000 | 4000 | 0 | full ring | . $01-100$ | . 06 (6) | 50 | C,R | 3150 | c, f |
|  | Alfred | 6022 | 2000 | 4000 | 0 | full rng | . $01-100$ | I | 50 | C | 6890 | a |
|  | E-H | 572 | 2000 | 4000 | 0 | full ring |  |  | 50 | R |  |  |
|  | H-P | 8692B/8690A | 2000 | 4000 | 0 | full rng | . $01-100$ | . 04 | 50 | C,R | $3550$ | f |
|  | H-P | 8692A/8690A | 2000 | 4000 | 0 | full rng | .01-100 | . 07 | 50 | $C, R$ | 3250 | f |
|  | LFE | 832-S-1 | 2000 | 4000 | 1 MHz | full rng | .01-100 | .04-0.15 | $50$ | C,R | request |  |
|  |  | N900S |  |  |  | full rng |  |  |  |  | $1995$ |  |
| $\begin{gathered} \text { SW- } \\ 20 \end{gathered}$ | Micro-Power | H204L/220 | 2000 | 4000 | 0 | full rng | .01-100 | . 08 | ina | C | 3550 | f |
|  | Narda | 64 S 2 | 2000 | 4000 | 0 | full rng | . $01-100$ | . 048 | ina | C,R | 3250 |  |
|  | Narda | 6451 | 2000 | 4000 | 0 | full rng | .01-100 | . 05 | ina | C,R | 2750 |  |
|  | Servo | 5880 | 2000 | 4000 | 0 | full rng | . $01-100 \mathrm{~Hz}$ | . 07 | ina | C,R | 2990 | a |
|  | Weinschel | S775A | 2000 | 4000 | 0.2 MHz | full rng | note 19 | . 07 | 50 | $C, R$ | 2750 |  |
|  | Alfred | 652K-S5/650 | 1700 | 4200 | 0 | full rng | . $01-100$ | . 03 (5) | ina | C,R | 3825 | c,f |
|  | Alfred | $642 \mathrm{~K}-\mathrm{Sl}$ | 1700 | 4200 | 0 | full rng | . $01-100$ | . 03 | ina | C,R | 3150 | a,c |
|  | Alfred | 652-S5/650 | 1700 | 4200 | 0 | full rng | .01-100 | . 035 (6) | ina | C,R | 3475 | c,f |
|  | Alfred | $642-51$ | 1700 | 4200 | 0 | full rng | .01-100 | $.035$ | ina | C,R | 3300 | a,c |
|  | Alfred | 652A-S5/650 |  |  | 0 | full rng | .01-100 | . 015 (6) |  | C,R |  | c,f |
| $\begin{gathered} \text { SW- } \\ 21 \end{gathered}$ | Alfred H-P | 652AK-S5/650 H01-8692B/8690A | 1700 | 4200 | 0 | full rng | . $01-100$ | . 015 (5) | ina | C, R | 4075 | c,f |
|  | H-P Micro- | H01-8692B/8690A H204LA/220 | 1700 1700 | 4200 | 0 | full rng | . $01-100$ | . 015 | 50 | C,R | 3850 |  |
|  | Servo | R880 | 1700 | 4200 | 0 | full rng | . $01-100 \mathrm{~Hz}$ | . 02 | ina | C.R | 38290 |  |
|  | $R$ \& S | SMC | 2400 | 4700 | 0 | full mg | 10 Hz | 20-30 dBm | 50 | $\mathrm{C}^{\text {, }}$ | 9000 |  |
|  | Servo | T880 | 2400 | 5300 | 0 | full rng | . $01-100 \mathrm{~Hz}$ | . 05 | ina | C,R | 3250 | a |
|  | Polarad | 1307 | 5500 | 6600 | 0 | 40 | $50-60 \mathrm{~Hz}$ | note 10 | 50 | C,R | 2650 | c |
|  | Polarad | 1307-P | 5500 (11) | 6600 | 0 | 40 | $50-60 \mathrm{~Hz}$ | note 10 | 50 | C, R | 2800 | c |
|  | Alfred Alfred | $633 A-S 1$ $653 A-S 1 / 650$ | 3500 3500 | 6750 6750 | 0 | full rng | . $01-100$ | ו0. | 50 | C,R | $3850$ | $a, c$ |
|  | Alfred | 653A-S1/650 |  | 6750 | 0 | full rng | . $01-100$ | . 02 (5) |  | $C, R$ |  | c, f |
| $\begin{gathered} \text { SW- } \\ 22 \end{gathered}$ | Alfred | $653 \mathrm{AK}-\mathrm{S} 1 / 650$ |  |  |  | full rng |  |  |  |  |  |  |
|  | Alfred | $643 \mathrm{~K}-\mathrm{S1}$ | $3500$ | 6750 | 0 | full rng | .01-100 | $.03(4)$ $.03(6)$ | 50 | C,R | 3800 |  |
|  | Alfred | 653K-S1/650 | 3500 | 6750 | 0 | full rng | .01-100 | .03(6) | 50 | C,R | 4050 | c, f |
|  | Alfred | $653-$ S1/650 $643-\mathrm{S} 1$ | 3500 | 6750 | 0 | full rng | . $01-100$ | . 04 (6) | 50 | C,R | 3540 | c, f |
|  | Alfred | $643-\mathrm{Sl}$ | 3500 | 6750 | 0 | full rng | .01-100 | .04(2) | 50 | $C, R$ | 3290 | c |
|  | Alfred | 633D-S1 | 3500 | 6750 | 0 | full rng | . $01-100$ | $.008$ | 50 | C,R | 4100 | $a, c$ |
|  | Micro-Power | H356L/220 | 3500 | 6750 | 0 | full rng | . $101-100$ | $.04$ | ina | C | 4000 | f |
|  | R \& S | SMC | 3600 | 7100 | 0 | full rng | 10 Hz | $15-25 \mathrm{dBm}$ | 50 | C | 9000 |  |
|  | Polarad | $1307-1$ | $5200$ | 7200 | 0 |  | $50-60 \mathrm{~Hz}$ | note 10 | 50 | C,R | 2300 | c |
|  | Polarad | 1307-1P | $5200{ }^{(11)}$ | 7200 | 0 |  | $50-60 \mathrm{~Hz}$ | note 10 | 50 | $C, R$ | 2450 | c |
| $\begin{gathered} \text { SW- } \\ 23 \end{gathered}$ |  |  |  |  |  |  |  |  |  |  | 2650 | c |
|  | Polarad | 1308-P | $7100(11)$ | $7800$ | $0$ | $40$ | $50-60 \mathrm{~Hz}$ | note 10 | $50$ | C,R | 2800 |  |
|  | Alfred | 633A | $4000$ | 8000 | 0 | full rng | . $01-100$ | . 02 | ina | C,R | 3390 | a |
|  | Alfred | 653A/650 | $4000$ | 8000 | 0 | full rng | . $01-100$ | .02(5) | 50 | C,R | 3350 | $c, f$ |
|  | Alfred | 653AK/650 | $4000$ | 8000 | 0 | full rng | .01-100 | .02(5) | 50 | $C, R$ | 3700 | $c, f$ |
|  | Alfred | 643K | 4000 | 8000 | 0 | full rng | .01-100 | . $025{ }^{(4)}$ | 50 | C,R | 3230 | c |
|  | Alfred | 653K/650 | 4000 | 8000 | 0 | full rng | . $01-100$ | . 025 (6) | 50 | C,R | 3450 | c, f |
|  | Alfred | $643$ | $4000$ | 8000 | 0 | full rng | . $01-100$ | .03(4) | 50 | C,R | 2850 | c |
|  | Alfred | $653 / 650$ | $4000$ | $8000$ | $0$ | full rng | .01-100 | $.03(6)$ | 50 | $C, R$ | $3100$ | c, f |
|  | Alfred |  |  | 8000 | 0 | full rng | . $01-100$ | 0.5 | 50 | C |  |  |
| $\begin{gathered} \text { SW- } \\ 24 \end{gathered}$ | Alfred | 633D | 4000 | 8000 | 0 | full rng |  | . 008 | 50 | C,R | 3650 | c |
|  | E-H | 573 | 4000 | 8000 | 0 | full rng | note 1 | . 035 | 50 | R | 3460 |  |
|  | H-P | 8693A/8690A | 4000 | 8000 | 0 | full rng | . $01-100$ | . 03 | 50 | C,R | 3125 | f |
|  | H-P | 8693B/8690A | 4000 | 8000 | $0$ | full rng | . $01-100$ | $.015$ | 50 | C,R | $3450$ | f |
|  | LFE | 832-C-1 | 4000 | 8000 | 1 MHz | full rng | .01-100 | .02-0.15 | 50 | C,R | request |  |
|  | MSI | N900C | 4000 | 8000 | 0 | full rng | ina | . 025 | 50 | R | 1995 |  |
|  | Micro-Power | H408L/220 | 4000 | 8000 | 0 | full rng | .01-100 | . 03 | ina | C, R | 3550 | f |
|  | Servo | C880 | 4000 | 8000 | $0$ | full rng | . $01-100 \mathrm{~Hz}$ | $.02$ | ina | C,R | 2975 | a |
|  | Weinschel | C775A | 4000 | 8000 | 0.2 MHz | full rng | note 20 | . 02 | 50 | C,R | 2800 |  |
|  | Alfred | 653A-S2/650 | 3700 | 8300 |  | full rng | . $01-100$ | . $005{ }^{(6)}$ | ina | C, R | 3650 | c, f |

Notes, abbreviations and manufacturers' index at end of this section.

## Sweep generators $8300-18,000 \mathrm{MHz}$

|  | Manufacturer | Model | FREQU | UENCY |  | SWEEP W | DTH | OUT |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. <br> MHz | Max. <br> MHz | Min. kHz | Max. <br> MHz | Rate Sec | Watts | Imp. <br> Ohms | Type | Price \$ | Notes |
| $\begin{gathered} \text { SW- } \\ 25 \end{gathered}$ | Alfred | 653AK-S2/650 | 3700 | 8300 | 0 | full rng | . $01-100$ | .005(5) | ina | C, R | 4000 | c, f |
|  | Alfred | 643-S2 | 3700 | 8300 | 0 | full rng | . $01-100$ | . $01{ }^{(2)}$ | ina | C,R | 3150 | a,c |
|  | Alfred | 643K-S2 | 3700 | 8300 | 0 | full ring | . $01-100$ | . $01{ }^{(4)}$ | ina | C,R | 3530 | a,c |
|  | Alfred | 653-S2/650 | 3700 | 8300 | 0 | full rng | . $01-100$ | . $011^{(6)}$ | ina | C, R | 3400 | c,f |
|  | Alfred | $653 \mathrm{~K}-\mathrm{S} 2 / 650$ | 3700 | 8300 | 0 | full ring | . $01-100$ | . $01{ }^{(5)}$ | ina | $C, R$ | 3775 | c,f |
|  | H-P | H01-8693B/8690A | 3700 | 8300 | 0 | full rng | . $01-100$ | . 005 | 50 | C, R | 3750 | f |
|  | Micro-Power | H408LA/220 | 3700 | 8300 | 0 | full rng | . $01-100$ | . 015 | ina | C | 3900 | f |
|  | Servo | W880 | $3700$ | 8300 | 0 | full rng | . $01-100 \mathrm{~Hz}$ | . 005 | ina | $C, R$ | 3275 | a |
|  | Polarad | 1308-1 | $7100$ | 8500 | 0 | 40 | $50-60 \mathrm{~Hz}$ | note 10 | 50 | C,R | 2450 | c |
|  | Polarad | 1308-1P | 7100 (11) | 8500 | 0 | 40 | $50-60 \mathrm{~Hz}$ | note 10 | 50 | $C, R$ | 2600 | c |
| $\begin{gathered} \text { SW- } \\ 26 \end{gathered}$ | R \& S | SMC | 4800 | 9600 | 0 | full rng | 10 | $15-25 \mathrm{dBm}$ | 50 | C | 9000 |  |
|  | Servo | J880 | 5300 | 10,000 | 0 | full rng | . $01-100 \mathrm{~Hz}$ | . 01 | ina | C, R | 3450 | a |
|  | Alfred | 634A | 7000 | 11,000 | 0 | full ring | . $01-100$ | . 006 | ina | C,R | 3650 | c |
|  | Alfred | 654A/650 | 7000 | 11,000 | 0 | full rng | . $01-100$ | . $011^{(6)}$ | 50 | C,R | $3450$ | $c, f$ |
|  | Alfred | 654AK/650 | 7000 | 11,000 | 0 | full ring | . $01-100$ | . $01{ }^{(5)}$ | 50 | $C, R$ | 3850 | c, f |
|  | Alfred | 644K | 7000 | 11,000 | 0 | full rng | . $01-100$ | . $015{ }^{(4)}$ | 50 | C,R | 3300 | c |
|  | Alfred | 654K/650 | 7000 | 11,000 | 0 | full ring | . $01-100$ | . 015 (6) | 50 | $C, R$ | 3425 | c, f |
|  | Alfred | 644 | 7000 | 11,000 | 0 | full rng | . $01-100$ | . $02{ }^{(2)}$ | 50 | C,R | 2900 | c |
|  | Alfred | 654/650 | $7000$ | $11,000$ | 0 | full rng | . $01-100$ | $.02{ }^{\text {(6) }}$ | 50 | C,R | 3150 | c, f |
|  | Alfred |  |  |  | 0 | full rng | . $01-100$ |  |  |  |  |  |
| SW-27 | H-P | H02-8694A/8690A | 7000 | 11,000 | 0 | full rng | . $01-100$ | . 025 | 50 | C,R | request | $f$ |
|  | $\mathrm{H}-\mathrm{P}$ | H02-8694B/8690A | 7000 | 11,000 | 0 | full rng | . $01-100$ | . 015 | 50 | $C, R$ | 3500 | $f$ |
|  | MSI | N 900 H | 7000 | 11,000 | 0 | full ring | ina | . 025 | 50 | R | 1995 |  |
|  | Micro-Power | H711L/220 | 7000 | 11,000 | 0 | full rng | . $01-100$ | . 025 | ina | C | 3750 | f |
|  | Alfred | 6025 | 8000 | 12,000 | 0 | full rng | . $01-100$ | 1 | 50 | C | 8190 |  |
|  | E-H | 574-1 | 7000 | 12,000 | 0 | full rng | note 1 | . 03 | 50 | R | 3760 |  |
|  | Weincshel | X775A | 8200 | 12,400 | 0 | full rng | note 21 | . 02 | 50 | C, R | 2900 |  |
|  | E-H | 574-2 | 8200 | 12,400 | 0 | full ring | note 1 | . 024 | 50 | R | 3580 |  |
|  | MSI | N900X | $8200$ | 12,400 | 0 | full rng | ina | $.025$ | 50 |  | $1995$ |  |
|  | Alfred | 635A |  | 12,400 | 0 | full rng | .01-100 |  |  | C, R |  | a |
| $\begin{aligned} & \text { SW- } \\ & 28 \end{aligned}$ | Alfred | 655A/650 | 8000 | 12,400 | 0 | full rng | . $01-100$ | . 02 (5) | 50 | C,R | 3375 | c, f |
|  | Alfred | 655AK/650 | 8000 | 12,400 | 0 | full rng | . $01-100$ | . $02{ }^{(4)}$ | 50 | C,R | 3750 | c, f |
|  | Alfred | 645 K | 8000 | 12,400 | 0 | full rng | . $01-100$ | .05(4) | 50 | C,R | 3300 |  |
|  | Alfred | $655 \mathrm{~K} / 650$ | 8000 | 12,400 | 0 | full rng | . $01-100$ | .05(6) | 50 | C,R | 3500 | c, f |
|  | Alfred | $645$ | 8000 | 12,400 | 0 | full rng | . $01-100$ | . $06{ }^{(2)}$ | 50 | $C, R$ | 2900 | c |
|  | Alfred | 655/650 | 8000 | 12,400 | 0 | full rng | . $01-100$ | . $06{ }^{(6)}$ | 50 | C,R | 3100 | c,f |
|  | H-P | 8694A/8690 A | 8000 | 12,400 | 0 | full rng | . $01-100$ | . 05 | 50 | C,R | 3125 | $f$ |
|  | H-P | 8694B/8690A | 8000 | 12,400 | 0 | full rng | . $01-100$ | $.03$ | 50 | C,R | 3475 | f |
|  | LFE | $832-X-1$ H812L/220 | 8000 8000 | 12,400 12,400 | $1 \mathrm{MHz}$ | full rng full rng | $.01-100$ $.01-100$ | $\begin{aligned} & .05-0.15 \\ & .05 \end{aligned}$ | ina ina | $C, R$ $C$ | $\begin{aligned} & \text { request } \\ & 3600 \end{aligned}$ |  |
|  | Micro-Power | H812L/220 | 8000 | 12,400 |  | full rng | .01-100 |  |  |  |  | f |
| $\begin{gathered} \text { SW- } \\ 29 \end{gathered}$ | Servo | X880 $654 \mathrm{~A}-51 / 650$ |  |  |  |  | . $01-100 \mathrm{~Hz}$ |  | ina | C,R | 3050 |  |
|  | Alfred | 654A-SI/650 | 7000 | 12,400 | 0 | full rng | . $01-100$ | $.01(5)$ $.01(5)$ | 50 50 | C,R | 3600 | c, f |
|  | Alfred | $654 \mathrm{AK}-\mathrm{SI} / 650$ $644 \mathrm{~K}-\mathrm{SI}$ | 7000 | 12,400 12,400 | 0 | full rng | . $101-100$ | $\begin{aligned} & .01(5) \\ & .015(4) \end{aligned}$ | ina | C,R C, R | 4000 3500 | c,f a,c |
|  | Alfred | $654 \mathrm{~K}-\mathrm{SI} / 650$ | 7000 | 12,400 | 0 | full rng | . $01-100$ | . $015{ }^{(6)}$ | 50 | C,R | 3700 | c, f |
|  | Alfred | 644-S1 | 7000 | 12,400 | 0 | full rng | . $01-100$ | . $02(2)$ | ina | C,R | $3100$ | $a, c$ |
|  | Alfred | 654-S1/650 | 7000 | 12,400 | 0 | full rng | .01-100 | . 02 (6) | 50 | C,R | 3300 | c, f |
|  | H-P | H01-8694A/8690A | 7000 | 12,400 | 0 | full rng | . $01-100$ | $.025$ | 50 | C,R | request | $f$ |
|  | H-P | $\mathrm{H} 01-8694 \mathrm{~B} / 8690 \mathrm{~A}$ N 900 HX | 7000 | $\begin{aligned} & 12,400 \\ & 12400 \end{aligned}$ | 0 | full rng | .01-100 | $\begin{aligned} & .015 \\ & .015 \end{aligned}$ | $\begin{aligned} & 50 \\ & 50 \end{aligned}$ | $\begin{aligned} & C, R \\ & R \end{aligned}$ | $\begin{aligned} & 3750 \\ & 1995 \end{aligned}$ | f |
|  | MSI | N900HX | 7000 | 12,400 | 0 | full rng | ina | . 015 | 50 | R | 1995 |  |
| $\begin{gathered} 5 W- \\ 30 \end{gathered}$ | Micro-Power | H712L/220 | 7000 | 12,400 | 0 | full ring | $.01-100$ | $.025$ | ina | C |  |  |
|  | Servo | H880 | 7000 | 12,400 | 0 | full rng | . $01-100 \mathrm{~Hz}$ | . 01 (6) | ina | C, R | 3375 | a |
|  | Alfred | 646 | 10,000 | 15,500 | 0 | full ring | $.01-100$ | . 035 (6) | 50 | C,R | 3450 | c |
|  | Alfred | 656/650 | 10,000 | 15,500 | 0 | full ring | . $01-100$ | . $035{ }^{(6)}$ | 50 | $C, R$ | $3450$ | c, f |
|  | Alfred | 637 A | 12,400 | 18,000 | 0 | full rng | . $01-100$ | . 01 | ina | C,R | 3790 | a |
|  | Alfred | 647K | 12,400 | 18,000 | 0 | full rng | . $01-100$ |  | ina | C, R | 3500 | $a, c$ |
|  | Alfred | 657K/650 | 12,400 | 18,000 | 0 | full rng | . $01-100$ | . 025 (5) | ina | C, R | 3725 | c,f |
|  | Alfred | 647 | 12,400 | 18,000 | 0 | full rng | . $01-100$ | . $04{ }^{(6)}$ | 50 | C, R | 3000 | c |
|  | Alfred | 657/650 | 12,400 | 18,000 | 0 | full rng | . $01-100$ | . $04{ }^{(6)}$ | 50 | C, R | 3200 | c, f |
|  | E-H | 575 | 12,400 | 18,000 | 0 | full ring | note 1 | . 048 | 50 | R | 3730 |  |

Notes, abbreviations and manufacturers' index at end of this section.


## 

The benefits of swept frequency measurement in terms of quicker testing and more precise answers easily justifies the employment of a Sweep Generator in both lab and production applications. Now, Telonic's SM-2000


Sweep Generator (left) offers these benefits in a configuration that gives the instrument maximum versatility at a low equipment investment. The SM-2000 accepts
the 19 different oscillators, shown above, ranging from the

LA-1M that covers 20 Hz to 20 KHz to the E-3 that goes to 3120 MHz . The entire spectrum from DC to 3 Gc can be viewed with as much detail as needed. In some cases a whole octave may be displayed on the scope at one time.
The SM-2000 Sweep Generator provides the method, the machinery, and the flexibility for a myriad of frequency measurement applications. Your local Telonic representative would be glad to
 show you how.

Does your work involve application or manufacture of Power Supplies, Oscillators, RF Circuits, Audio Amplifiers, UHF Tuners, Communication Networks, Crystal Devices, R.F. Filters or the like? Then find out how you can apply swept frequency methods to make your work easier, and more reliable. Telonic Application Techniques cover all these and more. Yours on request


## Sweep generators $18,000-40,000 \mathrm{MHz}$

|  | Manufacturer | Model | FREQUENCY |  | SWEEP WIDTH |  |  | OUTPUT |  | Type | Price \$ | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Min. MHz | Max. <br> MHz | Min. kHz | Max. <br> MHz | Rate Sec | Watts | Imp. Ohms |  |  |  |
| $\begin{gathered} \text { SW- } \\ 31 \end{gathered}$ | H-P | 8695A | 12,400 | 18,000 | 0 | full rng | .01-100 | . 04 | 50 | C, R | 3250 |  |
|  | LFE | 832-KU-1 | 12,400 | 18,000 | 1 Mhz | full rng | . $01-100$ | .04-0.2 | ina | C, R | request |  |
|  | Micro-Power | H1218/220 | 12,400 | 18,000 | 0 | full rng | .01-100 | . 04 | ina | C | 3650 | $f$ |
|  | Servo | U880 | 12,400 | 18,000 | 0 | full rng | . $01-100 \mathrm{~Hz}$ | . 003 | ina | $C, R$ | 4100 | a |
|  | Weinschel | Y775A | 12,400 | 18,000 | 0.2 MHz | full rng | note 22 | . 01 | 50 | $C, R$ | 3300 |  |
|  | Servo | Y880 | 10,000 | 20,000 | 0 | full rng | . $01-100 \mathrm{~Hz}$ | . 003 | ina | C, R | 4100 | a |
|  | H-P | 8696A | 18,000 | 26,000 | 0 | full ring | . $01-100$ | . 01 | 50 | C, R | 4050 |  |
|  | Alfred | 658/650 | 18,000 | 26,500 | 0 | full rng | . $01-100$ | . 01 (6) | 50 | C,R | 3950 | c, f |
|  | Alfred | 648 | 18,000 | 26,500 | 0 | full rng | . $01-100$ | . 02 (6) | 50 | C, R | 3650 | , |
|  | E-H | 576 | 18,000 | 26,500 | 0 | full rng | note 1 | . 012 | WG | R | 4570 |  |
| $\begin{gathered} \text { SW- } \\ 32 \end{gathered}$ | Micro-Power | H1826/220 | 18,000 | 26,500 | 0 | full rng | . $01-100$ | . 02 |  |  | 4500 | f |
|  | Servo | K880 | 18,000 | 26,500 | 0 | full rng | . $01-100 \mathrm{~Hz}$ | . 005 | ina | $C, R$ | 4500 | a |
|  | Weinschel | U775A | 27,000 | 40,000 | 0.2 MHz | full rng | note 23 | . 0035 | ina | C,R | 4300 |  |
|  | Alfred | 659/650 | 26,500 | 40,000 | 0 | full rng | . $01-100$ | . $005{ }^{(6)}$ | 50 | C,R | 5650 | c, f |
|  | Alfred | 649 | 26,500 | 40,000 | 0 | full rng | . $01-100$ | .005(6) | 50 | $C, R$ | 5300 | c |
|  | E-H | 577 | 26,500 | 40,000 | 0 | full rng | note 1 | . 006 | WG | R | 6870 |  |
|  | Servo | V880 | 26,500 | 40,000 | 0 | full rng | . $01-100 \mathrm{~Hz}$ | . 005 | ina | $C, R$ | 6350 | a |
|  | Micro-Power | H2640/220 | 26,500 | 40,000 | 0 | full rng | . $01-100$ | . 005 | ina | C | 6400 | f |
|  | H-P | 8697A | 26,000 | 40,000 | 0 | full rng | . $01-100$ | . 005 | 50 | $C, R$ | 5850 |  |

Notes, abbreviations and manufacturers' index at end of this section.

## NOTES

## Sweep Generators

a. Zero or blanking output available for scope return trace.
b. Has phasing control of scope output.
c. Input: $115 / 230 \mathrm{~V}, 50-400 \mathrm{~Hz}$.
d. Has switched fixed markers
e. Locks to line frequency but may be adjusted to detect hum.
f. Prices shown are for tuning unit and basic oscillator. The basic oscillator can be used with any of this series of tuning heads.

1. Sweep rate $.001-1000$ seconds.
2. Output unleveled.
3. RF channels adjustable from $5-20 \mathrm{MHz}$, IF channels adjustable from $10-40 \%$ of center frequency.
4. Output leveled or unleveled.
5. Pin diode leveled.
6. Grid leveled.
7. Fixed, $1.67,5$ and 10 kHz .
8. Adjustable $7^{\circ}$ to $320^{\circ}$.
9. Adjustable $2.3^{\circ}$ to $600^{\circ}$ per minute.
10. +3 to -127 dBm .
11. Can measure microwave power from an external source. The rear tuning shaft extension provides programable motor drive.
12. Prices shown are for tuning unit. This tuning unit can be used with model 1500 at $\$ 650$ extra or the model 860 at $\$ 495$ extra.
13. 500 kHz for sound $\mathrm{IF}, 13 \mathrm{MHz}$ for picture.
14. Center frequencies and sweep widths covered by each band;
Band A - $100 \mathrm{kHz}-12 \mathrm{MHz}$, width 100 kHz 12 MHz .

Band B - 12-20 MHz, width $60 \%$ of center frequency.
Band C - $20-32 \mathrm{MHz}$, width $60 \%$ of center frequency.
Band D - 32-52 MHz, width 15 MHz .
Band E $-52-90 \mathrm{MHz}$, width 20 MHz .
Band F $-90-150 \mathrm{MHz}$, width 20 MHz .
15. Center frequencies and sweep widths covered by each band;
Band A - $100 \mathrm{kHz}-12 \mathrm{MHz}$, width 100 kHz 12 MHz .
Band $B-20-30 \mathrm{MHz}$, width $60 \%$ of center frequency.
Band C - 35-55 MHz, width $60 \%$ of center frequency.
Band D - 55-215 MHz, width $20-50 \mathrm{MHz}$ at high end of band.
16. Wide band 6 times marker spread, narrow band 3 times marker spread.
17. Prices shown are for tuning unit. This tuning unit can be used with model 1500 at $\$ 525$ extra or model 121 at $\$ 895$ extra.
18. Model H07-207A sweep motor drive provides full band sweep speeds of $430( \pm 10 \%)$ or $43( \pm 10 \%)$ seconds.
19. Sweep rate $0.1-100 \mathrm{GHz}$.
20. Sweep rate $0.2-200 \mathrm{GHz}$.
21. Sweep rate $300 \mathrm{MHz}-300 \mathrm{GHz}$.
22. Sweep rate $0.4-400 \mathrm{GHz}$.
23. Sweep rate $0.1-1000 \mathrm{GHz}$.

## ABBREVIATIONS

C - Cabinet
R - Rack mount
ina - information not available
rng - range


## New Continuously Tunable 1 to 40 GHz Synchronizer-Model 136A

FEL's new 136A Synchronizer converts any voltage tunable signal source from 1 to 40 GHz to an ultra stable signal source with stability of 1 part in $10^{7}$ per day and 1 part in $10^{8}$ per second. It extends the capability of your existing signal generator!

Simplified tuning makes the all solid state Model 136A easy to operate. It's continuously tunable over entire range with crystal controlled stability . . . controls any voltage tunable tube or solid state oscillator . . . and has a lock-on indicator lamp. Balance meter and signal level meter are included. New proportional controlled oven provides exceptional short and long term stability.


Typical spectrum generated by an rf source with and without stabilization, using the FEL-136A. Note simultaneous frequency stabilization and incidental fm reduction in right hand photograph.

Expansion has created opportunities for qualified Microwave, Circuit Design and Instrumentation Engineers in Key Positions on our Technical Staff. Send complete resume in confidence to: Supervisor, Professional Employment.


OTHER FEL SERIES 130 SYNCHRONIZERS:

| Model | Frequency Range (GHz) | Price |
| :---: | :---: | :---: |
| 133A. | 1.0-12.4 | \$2250 |
| 134A | .. 12.4-18.0 | \$2350 |
| 135A | 18.0-40.0 | \$3450 |
| 137A | 1.0-18.0 | \$2750 |

Data subject to change without notice; Prices f.o.b. factory.

For complete information on the new 136A or any 130 Series Synchronizer, write or call your local FEL field engineering office today or: FREQUENCY ENGINEERING LABORATORIES, P. 0. Box 527, Farmingdale, New Jersey 07727, (201) 938-9221. TWX: 201-9382456.


FREQUENCY ENGINEERING
LABORATORIES

## Fast Recovery!

New, LEL IF Amplifiers, ITA-34, have $0.2 \mu \mathrm{sec}$. recovery time and excellent pulse response. Ideal for a wide variety of microwave receiving system applications, they also feature high dynamic range and furnish both IF and detected outputs.


## SPECIFICATIONS

| C.F. | 30 or 60 MHz |
| :---: | :---: |
| BW | 3 or 8 MHz |
| Recovery Time | $0.2 \mu \mathrm{sec}$. (typ.) |
| IF Gain |  |
| (into $50 \Omega$ ) | 75 dB (min.) |
| Video Gain |  |
| (into 1000 ) | 80 dB (min.) |
| Input | 50 ohms |
| Input (lin operation) |  |
| (lin. operation) | -15 dBM (max.) |
| Output |  |
| (lin. operation) | +10 dBM (max.) |
| External AGC range | 50 dB (min.) |
| N.F. | 7 dB (max.) |
| Weight | 20 oz. |
| Dimensions | $67 / 8^{\prime \prime} \times 11 / 8^{\prime \prime} \times 3^{\prime \prime}$ |
| Connectors |  |
| (IF and Video) | BNC |
| (Power) | DA 15 |
| Power required | -20 VDC @ 70 mA |
| Temperature | $-55^{\circ}$ to $+70^{\circ} \mathrm{C}$ |
| Price | \$325 |


(ONE WEEK)
More than 100 other standard IF Amplifiers are available many with such special characteristics as broad bandwidth, gain-and-phase-match, low noise, extremely low power drain.

Send now for complete data book including full specifications and performance curves.

VARIAN associato:

Index of Manufacturers and Model Numbers
(keyed to table locator symbols)

| INDEX |  | 654A/650 | (SW-26) |
| :---: | :---: | :---: | :---: |
|  |  | 654A-S1/650 | (SW-29) |
| Advanced Measurement |  | 654AK/650 | (SW-26) |
| Instruments, Inc (AMI) |  | 654AK-S1/650 | (SW-29) |
| 301 | (SW-7) | $654 \mathrm{~K} / 650$ | (SW-26) |
| 320 | ( $5 W-8$ ) | $654 \mathrm{~K}-51 / 650$ | (SW-29) |
| 321 | (SW-1) | 654-S1/650 | (SW-29) |
| 321 | (SW-1) | 655/650 | (SW-28) |
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| 631 D | (SW-15) | 657/650 | (SW-30) |
| $631 \mathrm{D}-51$ | (SW-17) | $657 \mathrm{~K} / 650$ | (SW-30) |
| 632A | (SW-18) | 658/650 | (SW-31) |
| 632D | (SW-18) | 659/650 | (SW-32) |
| 633A | (SW-23) | 6021 | (SW-16) |
| 633A-S1 | (SW-21) | 6022 | (SW-19) |
| 633D | (SW-24) | 6023 | (SW-23) |
| 633D-S1 | (SW-22) | 6024 | (SW-26) |
| 634A | (SW-26) | 6025 | (SW-27) |
| 635A | (SW-27) | Blonder-Tongue |  |
| 637A | (SW-30) |  | Labs, Inc |
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| 641 K | (SW-16) | 4122 | (SW-12) |
| $641 \mathrm{~K}-\mathrm{Sl}$ | (SW-17) |  |  |
| 641-S1 | (SW-17) | Clough-Brengle Co |  |
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| 642K | ( $5 W-19)$ | 182-A | (SW-1) |
| $642 \mathrm{~K}-\mathrm{Sl}$ | (SW-20) | $282-A$ | (SW-2) |
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| 648 | (SW-31) |  |  |
| 649 | (SW-32) | 360 |  |
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| $651 \mathrm{~K} / 650$ | (SW-15) | EPSCO, Inc |  |
| 651-S1/650 | (SW-18) |  |  |
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| 651AK-S1/650 | (SW-18) |  |  |
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| 652/650 | (SW-19) |  |  |  |
| 652-55/650 | (SW-20) | ST-4A | (SW-9) |
| 652A/650 | (SW-18) |  |  |
| 652A-S5/650 | (SW-20) | General Radio Co (Gen Radio) |  |
| $652 \mathrm{AK} / 650$ | (SW-18) |  |  |  |
| 652AK-S5/650 | (SW-21) |  |  |
| $652 \mathrm{~K} / 650$ | (SW-19) | 1025-A | (SW-9) |
| 652K-S5/650 | (SW-20) |  |  |
| 653/650 | (SW-23) | Grundig |  |
| 653-51/650 | (SW-22) |  |  |
| 653-S2/650 | (SW-25) | WS3 | (SW-12) |
| 653A/650 | (SW-23) |  |  |
| 653A-S1/650 | (SW-21) | Heath Co |  |
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| 653AK/650 | (SW-23) | $\begin{aligned} & \text { FMO-1 } \\ & \text { IG-52 } \end{aligned}$ | (SW-6) |
| 653AK-S1/650 | (SW-22) |  | (SW-8) |
| 653AK-S2/650 | (SW-25) |  |  |
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| 653K-S2/650 | (SW-25) | 207A | (SW-2) |
| 654/650 | (SW-26) | 3211A | (SW-6) |



## No, it's not a microwave sweep oscillator. It's the only microwave sweep signal generator!

Here, in one compact package, is the microwave industry's only electronic Sweep Signal Generator. Alfred's new 630D Series now provides precise frequency tuning plus known absolute power output over a 60 db range, calibrated in dbm, all during swept or CW operation. Note these special features:
Flat Output-Feedback leveler holds power variation to less than $\pm 0.5 \mathrm{db}$ at rated output over each range. Variation in any 100 Mc range is less than $\pm 0.1 \mathrm{db}$. Absolute accuracy $\pm 3 / 4 \mathrm{db}$ at rated power output.
Multiple Frequency Markers allow frequency calibration with 3 markers during broadband sweep and 2 during symmetrical sweep.
Complete Sweep Flexibility $-F_{1} \rightarrow F_{2}$ sweep for broadband evaluation. $F_{0} \pm \Delta \mathrm{F}$ symmetrical sweep for expanded display.
Separate $F_{0}$ Control independent of $F_{1} \rightarrow F_{2}$ allows switching from broadband sweep to symmetrical sweep without "disadjusting controls."
Transistorized-10 $1 / 2^{\prime \prime}$ panel height-lightweight-low power consumption-only five vacuum tubes used.
Stabilized Power Output-Dual bolometers assure con-
"Project responsibility opportunities exist for qualified engineers on our technical staff. An equal opportunity employer."
stant power output over wide temperature range.
Available in Five Bands-1 to 2, 1.4 to 2.5, 2 to $4,3.5$ to 6.75 and 4 to 8 Gc . Frequency is continuously adjustable over entire range with direct calibrated dial (1\% accuracy).
Coverage to $\mathbf{1 8} \mathbf{G c}$-Series 630A provide calibrated level output without the attenuator through 18 Gc in 9 bands.

## KEY SPECIFICATIONS

Frequency Range: Model 631D, 1 to 2 Gc; Model 631D-S1, 1.4 to 2.5 Gc ; Model 632D, 2 to 4 Gc ; Model 633D-S1, 3.5 to 6.75 Gc ; Model 633D, 4 to 8 Gc . RF Power: +10 to $-50 \mathrm{dbm}(+8$ to -45 dbm for 633D-S1 and 633D). Continuously variable over full range. Greater power output available unleveled. Residual FM: 50 kc peak ( 80 kc peak for 633D-S1 and 633D). Drift: $\pm 0.01 \%$. Sweep Width: Continuously adjustable from $2 \%$ to $100 \%$ of the frequency range. Symmetrical Sweep: 0 to $\pm 5 \%$ of range about any frequency. Sweep Time: 100 to 0.01 seconds. Amplitude Modulation: CW, square wave or external.

For complete information, write us at 3176 Porter Drive, Palo Alto, California. Phone: (415) 326-6496.

## NEW sweeper from WILTRON-50 kHz-100 MHz



An engineer's answer for:
Broadband system checking 50 kHz to 100 MHz in one sweep. All spurious and harmonics 30 db down.
Automatic test system with programming of center frequency, $\Delta \mathrm{f}$ and amplitude. Filter testing with 5 kHz stability.
Receiver testing with AM or FM modulation and with internal leveling.
Response curve plotting with 0.2 flat signal output.
Lossy device check with 1 volt rms output.
Price of Model 610B Main Frame, \$1,190;
Model 611B Plug-in shown above, 50 kHz to $100 \mathrm{MHz}, \$ 795$.



PRECISION POWER INVERTER 60 to 400 CPS, 115 VAC- 10 to 200 watts, accuracy to $.001 \%$. Power inverter employs precision Oscillator as a time base. Can be used to drive motors for clocks, tape decks, facsimile machines, etc.


## ECONOMY

 OSCILLATORModel T - gives long-term stability 800 to 7000 CPS. Priced singly from $\$ 29.00$ each. Measures $1^{\prime \prime} \times 1^{\prime \prime}$ $\times 21 / 4^{\prime \prime}$.

| OA | (SW-16) |
| :---: | :---: |
| 8691B/8690A | (SW-16) |
| 8692A/8690A | (SW-19) |
| 8692B/8690A | (SW-19) |
| H01-8692B/8690A | (SW-21) |
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| 8695A | (SW-31) |
| 8696A | (SW-31) |
| 8697A | (SW-32) |

Hickok Electrical Instrument Co

| 288 AX | $(\mathrm{SW}-7)$ |
| :--- | :--- |
| 615 | $(\mathrm{SW}-9)$ |

ITT Industrial Products Div
74217-A (SW-1)

| Jerrold Electronics Corp |  |
| :---: | :---: |
| 601-5B | (SW-9) |
| 602-5B | (SW-6) |
| 890 | (SW-14) |
| 900-A | (SW-14) |
| 900-C | (SW-14) |
| 1015 | ( $5 W-3$ ) |
| H-71/707C | (SW-6) |
| H-72/707C | (SW-7) |
| H-73/707C | (SW-4) |
| H-75/707C | (SW-8) |
| SS-300 | (SW-10) |

Kay Electric Co

| 100 | (SW-14) |
| :---: | :---: |
| 110 | (SW-13) |
| 111 | (SW-12) |
| 121 | (SW-15) |
| 141 | (SW-2) |
| 150B | (SW-4) |
| 154A | (SW-6) |
| 159B | (SW-10) |
| 361 C | (SW-8) |
| 370A | (5W-4) |
| 380A | (SW-5) |
| 385A | (SW-10) |
| 386 | ( $5 W-10$ ) |
| 386AN | (SW-10) |
| 386AR | (SW-5) |
| 865A | ( $5 W-7$ ) |
| 866A | (SW-7) |
| 932A | (SW-8) |
| 932B | (SW-7) |
| 935B | (SW-9) |
| 1483A | (SW-13) |
| P121/121 | (SW-14) |
| P122/121 | (SW-15) |
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| P141A | (SW-2) |
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| P152 | (SW-4) |
| P154 | (SW-7) |
| P855 | ( $5 W-4$ ) |
| P860 | (SW-8) |
| P867 | (SW-11) |

Kruse-Storke Electronics

| $5009 / 5000$ | $(5 W-11)$ |
| :--- | :--- |
| $5010 / 5000$ | $(\mathrm{SW}-13)$ |
| $5011 / 5000$ | $(\mathrm{SW}-16)$ |
| $5012 / 5000$ | $(\mathrm{SW}-17)$ |

LTV Ling Electronics

| $C O-10-A$ | $(S W-1)$ |
| :--- | :--- |
| $C O-10-B$ | $(S W-1)$ |

Laboratory For Electronics, Inc
(LFE)

| $832-\mathrm{C}-1$ | $(\mathrm{SW}-24)$ |
| :--- | :--- |
| $832-\mathrm{KU}-1$ | $(\mathrm{SW}-31)$ |
| $832-\mathrm{L}-1$ | $(\mathrm{SW}-16)$ |
| $832-\mathrm{S}-1$ | $(\mathrm{SW}-19)$ |
| $832-\mathrm{X}-1$ | $(\mathrm{SW}-28)$ |

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Micro-Power, Inc
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H25MD/220 (SW-11)
H37MD/220 (SW-11)
H41MD/220 (SW-14)
H51MD/220 (SW-13)
H102L/220 (SW-16)
H142L/220 (SW-18)
H204L/220 (SW-20)
$\begin{array}{ll}\text { H204LA/220 } & \text { (SW-21) } \\ \text { H356L/220 } & \text { (SW-22) }\end{array}$
$\begin{array}{ll}\text { H356L/220 } & \text { (SW-22) } \\ \text { H408L/220 } & \text { (SW-24) }\end{array}$
H408LA/220 (SW-25)
$\begin{array}{ll}\text { H71 1L/220 } & \text { (SW-27) } \\ \text { H712L/220 } & \text { (SW-30) }\end{array}$
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H1218/220 (SW-31)
H1826/220 (SW-32)
H2640/220 (SW-32)
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| N900C | $($ SW-24 $)$ |
| :--- | ---: |
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| (SW-20) |  |
| 64S2 | (SW-20) |

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| :---: | :---: |
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| 1307-P | (SW-21) |
| 1308 | (SW-23) |
| 1308-1 | (SW-25) |
| 1308-1P | (SW-25) |
| 1308-P | (SW-23) |
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| E410C | (SW-8) |
| Probescope Co |  |
| 5 | (SW-1) |
| 100 | (SW-2) |
| 500 | (SW-2) |

RCA, Electronic Components \& Devices
WR-69A (SW-5)
Rohde \& Schwarz Sales Co, Inc ( $\mathrm{R} \& \mathrm{~S}$ )

| SMC | $($ SW-17 $)$ |
| :--- | :--- |
| SMC | $($ SW-18 $)$ |
| SMC | $($ SW-21) |
| SMC | $(S W-22)$ |
| SMC | $(S W-26)$ |
| SWF | $(S W-9)$ |
| SWH | $(S W-3)$ |
| SWLU | $(S W-14)$ |
| SWOB I | $($ SW-11) |
| SWOB II | $($ SW-15 $)$ |
| SWOF | $(S W-4)$ |

Servo Corp of America

| C880 | $(S W-24)$ |
| :--- | :--- |
| H880 | $(S W-30)$ |
| J880 | $(S W-26)$ |
| K880 | $(S W-32)$ |
| L880 | $(S W-17)$ |
| P880 | $(S W-13)$ |

## Conceited

There's a simple explanation. The New Jerrold 900-C Sweep Signal Generator combines so many superb features in a single slim-line unit that it has literally become "King of The Hill".

Just look at some of the things you don't need with the 900-C.
. . . a high gain oscilloscope
... a variable attenuator
. . . a marker generator
... an external detector
All of these functions are built right into the new 900-C-the moneysaving, time-saving, space-saving champion. And it sports outstanding features like four mode operation and continuously variable sweep widths from 10 kHz to 400 MHz .
Whatever the unit under test - whatever the application - you're sure to find the Jerrold 900-C the most versatile, stable, easy-to-use sweep signal generator you have ever worked with.
No wonder it's conceited! Send for specs and we'll prove it.



You'll find the complete text applications information - theory technical data - specifying information for standard and custom delay lines for your application - in these authoritative LFE Catalog-Handbooks. Get them, now!


## ELECTRONICS DIVISION

Laboratory For Electronics, Inc. WALTHAM, MASSACHUSETTS 02154 Tel: 617-894-6600 - TWX: 710-324-0681


## Meet the DC voltage standard with:

## STABILITY WITHIN 15 PPM

... for 7 days, 25 ppm for 6 months.
Recorded stability history available.

## $0.003 \%$ ACEURAGY

...ensured by temperature-controlled precision Zener reference.

## IUMEDIATE DELIVERY

. . .t the COHU Model 326 is off-the-shelf. . . like the entire family of COHU DC voltage standards.
... and voltages from 0 to 1222.2221 in 3 ranges; steps as small as 1 Nv .

Price: $\$ 2490.00$ F.0.B. San Diego, additional export charge.

Box 623
San Diego, Calif. 92112
Phone 714-277-6700

## Oscillators $\quad .016-100 \mathrm{kHz}$

For information on how to use these tables, turn to page 2

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline \& \multirow[b]{2}{*}{Oscillators Manufacturer} \& \multirow[b]{2}{*}{Model} \& \multicolumn{4}{|c|}{FREQUENCY} \& \multirow[b]{2}{*}{Output Volts} \& \multirow[b]{2}{*}{\[
\begin{aligned}
\& \text { \# of } \\
\& \text { ranges }
\end{aligned}
\]} \& \multirow[b]{2}{*}{Type} \& \multirow[b]{2}{*}{\[
\begin{aligned}
\& \text { Price } \\
\& \$
\end{aligned}
\]} \& \multirow[b]{2}{*}{Notes} \\
\hline \& \& \& \[
\begin{aligned}
\& \mathrm{Min} \\
\& \mathrm{kHz}
\end{aligned}
\] \& Max kHz \& Acc \% \& Stability \% \& \& \& \& \& \\
\hline OS-1 \& \begin{tabular}{l}
Nav Comp Ind Test Equip Ind Test Equip Ind Test Equip Ind Test Equip \\
ITT \\
Weston ITT Gen Radio Ind Test Equip
\end{tabular} \& \[
\begin{array}{|l}
1350 B \\
600 \\
\text { OPS-100 } \\
\text { JF-400 } \\
1400 \\
74191-A \\
711 \text { A-1 } \\
74191-B \\
1214-A \\
1040
\end{array}
\] \& \[
\begin{aligned}
\& .001 \\
\& .06 \\
\& 0.4 \\
\& 0.4 \\
\& 0.4 \\
\& 0.8 \\
\& .80001 \\
\& 1 \\
\& 0.4 \\
\& 0.4
\end{aligned}
\] \& \[
\begin{aligned}
\& .016 \\
\& .06 \\
\& 0.4 \\
\& 0.4 \\
\& 0.4 \\
\& 0.8 \\
\& .999 \\
\& 1 \\
\& 1 \\
\& 1
\end{aligned}
\] \& \[
\begin{aligned}
\& \pm 0.2 \\
\& \pm .005 \\
\& \pm 0.1 \\
\& \pm 0.1 \\
\& \pm .005 \\
\& \pm 3 \\
\& 1 \\
\& \pm 3 \\
\& 2 \\
\& 0.2
\end{aligned}
\] \& \[
\begin{aligned}
\& 0.1 \\
\& 1 \\
\& \pm 0.1 \\
\& 1 \\
\& 1 \\
\& \text { ina } \\
\& \text { ina } \\
\& \text { ina } \\
\& \text { ina } \\
\& 0.2
\end{aligned}
\] \& \[
\begin{array}{|l}
4-12 \\
0-10 \\
115 \\
\text { ina } \\
0-10 \\
1 \mathrm{~mW} \\
1-50 \\
1 \mathrm{~mW} \\
200 \mathrm{~mW} \\
120(22)
\end{array}
\] \& \[
\begin{aligned}
\& 1 \\
\& 1 \\
\& 1 \\
\& 1 \\
\& 1 \\
\& 1 \\
\& 1 \\
\& 1 \\
\& 5 \\
\& 1 \\
\& 2 \\
\& 2
\end{aligned}
\] \& \(C, R\)
\(C\)
\(R\)
\(C\)
\(C\)
\(C\)
\(C\)
\(R\)
\(C\)
\(C\)
\(C\) \& \[
\begin{gathered}
2195 \\
459 \\
895 \\
140 \\
290 \\
110 \\
\text { request } \\
110 \\
95 \\
145
\end{gathered}
\] \& a \\
\hline OS-2 \& \begin{tabular}{l}
Gen Radio Ind Test Equip Krohn-Hite Gen Radio Krohn-Hite \\
R \& S \\
H-P \\
B \& K \\
S-A \\
Tech Materiel
\end{tabular} \& \[
\begin{aligned}
\& 1307-A \\
\& 1040-A \\
\& 440-\mathrm{B} \\
\& 1305-\mathrm{A} \\
\& 400-\mathrm{C} \\
\& \text { SRT } \\
\& 202-\mathrm{A} \\
\& 1017-\mathrm{A} \\
\& 2140 \\
\& \text { TTG-2 }
\end{aligned}
\] \& \begin{tabular}{l}
0.4 \\
0.4 \\
.001 \\
.00001 \\
.009 Hz \\
.00001 \\
. 008 Hz \\
. 002 \\
0.4 \\
0.935
\end{tabular} \& \[
\begin{array}{|l}
\hline 1 \\
1 \\
1 \\
1 \\
1.1 \\
1.11 \\
1.2 \\
2 \\
2.5 \\
2.805
\end{array}
\] \& \[
\begin{aligned}
\& 3 \\
\& 0.2 \\
\& \pm .05 \\
\& \pm 2 \\
\& \pm 2 \\
\& \pm 1 \\
\& \pm 1 \\
\& 2 \\
\& 1 \\
\& 3 \\
\& \text { ina }
\end{aligned}
\] \& \begin{tabular}{l}
ina \\
0.2 \\
. 005 \\
0.2 \\
1 \\
\(\pm 0.3\) \\
1 \\
0.8 Hz \\
\(\pm .05\) \\
ina
\end{tabular} \& \[
\begin{aligned}
\& 2 \\
\& 120(23) \\
\& 10 \\
\& 10 \\
\& 10 \\
\& 0.1-1 \\
\& 30 \\
\& 12.5 \\
\& 20 \\
\& 0.5
\end{aligned}
\] \& \[
\begin{aligned}
\& 2 \\
\& 2 \\
\& 2 \\
\& 6 \\
\& 5 \\
\& 3 \\
\& 3 \\
\& 5 \\
\& 2 \\
\& 1 \\
\& 2
\end{aligned}
\] \& \[
\begin{aligned}
\& C \\
\& C \\
\& C, R \\
\& R \\
\& R \\
\& C \\
\& C, R \\
\& C, R \\
\& R, R \\
\& R
\end{aligned}
\] \& \[
\begin{array}{r}
130 \\
220 \\
1150 \\
995 \\
465 \\
1640 \\
550 \\
1390 \\
350 \\
478
\end{array}
\] \&  \\
\hline OS-3 \& \begin{tabular}{l}
Waveforms \\
ITT \\
H-P \\
H-P \\
Gen Radio \\
Muirhead \\
Clough-Brengle \\
ITT \\
H-P \\
B \& K
\end{tabular} \& \begin{tabular}{l}
472C \\
74191-C \\
H48-241A \\
H30-241A \\
1311-A
\[
\begin{aligned}
\& \text { D-880-A/1 } \\
\& 179-A \\
\& 74186-C \\
\& 205 A G \\
\& 1024 A
\end{aligned}
\]
\end{tabular} \& 0.3
5
0.1
0.1
.05
.00001
.025
.03
.02
.02 \& \[
\begin{aligned}
\& 3 \\
\& 5 \\
\& 10(17) \\
\& 10(18) \\
\& 10 \\
\& 11.2 \\
\& 15 \\
\& 16 \\
\& 20 \\
\& 20
\end{aligned}
\] \& \[
\begin{aligned}
\& \pm 0.5 \\
\& \pm 3 \\
\& \pm 0.2 \\
\& \pm 0.2 \\
\& 1 \\
\& \pm 0.2 \\
\& 2 \\
\& \pm 1 \\
\& 2 \\
\& 1
\end{aligned}
\] \& \[
\begin{aligned}
\& .005 \\
\& \text { ina } \\
\& .04 \\
\& .04 \\
\& 0.1 \\
\& \\
\& .05 \\
\& \text { ina } \\
\& \text { ina } \\
\& 2 \\
\& 7 \mathrm{~Hz}
\end{aligned}
\] \& \[
\begin{array}{|l}
8 \\
1 \mathrm{~mW} \\
\text { note } 16 \\
\text { note } 16 \\
0-100 \\
10 \\
100 \mathrm{~mW} \\
-80 \mathrm{dBm} \\
5 \mathrm{~W} \\
12.5
\end{array}
\] \&  \& C
\(C\)
\(C\)
\(C\)
\(C\)
\(C, R\)
\(C\)
\(C\)
\(C\)
\(C, R\)
\(C, R\) \& \[
\begin{array}{r}
225 \\
110 \\
650 \\
675 \\
225 \\
\\
1450 \\
105 \\
1385 \\
600 \\
1720
\end{array}
\] \& a

a
e <br>

\hline OS-4 \& | H-P |
| :--- |
| B \& K |
| H-P |
| ITT |
| ITT |
| Gen Radio |
| Grundig |
| Marconi |
| Marconi |
| R\&S | \& \[

$$
\begin{aligned}
& 201 \mathrm{C} \\
& 1022 \\
& 206 \text { A } \\
& 74213-A \\
& 74233-B \\
& 1308-A \\
& 295 \\
& \text { TF2100 } \\
& \text { TF2000 } \\
& \text { SIT }
\end{aligned}
$$
\] \& .02

.02
.02
.02
.02
.02
.02
.02
.02

.02 \& $$
\begin{aligned}
& 20 \\
& 20 \\
& 20 \\
& 20 \\
& 20 \\
& 20 \\
& 20 \\
& 20 \\
& 20 \\
& 20
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& 1 \\
& 1 \\
& 2 \\
& \pm 2 \\
& \pm 1 \\
& \pm 3 \\
& 2 \\
& 2 \\
& \pm 1 \\
& \pm 1 \\
& 2
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 2 \\
& 8 \mathrm{~Hz} \\
& 2 \\
& \text { ina } \\
& \text { ina } \\
& \\
& .03 \\
& 0.5 \mathrm{~Hz} \\
& .003 \\
& .003 \\
& 4 \mathrm{~Hz}
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 42.5 \\
& 12.5 \\
& 10 \\
& -50 \mathrm{dBm} \\
& -40 \mathrm{dBm} \\
& 0-400 \\
& 8 \mathrm{~W} \\
& 8.5(8) \\
& 8.5 \\
& 1 \mathrm{~W}
\end{aligned}
$$

\] \& \[

\left\lvert\, $$
\begin{aligned}
& 1 \\
& 1 \\
& 7 \\
& 7
\end{aligned}
$$\right.
\] \& $C, R$

$C, R$
$C, R$
$C$
$C$
$C$
$C, R$
$C$
$C, R$
$C, R$

$C$ \& $$
\begin{array}{r}
250 \\
1150 \\
900 \\
690 \\
400 \\
1250 \\
260 \\
515 \\
925 \\
1400
\end{array}
$$ \&  <br>

\hline OS-5 \& | Marconi |
| :--- |
| Probescope |
| R\&S |
| Krohn-Hite |
| Krohn-Hite |
| Radiometer |
| Siemens |
| H-P |
| Gen Radio |
| Radiometer | \& \[

$$
\begin{aligned}
& \text { TF2005 } \\
& \text { SG-376/U } \\
& \text { SRN } \\
& 452 \\
& 450 \\
& \text { H032 } \\
& \text { W36 } \\
& \text { 200AB } \\
& \text { 1304-B } \\
& \text { H012 }
\end{aligned}
$$

\] \& \[

$$
\begin{array}{|l}
\hline .02(7) \\
.01 \\
.002 \mathrm{~Hz} \\
.001 \\
.0001 \\
0 \\
.03 \\
.03 \\
.03 \\
0
\end{array}
$$

\] \& \[

$$
\begin{aligned}
& 20 \\
& 20 \\
& 20 \\
& 20 \\
& 20 \\
& 21 \\
& 30 \\
& 40 \\
& 40 \\
& 40
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& \pm 1 \\
& \text { ina } \\
& 2 \\
& \pm .05 \\
& \pm .05 \\
& 2 \\
& \text { ina } \\
& 2 \\
& 1 \\
& 0.5
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& .003 \\
& \text { ina } \\
& \pm .01 \\
& .005 \\
& .005 \\
& \\
& 15 \mathrm{~Hz} \\
& 0.5 \\
& 2 \\
& \text { ina } \\
& 3 \mathrm{~Hz}
\end{aligned}
$$
\] \& 8.5

$2(7)$
$10 \mu \mathrm{~V}-30$
10
10
$300 \mu \mathrm{~V}-100$
$1 \mathrm{mV}-30$
24.5
$5 \mathrm{mV}-50$

$10 \mu \mathrm{~V}-50$ \& \[
$$
\begin{aligned}
& 7 \\
& 1 \\
& 4 \\
& 2 \\
& 2 \\
& 2 \\
& 1 \\
& 4 \\
& 4 \\
& 4 \\
& 2 \\
& 2
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& C, R \\
& C \\
& C \\
& C, R \\
& C, R \\
& C \\
& C \\
& C, R \\
& R \\
& C
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1415 \\
& \text { ina } \\
& 855 \\
& 1975 \\
& 1485 \\
& 449 \\
& 499 \\
& \text { ina } \\
& 170 \\
& 925 \\
& 1205
\end{aligned}
$$
\] \&  <br>

\hline OS-6 \& | Clough-Brengle |
| :--- |
| Clough-Brengle |
| Krohn-Hite |
| H-P |
| Krohn-Hite |
| Optimation |
| Optimation |
| Optimation |
| Optimation |
| B \& W | \& | 405 |
| :--- |
| 402 |
| 420-C |
| 203A |
| 4030 |
| RCD-1 |
| RCD-4 |
| ACl5 |
| RCD-2R |
| 210 | \& \[

$$
\begin{array}{|l}
.02 \\
.02 \\
.00035 \\
.005 \mathrm{~Hz} \\
.0001 \\
.0001 \\
.0001 \\
.0001 \\
.0001 \\
.01
\end{array}
$$

\] \& \[

$$
\begin{aligned}
& 50 \\
& 50 \\
& 52 \\
& 52 \\
& 60 \\
& 99.9 \\
& 99.9 \\
& 99.9 \\
& 99.9 \\
& 99.99 \\
& 100
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& \pm 1.5 \\
& \pm 1.5 \\
& \pm 2 \\
& \pm 1 \\
& 1 \\
& \pm 1 \\
& \pm 1 \\
& \pm 1 \\
& 1 \\
& \pm 0.1 \\
& \pm 2
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& \text { ina } \\
& \text { ina } \\
& 1 \\
& 1 \\
& \pm .02 \\
& .01 \\
& .01 \\
& .01 \\
& .01 \\
& \text { ina }
\end{aligned}
$$

\] \& \[

$$
\begin{array}{|l|}
100 \mathrm{~mW}(21) \\
100 \mathrm{~mW}(8) \\
10 \\
30 \\
10 \\
0-5(8) \\
0-5(11) \\
0-15 \\
0-5 \\
10
\end{array}
$$

\] \& \[

$$
\begin{aligned}
& 2 \\
& 2 \\
& 5 \\
& 7 \\
& 4 \\
& 4 \\
& 4 \\
& 4 \\
& 4 \\
& 4
\end{aligned}
$$
\] \& $C$

$C$
$C, R$
$C$
$C$
$R$
$C, R$
$C, R$
$R$
$R$

$C$ \& \[
$$
\begin{array}{r}
340 \\
340 \\
410 \\
1200 \\
\text { note } 6 \\
\\
625 \\
880 \\
1090 \\
795 \\
187
\end{array}
$$

\] \& | b,c b,e c,f, i |
| :--- |
| b |
| b |
| b |
| b | <br>

\hline
\end{tabular}

Notes, abbreviations and manufacturers' index at end of this section.

Oscillators $\quad 100-1000 \mathrm{kHz}$

|  | Oscillators . Manufacturer |  | FREQUENCY |  |  |  | Output Volts | \# of ranges | Type | Price \$ | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Model | Min <br> kHz | Max <br> kHz | Acc \% | Stability \% |  |  |  |  |  |
| OS-7 | Waveforms Gen Radio Heath Waveforms Waveforms | $\begin{aligned} & 401 \mathrm{C} \\ & 1309-A \\ & 1 G-72 \\ & 452 \\ & 471 B \end{aligned}$ | $\begin{aligned} & .01 \\ & .01 \\ & .01 \\ & .01 \\ & .01 \end{aligned}$ | $\begin{aligned} & 100 \\ & 100 \\ & 100 \\ & 100 \\ & 100 \end{aligned}$ | $\begin{aligned} & \pm 3 \\ & \pm 2 \\ & \pm 5 \\ & 1 \\ & 1 \end{aligned}$ | .005 <br> ina ina . 005 . 005 | $\begin{array}{\|l\|} \hline 20 \\ 5 \\ .003-10 \\ 8 \\ 10 \end{array}$ | $\begin{array}{\|l} \hline 4 \\ 4 \\ 8 \\ 4 \\ 4 \end{array}$ | $\begin{aligned} & C \\ & C \\ & C \\ & R \\ & C \end{aligned}$ | $\begin{aligned} & 200 \\ & 325 \\ & 42 \mathrm{kit}(2) \\ & 1000 \\ & 250 \end{aligned}$ | b |
|  | Waveforms IERC H-P <br> Holt <br> Waveforms | $\begin{aligned} & 401 B \\ & \text { ADO-102 } \\ & 202 C \\ & 448 \\ & 473 B \end{aligned}$ | $\begin{aligned} & .01 \\ & .01 \\ & .001 \\ & .001 \\ & .001 \end{aligned}$ | $\begin{aligned} & 100 \\ & 100 \\ & 100 \\ & 100 \\ & 100 \end{aligned}$ | $\begin{aligned} & \pm 3 \\ & \pm 1.5 \\ & 2 \\ & \pm 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & .005 \\ & \pm 1 \\ & 2 \\ & \pm 0.2 \\ & .005 \end{aligned}$ | $\begin{aligned} & 10 \\ & 0-50 \\ & 10 \\ & 10 \\ & 10 \end{aligned}$ | $\begin{aligned} & 4 \\ & 4 \\ & 5 \\ & 5 \\ & 5 \end{aligned}$ | C C,R C, R <br> R $C, R$ | $\begin{array}{r} 180 \\ 575 \\ 330 \\ 1540 \\ 410 \end{array}$ | c e c |
| OS-8 | Waveforms <br> Krohn-Hite <br> H-P <br> Krohn-Hite <br> Krohn-Hite | $\begin{aligned} & 403 \mathrm{~B} \\ & 4000 \\ & 3300 \mathrm{~A} / 3301 \mathrm{~A} \\ & 440-\mathrm{A} \\ & 4010 \end{aligned}$ | $\begin{aligned} & .001 \\ & .0001 \\ & .00001 \\ & .001 \mathrm{~Hz} \\ & .001 \mathrm{~Hz} \end{aligned}$ | $\begin{aligned} & 100 \\ & 100 \\ & 100 \\ & 100 \\ & 100 \end{aligned}$ | $\begin{aligned} & 3 \\ & 1 \\ & \pm 1 \\ & \pm 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & .005 \\ & \pm .02 \\ & \pm 0.25 \\ & .05 \\ & \pm .02 \end{aligned}$ | $\begin{aligned} & 10 \\ & 10 \\ & 35 \\ & 10 \\ & 10 \end{aligned}$ | $\begin{aligned} & 5 \\ & 3 \\ & 7 \\ & 5 \\ & 5(5) \end{aligned}$ | $\begin{aligned} & C, R \\ & C, R \\ & C \\ & C, R \\ & C, R \end{aligned}$ | $\begin{aligned} & 350 \\ & 850 \\ & 570 \\ & 625 \\ & 925 \end{aligned}$ | $\begin{aligned} & c \\ & f \\ & b, c \\ & c \end{aligned}$ |
|  | Krohn-Hite <br> Muirhead <br> Wayne Kerr <br> Probescope <br> B \& K | $\begin{aligned} & 4020 \\ & D-890-A / 1 \\ & S-121 \\ & R C-120 \\ & 1013 \end{aligned}$ | $\begin{aligned} & .001 \mathrm{~Hz} \\ & .001 \\ & .01 \\ & .009 \\ & 0.2 \end{aligned}$ | $\begin{aligned} & 100 \\ & 111.1 \\ & 120 \\ & 120 \\ & 200 \end{aligned}$ | $\begin{aligned} & 1 \\ & \pm 0.2 \\ & 1 \\ & \text { ina } \\ & 1 \end{aligned}$ | $\begin{aligned} & \pm .02 \\ & \pm .02 \\ & 100 \mathrm{ppm} \\ & \text { ina } \\ & 80 \mathrm{~Hz} \end{aligned}$ | $\begin{aligned} & 10 \\ & 2 \mathrm{~W} \\ & 0-30 \\ & 0-17(7) \\ & 12.5 \end{aligned}$ | $\begin{array}{\|l} 5(4) \\ 2 \\ 37 \\ 1 \\ 1 \end{array}$ | $\begin{aligned} & C, R \\ & C \\ & C \\ & C \\ & C, R \end{aligned}$ | $\begin{array}{r} 1025 \\ 1450 \\ 470 \\ \text { ina } \\ 1390 \end{array}$ | $\begin{aligned} & \mathrm{c} \\ & \mathrm{c} \end{aligned}$ |
| OS-9 | EICO <br> RCA <br> Hathaway <br> Muirhead <br> ITT | $\begin{aligned} & 377 \\ & \text { WA-44C } \\ & N-1 \\ & K-126-A \\ & 74254-A \end{aligned}$ | $\begin{aligned} & .02 \\ & .02 \\ & .002 \\ & .001 \\ & 0.3 \end{aligned}$ | $\begin{aligned} & 200 \\ & 200 \\ & 200 \\ & 222.2 \\ & 300 \end{aligned}$ | $\begin{aligned} & \pm 3 \\ & \pm 5 \\ & 2 \\ & \pm 0.4 \\ & \pm 1 \end{aligned}$ | ina <br> $\pm 2$ <br> ina <br> $\pm .02$ <br> ina | $\begin{aligned} & 10 \\ & 8 \\ & 1.5 \\ & 3 \\ & -49 \mathrm{dBim} \end{aligned}$ | $\begin{aligned} & 4 \\ & 4 \\ & 5 \\ & 4 \\ & 3 \end{aligned}$ | $C$ $C$ $C$ $C$ $C$ | $\begin{array}{r} 55 \\ 98 \\ 340 \\ 1055 \\ 700 \end{array}$ | $\begin{array}{\|l} \text { b } \\ \text { b } \\ \text { c } \\ \text { a } \end{array}$ |
|  | R \& S <br> Radiometer <br> Gen Radio <br> Waveforms <br> Krohn-Hite | SRM <br> RC03 <br> 1210C <br> 512F <br> $430-A B$ | $\begin{aligned} & .03 \\ & .03 \\ & .02 \\ & .0005 \\ & .0046 \end{aligned}$ | $\begin{aligned} & 300 \\ & 300 \\ & 500 \\ & 500 \\ & 520 \end{aligned}$ | $\begin{aligned} & 2 \\ & 1.5 \\ & 3 \\ & \pm 1 \\ & \pm 2 \end{aligned}$ | $\begin{aligned} & .01 \\ & \pm 0.5 \mathrm{~dB} \\ & 1 \\ & .01 \\ & 2 \end{aligned}$ | $\begin{aligned} & 1 \\ & 0-150 \\ & 7 \\ & 50 \\ & 10 \end{aligned}$ | $\begin{aligned} & 4 \\ & 4 \\ & 5 \\ & 6 \\ & 5 \end{aligned}$ | $\begin{aligned} & C \\ & C \\ & C \\ & C \\ & C, R \end{aligned}$ | $\begin{aligned} & 572 \\ & 591 \\ & 280 \\ & 475 \\ & 245 \end{aligned}$ |  |
| OS-10 | Marconi <br> H-P <br> Marconi <br> H-P <br> H-P | $\begin{aligned} & \text { TF2001 } \\ & \text { 236A } \\ & \text { TF2101 } \\ & \text { 204B } \\ & \text { 208A } \end{aligned}$ | $\begin{aligned} & .03 \\ & .05 \\ & .03 \\ & .005 \\ & .005 \end{aligned}$ | $\begin{aligned} & 560 \\ & 560 \\ & 560 \\ & 560 \\ & 560 \end{aligned}$ | $\begin{aligned} & \pm 3 \\ & \pm 3 \\ & \pm 3 \\ & \pm 3 \\ & \pm 3 \end{aligned}$ | $\begin{aligned} & .02 \\ & 0.1 \\ & .02 \\ & 0.3 \\ & 0.3 \end{aligned}$ | $\begin{array}{\|l} \hline 1.1(9) \\ +10 \mathrm{dBm} \\ 1.1(10) \\ 2.5 \\ 2.5 \end{array}$ | $\begin{aligned} & 6 \\ & 4 \\ & 6 \\ & 5 \\ & 5 \end{aligned}$ | $\begin{aligned} & C, R \\ & C \\ & C, R \\ & C \\ & C(19) \end{aligned}$ | $\begin{aligned} & 700 \\ & 525 \\ & 385 \\ & 315 \\ & 525 \end{aligned}$ | a ${ }^{\text {a,e }}$ |
|  | Stewart <br> H-P <br> H-P <br> Waveforms <br> Prec Apparatus | $\begin{aligned} & \text { TO } \\ & 200 \mathrm{CD} \\ & 200 \mathrm{~S} \\ & 401 \mathrm{H} \\ & \mathrm{E}-310 \end{aligned}$ | $\begin{aligned} & .0055 \\ & .005 \\ & .005 \\ & .005 \\ & .005 \end{aligned}$ | $\begin{aligned} & 600 \\ & 600 \\ & 600 \\ & 600 \\ & 600 \end{aligned}$ | $\begin{aligned} & 3 \\ & 2 \\ & \pm 2 \\ & \pm 2 \\ & \pm 1 \end{aligned}$ | 2 <br> 2 <br> ina <br> 0.1 <br> ina | $\begin{aligned} & 5,10 \\ & 10 \\ & 3 \\ & 10 \\ & 10 \end{aligned}$ | $\begin{aligned} & 11 \\ & 5 \\ & 5 \\ & 5 \\ & 5 \end{aligned}$ | $\begin{aligned} & C \\ & C, R \\ & C, R \\ & C \\ & C \end{aligned}$ | $\begin{aligned} & 270 \\ & 200 \\ & 230 \\ & 220 \\ & 200 \end{aligned}$ | $a$ $e$ $e$ |
| OS-11 | ITT <br> ITT <br> ITT <br> Prec Apparatus <br> Gen Radio <br> Hallicrafters <br> Hallicrafters <br> H-P <br> Century <br> Heath | $\begin{aligned} & 74188-D \\ & 74188-E \\ & 74188-F \\ & \text { E-330 } \\ & 1214-M \\ & \\ & \text { CFS-180A } \\ & \text { CFS-250A } \\ & 101 A \\ & 820 B \\ & \text { IG-82 } \end{aligned}$ | $\begin{aligned} & 4 \\ & 4 \\ & 4 \\ & .007 \\ & 1000 \\ & \\ & 100 \\ & 100 \\ & 100 \\ & 0.1 \\ & .02 \end{aligned}$ | $\begin{aligned} & 610 \\ & 610 \\ & 610(3) \\ & 750 \\ & 1000 \\ & \\ & 1000 \\ & 1000 \\ & 1000 \\ & 1000 \\ & 1000 \end{aligned}$ | $\begin{aligned} & \pm 1 \\ & \pm 1 \\ & \pm 1 \\ & \pm 5 \\ & 1 \\ & 2 / 10^{10} \\ & 5 / 10^{11} \\ & .05 \mathrm{ppm} \\ & .001 \\ & \pm 5 \end{aligned}$ | ina ina ina ina ina 2/1010 5/1011 .05 ppm 1 ppm ina | $\begin{aligned} & -80 \mathrm{dBm} \\ & -80 \mathrm{dBm} \\ & -80 \mathrm{dBm} \\ & 10 \\ & 300 \mathrm{~mW} \\ & \\ & 0.75 \\ & 1 \\ & 1 \\ & 0-1 \\ & .01-10 \end{aligned}$ | $\begin{aligned} & 2 \\ & 2 \\ & 2 \\ & 6 \\ & 1 \\ & 2(12) \\ & 2(12) \\ & 2(12) \\ & 2(12) \\ & 5 \\ & 5 \end{aligned}$ | C <br> C <br> C <br> C <br> C <br> C, R <br> C, R <br> C, R <br> R <br> C | 1235 <br> 1235 <br> 1235 <br> 130 <br> 95 <br> request <br> request <br> 600 <br> 3400 <br> 52 kit | a a $b, c$ b |
| OS-12 | Heath <br> Waveforms <br> Waveforms <br> Clough-Brengle <br> Clough-Brengle | $\begin{aligned} & \text { EUW-27 } \\ & 510 B \\ & 510 \mathrm{C} \\ & 411 \\ & 420 \end{aligned}$ | $\begin{aligned} & .02 \\ & .02 \\ & .02 \\ & .02 \\ & .02 \end{aligned}$ | $\begin{aligned} & 1000 \\ & 1000 \\ & 1000 \\ & 1000 \\ & 1000 \end{aligned}$ | $\begin{aligned} & \pm 5 \\ & \pm 3 \\ & \pm 3 \\ & 2 \\ & 2 \end{aligned}$ | ina 0.5 <br> 0.5 <br> ina <br> ina | $\begin{aligned} & .01-10 \\ & 10 \\ & 3 \\ & 10 \\ & 100 \mathrm{~mW} \end{aligned}$ | $\begin{aligned} & 5 \\ & 5 \\ & 5 \\ & 5 \\ & 5 \end{aligned}$ | $\begin{aligned} & C \\ & C \\ & C \\ & C \\ & C \end{aligned}$ | $\begin{aligned} & 94 \text { wired } \\ & 180 \\ & 200 \\ & 120 \\ & 200 \end{aligned}$ | b |
|  | $R \& S$ <br> H-P <br> H-P <br> Century <br> Siemens | $\begin{aligned} & \text { SRB } \\ & 241 \mathrm{~A} \\ & 100 \mathrm{E} \\ & 821 \mathrm{~B} \\ & \mathrm{~W} 38 \end{aligned}$ | $\begin{aligned} & .01 \\ & .01 \\ & .01 \\ & .01 \\ & .01 \end{aligned}$ | $\begin{aligned} & 1000 \\ & 1000 \\ & 1000 \\ & 1000 \\ & 1000 \end{aligned}$ | $\begin{aligned} & \pm 1 \\ & \pm 1 \\ & .05 \mathrm{ppm} \\ & .001 \\ & \text { ina } \end{aligned}$ | $\begin{aligned} & \pm .03 \\ & .04 \\ & .05 \mathrm{ppm} \\ & 1 \mathrm{ppm} \\ & 0.1 \end{aligned}$ | $\begin{aligned} & 1 \mathrm{mV}-30 \\ & 2.5 \\ & 5 \\ & 0-1 \\ & 20 \mu \mathrm{~V}-20 \end{aligned}$ | $\begin{aligned} & 5 \\ & \text { note } c \\ & 6(12) \\ & 5 \\ & 8 \end{aligned}$ | $\begin{aligned} & C \\ & C \\ & C, R \\ & R \\ & C \end{aligned}$ | $\begin{array}{r} 980 \\ 490 \\ 1000 \\ 3550 \\ 1950 \end{array}$ | $\begin{aligned} & e \\ & \text { h } \\ & \text { b,c } \end{aligned}$ |

Notes, abbreviations and manufacturers' index at end of this section.

Oscillators $1-920 \mathrm{MHz}$

|  | Oscillators Manufacturer | Model | FREQUENCY |  |  |  | Output Volts | \# of ranges | Type | $\underset{\$}{\text { Price }}$ | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \mathrm{Min} \\ & \mathrm{kHz} \end{aligned}$ | $\begin{aligned} & \text { Max } \\ & \mathrm{MHz} \end{aligned}$ | Acc \% | Stability \% |  |  |  |  |  |
| OS-13 | Waveforms <br> Hathaway <br> Waveforms <br> Muirhead <br> Century <br> Century <br> Century <br> H-P <br> Century <br> Schlumberger | $401 F$ <br> $\mathrm{N}-2 \mathrm{~A}$ <br> 471 F <br> K-205-A <br> 822B <br> 823B <br> 824B <br> 5102A <br> 825B <br> FS-1 | . 001 <br> .001 <br> . 001 <br> . 001 <br> . 001 <br> .0001 <br> .00001 <br> .00001 <br> . 001 Hz <br> 0 | $\begin{array}{\|l} 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1.2 \end{array}$ | $\pm 3$ 2 1 $\pm 1$ .001 .001 .01 $3 / 10^{9}$ .001 $1 / 10^{7}$ | 0.1 <br> ina <br> 0.1 <br> $\pm .01$ <br> 1 ppm <br> 1 ppm 1 ppm $3 / 10^{9}$ <br> 1 ppm <br> $3 / 10^{9}$ | $\begin{aligned} & 10 \\ & 0-10 \\ & 10 \\ & 3 \\ & 0-1 \\ & 0-1 \\ & 0-1 \\ & 1 \\ & 0-1 \\ & .05 \end{aligned}$ | $\begin{aligned} & 6 \\ & 6 \\ & 6 \\ & 6 \\ & 5 \\ & 5 \\ & 5 \\ & 5 \\ & 2 \\ & 5 \\ & 6 \end{aligned}$ | $\begin{aligned} & C \\ & C \\ & C \\ & C \\ & C \\ & R \\ & R \\ & R \\ & R, R \\ & R \\ & R \\ & C \end{aligned}$ | $\begin{array}{r} 325 \\ 350 \\ 385 \\ 670 \\ 3700 \\ 3850 \\ 4000 \\ 6500 \\ 4150 \\ 4250 \end{array}$ | $\begin{aligned} & b, c \\ & b, c \\ & b, c \\ & k \\ & b, c \end{aligned}$ |
| OS-14 | ITT <br> Waveforms <br> ITT <br> Gen Radio <br> Schlumberger <br> Tech Materiel <br> Tech Materiel <br> H-P <br> H-P <br> H-P | $\begin{aligned} & 74222-A \\ & 402 \mathrm{~A} \\ & 74308-\mathrm{A} \\ & 1310-\mathrm{A} \\ & \text { FS2 } \\ & \text { TTG-2 } \\ & \text { CPS-1 } \\ & 106 A \\ & 106 B \\ & 107 \mathrm{AR} \end{aligned}$ | 10 .01 0.3 . 002 <br> 0 <br> 1999 <br> 2000 <br> 100 <br> 100 <br> 100 | $\begin{aligned} & 1.5 \\ & 1.5 \\ & 1.62 \\ & 2 \\ & 2 \\ & 2.001 \\ & 2.001 \\ & 4 \\ & 5(13) \\ & 5(14) \\ & 5(13) \end{aligned}$ | $\begin{aligned} & \pm 0.1 \\ & \pm 2 \\ & .01 \\ & \pm 2 \\ & 1 / 10^{7} \\ & \text { ina } \\ & 1 / 10^{8} \\ & 5 / 10^{11} \\ & 5 / 1011 \\ & 5 / 1010 \end{aligned}$ | $\begin{aligned} & \pm 50 \mathrm{~Hz} \\ & 0.1 \\ & \pm 1.5 \mathrm{~Hz} \\ & 0.1 \\ & 3 / 10^{9} \\ & \text { ina } \\ & 1 / 108 \\ & 5 / 10^{11} \\ & 5 / 10^{11} \\ & 5 / 10^{10} \end{aligned}$ | -80 dBm 8 -70 dBm 20 .05 1 1 W 1 1 1 | $\begin{aligned} & 1 \\ & 5 \\ & 5 \\ & 6 \\ & 6 \\ & 2 \\ & 2 \\ & 1 \\ & 3(12) \\ & 3(12) \\ & 3(12) \end{aligned}$ | $C$ $C$ $C$ $C$ $C$ $C$ $R$ $C$ $C, R$ $C, R$ $C, R$ | 1715 450 2400 295 4400 478 request 3450 3900 2400 |  |
| OS-15 | H-P <br> Tech Materiel <br> Wayne Kerr <br> H-P <br> H-P <br> Marconi <br> R\&S <br> H-P <br> Waveforms <br> Measurements | 107BR <br> PMO-4 <br> O-22D <br> 651B <br> 652A <br> TF1370A <br> SBF <br> 5103A <br> 511A <br> 139 | 100 <br> 2000 <br> 10 <br> . 01 <br> . 01 <br> .01 <br> .01 <br> .0001 <br> 10 <br> 3000 | $5(14)$ 8 10 10 10 10 10 10 12 20 | $\begin{aligned} & 5 / 1010 \\ & 30 \mathrm{ppm} \\ & 1 \\ & \pm 2 \\ & \pm 2 \\ & \\ & \pm 2 \\ & \pm 2 \\ & 3 / 10^{9} \\ & 3 \\ & \pm 1 \end{aligned}$ | $\begin{aligned} & 5 / 10^{10} \\ & 20 \mathrm{ppm} \\ & \text { ina } \\ & .02 \\ & .02 \\ & \pm 0.1 \\ & \pm .01 \\ & \pm 10^{9} \\ & 3.005 \\ & \text { ina } \end{aligned}$ | $\begin{array}{\|l\|} \hline 1 \\ 2 \mathrm{~W} \\ \text { note } 1 \\ 3.16 \\ 3.16 \\ \\ 1 \mathrm{mV}-3 \\ 1 \mu \mathrm{~V}-10 \\ 1 \\ 3 \\ 0.5 \end{array}$ | $\begin{aligned} & \hline 3^{(12)} \\ & 1 \\ & 6 \\ & 6 \\ & 6 \\ & 6 \\ & 6 \\ & 8 \\ & 2 \\ & 6 \\ & 4 \end{aligned}$ | $\begin{aligned} & C, R \\ & C \\ & C, R \\ & C \\ & C(20) \\ & C, R \\ & C, R \\ & C, R \\ & C, R \\ & C \end{aligned}$ | 2750 <br> request <br> 780 <br> 590 <br> 725 <br> 995 <br> 1960 <br> 7100 <br> 700 <br> 165 |  |
| OS-16 | ITT <br> ITT <br> Tech Materiel Schlumberger <br> Tech Materiel <br> Hallicrafters <br> PRD <br> Microdot <br> Gen Radio <br> Schlumberger | $\begin{aligned} & \text { 74195-B } \\ & \text { 74306-A } \\ & \text { TRX-1 } \\ & \text { FS30 } \\ & \text { CPO-1A } \\ & \text { MHS-400 } \\ & \text { VHF9922 } \\ & \text { 404A } \\ & \text { 1211-C } \\ & \text { DO1001 } \end{aligned}$ | $\begin{aligned} & 50 \\ & 10 \\ & 540 \\ & 10 \\ & 1750 \\ & 2000 \\ & 30 \\ & 10,000 \\ & 500 \\ & 50 \end{aligned}$ | $\begin{array}{\|l} 20 \\ 20 \\ 32 \\ 32 \\ 33.75 \\ 34 \\ 40 \\ 50 \\ 50 \\ 50 \end{array}$ | $\begin{array}{\|l} \hline \pm 400 \mathrm{~Hz} \\ \pm 1 \\ \text { ina } \\ 1 / 10^{7} \\ \text { ina } \\ \\ \text { ina } \\ \text { ina } \\ \pm 1 \\ \pm 2 \\ 2 / 10^{8} \end{array}$ | $\pm 5$ <br> ina 1 ppm $3 / 10^{9}$ <br> 1 ppm <br> $1 / 10^{8}$ <br> ina <br> $\pm .002$ <br> 0.4 <br> $1 / 10^{9}$ | $\begin{aligned} & -80 \mathrm{dBm} \\ & -50 \mathrm{dBm} \\ & 1 \\ & 1.3 \\ & 1 \mathrm{~W} \\ & \\ & 0.1-2.5 \\ & 10 \\ & 50 \mathrm{~W} \\ & 1.5 \mathrm{~W} \\ & 1 \end{aligned}$ | $\begin{array}{\|l\|} \hline 1 \\ 8 \\ 10 \\ 6 \\ \text { ina } \\ 4 \\ 4 \\ 1 \\ 1 \\ 2 \\ 1 \end{array}$ | $\begin{aligned} & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{R} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C}, \mathrm{R} \\ & \mathrm{R} \\ & \mathrm{R} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | 5225 <br> 1095 <br> 560 <br> 4650 <br> request <br> request <br> request <br> 2975 <br> 415 <br> 5750 | k |
| OS-17 | Gen Radio H-P <br> Tech Materiel Jerrold <br> Tektronix <br> Microdot <br> Arenburg <br> Kay <br> Gen Radio <br> Weinschel | $\begin{aligned} & \text { 1330-A } \\ & 5100 \mathrm{~A} / 5110 \mathrm{~A} \\ & \text { VOX-5 } \\ & \text { CM-11 } \\ & 191 \\ & \text { 406A } \\ & \text { PG-650C } \\ & 990 \\ & 1215-C \\ & \text { MS-1 } \end{aligned}$ | 5 .00001 2000 10,000 50 50,000 12 4500 50,000 50,000 | $\begin{array}{\|l\|} \hline 50 \\ 50 \\ 64 \\ 100 \\ 100 \\ 200 \\ 210 \\ 220 \\ 250 \\ 250 \end{array}$ | $\begin{aligned} & \pm 5 \\ & 3 / 10^{9} \\ & \text { ina } \\ & .003 \\ & 2 \\ & \pm 1 \\ & 2 \\ & \pm 1 \\ & \pm 1 \\ & \pm 1 \end{aligned}$ | ina $3 / 10^{9}$ $1 / 10^{5}$ ina . 01 $\pm .002$ 2 ina 0.2 2 Hz | $\begin{aligned} & 12 \\ & 1 \\ & 2 \\ & 1 \\ & 1 \\ & 5 \mathrm{mV}-5 \\ & 50 \mathrm{~W} \\ & 00-600 \\ & 1 \\ & 120 \mathrm{~mW} \\ & 40 \mathrm{~mW} \end{aligned}$ | $\begin{array}{\|ll} \hline 8 \\ \text { note } & 15 \\ 5 \\ 3 \\ 7 \\ 1 \\ 1 & \\ 21 & \\ 6 \\ 1 \\ 1 & \end{array}$ | $\begin{aligned} & C \\ & C, R \\ & R \\ & R, R \\ & C \\ & C \\ & C \\ & R \\ & C \\ & C \\ & R \end{aligned}$ | 825 <br> 12,500 <br> request <br> request <br> 400 <br> 2975 <br> 1750 <br> 375 <br> 275 1950 | h <br> h <br> b |
| OS-18 | Weinschel <br> PRD <br> Prec Apparatus <br> Schlumberger <br> Microdot <br> Sierra <br> Gen Radio <br> H-P <br> Gen Radio <br> Weinschel | MS-12A/MO-3 <br> UHF9922 <br> E-200C <br> FS500 <br> 408B <br> 470A-500 <br> 1208-C <br> 3200B <br> 1209-CL <br> MS-2 | 50,000 20,000 88 27,000 200 MHz 200 MHz 65,000 10,000 180 MHz 250 MHz | $\begin{aligned} & 250 \\ & 400 \\ & 440 \\ & 470 \\ & 500 \\ & 500 \\ & 500 \\ & 500 \\ & 600 \\ & 920 \end{aligned}$ | $\begin{aligned} & \pm 1 \\ & \text { ina } \\ & \text { ina } \\ & \text { ina } \\ & \pm 1 \\ & \text { ina } \\ & \pm 2 \\ & \pm 2 \\ & \pm 1 \\ & \pm 1 \end{aligned}$ | $\pm 0.1$ <br> ina ina 5/108 <br> $\pm .002$ <br> $\pm 0.2$ <br> 0.5 <br> $\pm .002$ <br> 0,2 <br> 2 Hz | $\begin{array}{\|l\|} \hline 80 \mathrm{~mW} \\ 2 \\ 80 \\ 1 \\ 50 \mathrm{~W} \\ 50 \mathrm{~W} \\ 240 \mathrm{~mW} \\ 25-200 \mathrm{~mW} \\ 320 \mathrm{~mW} \\ 100 \mathrm{~mW} \\ \hline \end{array}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \text { ina } \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 6 \\ & 1 \end{aligned}$ | R R $C$ $C$ $C$ $C$ $C$ $C$ $C$ $C$ $R$ | 2275 request 120 4925 2850 <br> 2650 325 475 360 2200 | b,d h |

Notes, abbreviations and manufacturers' index at end of this section.

Oscillators $920-6100 \mathrm{MHz}$

|  | Oscillators Manufacturer | Model | FREQUENCY |  |  |  | Output mW | \# of ranges | Type | Price \$ | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{aligned} & \mathrm{Min} \\ & \mathrm{MHz} \end{aligned}$ | Max MHz | $\begin{aligned} & \text { Acc } \\ & \% \end{aligned}$ | Stability \% |  |  |  |  |  |
| OS-19 | Weinschel <br> App Microwave <br> Gen Radio <br> Microdot <br> Sierra <br> Gen Radio <br> Sierra <br> Microdot <br> LFE <br> S-A | $\begin{aligned} & \text { MS-13/MO-3 } \\ & \text { C202 } \\ & 1209-\mathrm{C} \\ & 410 \mathrm{~B} \\ & 470 \mathrm{~A}-1000 \\ & 1361-\mathrm{A} \\ & 470 \mathrm{~A}-1800 \\ & 411 \mathrm{~A} \\ & 831-\mathrm{L}-1 \\ & 2120 / 28-1 \mathrm{~B} \end{aligned}$ | $\begin{aligned} & 250 \\ & 150 \\ & 250 \\ & 500 \\ & 470 \\ & 450 \\ & 1000 \\ & 900 \\ & 1000 \\ & 1000 \end{aligned}$ | 920 <br> 950 <br> 960 <br> 1000 <br> 1000 <br> 1050 <br> 1800 <br> 1800 <br> 2000 <br> 2000 | $\begin{aligned} & \pm 1 \\ & \pm 0.5 \\ & \pm 1 \\ & \pm 1 \\ & \text { ina } \\ & \\ & \pm 1 \\ & \text { ina } \\ & \pm 1 \\ & 0.1 \\ & \pm 5 \end{aligned}$ | $\begin{aligned} & \pm 0.1 \\ & \pm .002 \\ & 0.2 \\ & \pm .002 \\ & \pm 0.2 \\ & 0.2 \\ & .0 \\ & .01 \\ & \pm .002 \\ & 2 / 106 \\ & \pm 0.1 \end{aligned}$ | $\begin{aligned} & \hline 0.1 \\ & 0.1 \\ & 150 \\ & .05 \\ & .05 \\ & \\ & 150 \\ & .04 \\ & .025 \\ & 80 \\ & 100 \end{aligned}$ | $\begin{array}{\|l} \hline 1 \\ 3 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \end{array}$ | $\begin{aligned} & \hline R \\ & \mathrm{R}, \mathrm{R} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C}, \mathrm{R} \\ & \mathrm{C} \end{aligned}$ | 2400 <br> request 360 <br> 2850 <br> 2650 <br> 365 <br> request <br> 2975 <br> 5550 <br> 5450 | b,d <br> d <br> h <br> h <br> d |
| OS-20 | PRD <br> Weinschel S-A <br> PRD <br> Weinschel <br> Gen Radio <br> S-A <br> Weinschel <br> Polarad <br> LFE | L712 <br> L772A <br> 2162 <br> 19922 <br> MS-3 <br> 1218-B <br> 2130 <br> MS-8/MO-3 <br> 1205 <br> 814A-L-9 | 950 <br> 950 <br> 950 <br> 900 <br> 900 <br> 900 <br> 50 <br> 900 <br> 950 <br> 2000 | $\begin{aligned} & 2000 \\ & 2000 \\ & 2000 \\ & 2000 \\ & 2000 \\ & 2000 \\ & 2000 \\ & 2200 \\ & 2400 \\ & 2500 \end{aligned}$ | $\begin{aligned} & \pm 1 \\ & \pm 1 \\ & \pm 1 \\ & \text { ina } \\ & \pm 1 \\ & \pm 1 \\ & \pm 1 \\ & \pm 2 \\ & \pm 1 \\ & \pm 0.5 \\ & 0.1 \end{aligned}$ | ina ina 25 ppm ina 2 Hz <br> 0.1 <br> $\pm 0.5$ <br> $\pm .01$ <br> .0008 | $\begin{aligned} & 10 \\ & 100 \\ & .001 \\ & 0 \mathrm{dBm} \\ & 50 \\ & \\ & 200 \\ & 150 \\ & 20 \\ & 50 \\ & 100 \end{aligned}$ | $\begin{array}{\|l\|} \hline 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 3 \\ 1 \\ 1 \\ 1 \end{array}$ |  | 1195 <br> 1150 <br> 2500 <br> request <br> 2750 <br> 595 <br> 3850 <br> 3200 <br> 1425 <br> 4250 | b,h <br> b <br> b,d <br> i |
| OS-21 | FEL <br> Sierra <br> Gen Radio <br> Microdot <br> Narda <br> Airborne <br> LFE <br> FEL <br> Gen Radio <br> LFE | $\begin{aligned} & \text { CG121L-10C } \\ & 470 A-2500 \\ & 1220-A 1 \\ & 413 A \\ & 451 A \\ & 125 \\ & 814 A-S-1 \\ & \text { CG121S-20C } \\ & 1220-A 2 \\ & 814 A-S-2 \end{aligned}$ | $\begin{array}{\|l\|} \hline 2000 \\ 1800 \\ 2700 \\ 1800 \\ 750 \\ \\ 0.2 \\ 2500 \\ 2500 \\ 2950 \\ 2950 \end{array}$ | $\begin{array}{\|l\|} \hline 2500 \\ 2500 \\ 2960 \\ 3000 \\ 3000 \\ \\ \hline 000 \\ 3050 \\ 3200 \\ 3275 \\ 3600 \end{array}$ | $\begin{aligned} & \pm .01 \\ & \text { ina } \\ & \text { ina } \\ & \pm 1 \\ & \pm 1 \\ & \pm 1 \\ & 0.1 \\ & \pm .01 \\ & \text { ina } \\ & 0.1 \end{aligned}$ | 1 ppm <br> .01 <br> ina <br> $\pm .002$ <br> ina <br> . 004 <br> $5 / 10^{8}$ <br> 1 ppm <br> ina <br> $5 / 10^{8}$ | $\begin{aligned} & 100 \\ & .025 \\ & 1.0 \\ & .005 \\ & 300 \\ & .05 \\ & 75 \\ & 100 \\ & 90 \\ & 80 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 3 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{array}{\|l\|} \hline C \\ C \\ C \\ C \\ C \\ C, R \\ C \\ C \\ C \\ C, R \end{array}$ | 4675 <br> request 385 <br> 3500 <br> 1325 <br> 3450 <br> 3950 <br> 4237 <br> 408 <br> 3950 |  |
| OS-22 | FEL <br> Gen Radio <br> FEL <br> S-A <br> S-A <br> LFE <br> Weinschel <br> PRD <br> S-A <br> Gen Radio | $\begin{aligned} & \text { CG121S-21C } \\ & 1220-A 3 \\ & \text { CG121S-22C } \\ & 2120 / 28-2 \\ & 2163 \\ & 831-S-1 \\ & \text { S772A } \\ & \text { S712 } \\ & 2150 \\ & 1360-B \end{aligned}$ | $\begin{aligned} & 2900 \\ & 3400 \\ & 3300 \\ & 2000 \\ & 2000 \\ & 2000 \\ & 1900 \\ & 1900 \\ & 2000 \\ & 1700 \end{aligned}$ | 3600 3960 4000 4000 4000 4000 4000 4000 4100 4100 | $\begin{aligned} & \pm .01 \\ & \text { ina } \\ & \pm .01 \\ & \pm 5 \\ & \pm 1 \\ & 0.1 \\ & \pm 1 \\ & \pm 1 \\ & 1 \\ & \pm 1 \end{aligned}$ | 1 ppm ina <br> 1 ppm <br> $\pm 0.1$ <br> 25 ppm <br> $2 / 10^{6}$ <br> ina <br> ina <br> 25 ppm <br> 5 ppm | $\begin{aligned} & 100 \\ & 90 \\ & 100 \\ & 70 \\ & .001 \\ & 40 \\ & 100 \\ & 10 \\ & 500 \\ & 50 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 2 \end{aligned}$ | $\begin{aligned} & \hline C \\ & C \\ & C \\ & C \\ & C, R \\ & C, R \\ & C, R \\ & C \\ & C \\ & C, R \end{aligned}$ | $\begin{array}{r} 4237 \\ 415 \\ 5350 \\ 4975 \\ 2500 \\ 4950 \\ 1150 \\ 1010 \\ 2200 \\ 1350 \end{array}$ | d c d d <br> b,h b <br> g |
| OS-23 | Weinschel <br> Strand <br> Polarad <br> RFD <br> LFE <br> FEL <br> Gen Radio <br> FEL <br> Gen Radio <br> FEL | MS-9/MO-3 <br> 800 <br> 1206 <br> 712 <br> 814A-S-31 <br> CG121C-30C <br> 1220-A4 <br> G100C-IR <br> 1220-A5 <br> CG121C-31C | $\begin{aligned} & 2100 \\ & 2100 \\ & 1950 \\ & 1700 \\ & 3700 \\ & 3900 \\ & 3840 \\ & 4625 \\ & 4240 \\ & 4400 \end{aligned}$ | 4200 <br> 4200 <br> 4200 <br> 4200 <br> 4300 <br> 4400 <br> 4460 <br> 4860 <br> 4910 <br> 5000 | $\pm 1$ <br> 0.1 <br> $\pm 0.5$ <br> $\pm 0.25$ <br> 0.1 <br> $\pm .01$ <br> ina <br> .0005 <br> ina <br> $\pm .01$ | $\pm .01$ <br> .001 <br> . 0008 <br> ina <br> $5 / 10^{8}$ <br> 1 ppm ina <br> $\pm .0001$ <br> ina <br> 1 ppm | $\begin{aligned} & 50 \\ & 10 \\ & 50 \\ & \text { ina } \\ & .001 \\ & 100 \\ & 75 \\ & 10 \\ & 100 \\ & 100 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & \mathrm{R} \\ & \mathrm{C}, \mathrm{R} \\ & \mathrm{C} \\ & \mathrm{R} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \\ & \mathrm{C} \end{aligned}$ | 3150 <br> 5950 <br> 1425 <br> ina request <br> 5475 <br> 422 <br> ina <br> 415 <br> 5375 | b,d <br> d <br> c <br> c |
| OS-24 | LFE <br> Strand <br> FEL <br> Gen Radio <br> LFE <br> FEL <br> App Microwave <br> App Microwave <br> App Microwave <br> App Microwave | $\begin{aligned} & \text { 814A-C-10 } \\ & \text { 700-1 } \\ & \text { CG121C-32C } \\ & 1220-A 6 \\ & 814 A-C-1 \\ & \text { G110C-1C } \\ & \text { PG1K } \\ & \text { PH5K } \\ & \text { PH20K } \\ & \text { C201 } \end{aligned}$ | $\begin{aligned} & 5400 \\ & 5300 \\ & 5100 \\ & 5100 \\ & 5100 \\ & 5000 \\ & 100 \\ & 100 \\ & 100 \\ & 150 \end{aligned}$ | $\begin{aligned} & 5900 \\ & 5900 \\ & 5900 \\ & 5900 \\ & 5900 \\ & 6000 \\ & 6000 \\ & 6000 \\ & 6000 \\ & 6100 \end{aligned}$ | 0.1 <br> 0.1 <br> $\pm .01$ <br> ina <br> ina <br> $\pm .0001$ <br> 0.2 <br> 0.2 <br> 0.2 <br> 0.5 | 5/108 <br> .001 <br> 1 ppm ina 5/108 <br> ina <br> .001 <br> . 001 <br> .001 <br> . 002 | $\begin{aligned} & \hline 200 \\ & 50 \\ & 75 \\ & 80 \\ & 60 \\ & 1 \\ & 2 \mathrm{~kW} \\ & 2 \mathrm{~kW} \\ & 20 \mathrm{~kW} \\ & 1-60 \mathrm{~W} \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & \hline C, R \\ & C, R \\ & C \\ & C \\ & C, R \\ & C \\ & C, R \\ & C, R \\ & C, R \\ & C, R \end{aligned}$ | 3950 <br> 3600 <br> 4050 <br> 412 <br> 3750 <br> 14,000 <br> request request request request |  |

Notes, abbreviations and manufacturers' index at end of this section.

## Oscillators $6.1-33.52 \mathrm{GHz}$

|  | Oscillators Manufacturer |  | FREQUENCY |  |  |  | Output mW | \# of ranges | Type | Price \$ | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Model | $\begin{gathered} \mathrm{Min} \\ \mathrm{GHz} \end{gathered}$ | Max GHz | $\begin{aligned} & \text { Acc } \\ & \% \end{aligned}$ | Stability \% |  |  |  |  |  |
| OS-25 | App Microwave <br> Strand <br> FEL <br> Gen Radio <br> Strand <br> LFE <br> LFE <br> Strand <br> Weinschel <br> Gen Radio | PG5K <br> 700 $\begin{aligned} & \text { CG121C-33C } \\ & 1220-A 7 \\ & 700-2 \end{aligned}$ <br> 814A-C-31 <br> 814A-C-12 <br> 700-3 <br> MS-10/MO-3 <br> 1220-A8 | $\begin{aligned} & 0.15 \\ & 5.9 \\ & 5.925 \\ & 5.925 \\ & 6 \\ & 5.9 \\ & 5.4 \\ & 6.5 \\ & 4 \\ & 6.2 \end{aligned}$ | 6.1 <br> 6.3 <br> 6.425 <br> 6.45 <br> 6.5 <br> 6.5 <br> 6.5 <br> 7.3 7. <br> 7.425 | ina <br> 0.1 <br> $\pm .01$ <br> ina <br> 0.1 <br> 0.1 <br> 0.1 <br> 0.1 <br> $\pm 1$ <br> ina | ina <br> .001 <br> 1 ppm ina <br> .001 <br> $5 / 10^{8}$ <br> 5/108 <br> . 001 <br> $\pm .01$ <br> ina | 5 kW .001 100 100 .001 .001 200 .001 50 90 | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & C, R \\ & C, R \\ & C \\ & C \\ & C, R \\ & C, R \\ & C, R \\ & C, R \\ & C, R \\ & R \\ & C \end{aligned}$ | reques <br> 4500 <br> 5290 <br> 388 <br> 4500 <br> request <br> 4650 <br> 4500 <br> 3450 <br> 388 | d <br> b,d <br> c |
| OS-26 | S-A <br> LFE <br> S-A <br> S-A <br> Polarad <br> Weinschel <br> Polarad <br> Strand <br> LFE <br> FEL | $\begin{aligned} & 2120 / 28-4 \\ & 831-\mathrm{C}-1 \\ & 2164-2-8 \\ & 2164-1-8 \\ & 1207-\mathrm{M1} \end{aligned}$ <br> C772A <br> 1207 <br> 750 <br> 814A-X-5 <br> CG121X-40C | $\begin{aligned} & 4 \\ & 4 \\ & 2 \\ & 0.95 \\ & 3.8 \\ & 3.95 \\ & 3.8 \\ & 7.5 \\ & 7.5 \\ & 7.5 \end{aligned}$ | 8 8 8 8 8.1 8.1 8.2 8.2 8.5 8.5 8.5 | $\pm 5$ <br> 0.1 <br> $\pm 1$ <br> $\pm 1$ <br> $\pm 0.5$ <br> $\pm 1$ <br> $\pm 0.5$ <br> 0.1 <br> 0.1 <br> $\pm .01$ | $\pm 0.1$ <br> 5/10 <br> 20 ppm <br> 20 ppm <br> ina <br> ina ina . 001 <br> $5 / 10^{8}$ <br> 1 ppm | $\begin{aligned} & 20 \\ & 20 \\ & .001 \\ & .001 \\ & 80 \\ & 100 \\ & 25 \\ & .001 \\ & 200 \\ & 100 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 2 \\ & 3 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | $C$ $C, R$ $C$ $C$ $C$ $C$ $C, R$ $C$ $C, R$ $C, R$ $C$ | 5375 <br> 4950 <br> 11,700 <br> 15,900 <br> 1950 <br> 1295 <br> 1450 <br> 4500 <br> 4250 <br> 5425 | d <br> d |
| OS-27 | Strand <br> LFE <br> FEL <br> Strand <br> Weinschel <br> LFE <br> LFE <br> FEL <br> Weinschel <br> Strand | 300-A <br> 814A-X-21 <br> CG121X-41C <br> 500 <br> MS-30/MO-4 <br> 814A-X-12 <br> 814A-X-2 <br> CG121X-42C <br> MS-11/MO-3 <br> 230 | $\begin{aligned} & 8.5 \\ & 8.5 \\ & 8.5 \\ & 8.5 \\ & 7.5 \\ & 9.8 \\ & 9 \\ & 9 \\ & 7.2 \\ & 9.6 \end{aligned}$ | 9.6 <br> 10 <br> 10 <br> 10 <br> 10 <br> 10.3 <br> 10.5 <br> 10.5 <br> 10.5 <br> 10.6 | $\begin{aligned} & 5 / 104 \\ & 0.1 \\ & \pm .01 \\ & 0.1 \\ & \pm 0.1 \\ & \\ & 0.1 \\ & 0.1 \\ & \pm .01 \\ & \pm .01 \\ & 0.1 \end{aligned}$ | .001 <br> 5/108 <br> 1 ppm .0001 <br> ina <br> 5/108 <br> 5/108 <br> 1 ppm <br> ina <br> . 001 | $\begin{aligned} & 20 \\ & 500 \\ & 100 \\ & 500 \\ & 50 \\ & \\ & 200 \\ & 55 \\ & 75 \\ & 50 \\ & 50 \\ & 75 \end{aligned}$ | $\begin{array}{\|l\|} \hline 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \end{array}$ | $C$ $C, R$ $C$ $C$ $C, R$ $R$ $C, R$ $C, R$ $C$ $R$ $R$ $C, R$ | 2000 <br> 3750 <br> 3760 <br> 3600 <br> 4320 <br> 4300 <br> 3750 <br> 3730 <br> 3475 <br> request |  |
| OS-28 | Weinschel <br> Polarad <br> LFE <br> PRD <br> FEL <br> Weinschel <br> Strand <br> LFE <br> S-A <br> S-A | X772A <br> 1208 <br> 814A-X-3 <br> X712 <br> CG121X-43C <br> MS-31/MO-4 <br> 400 <br> 831-X-1 <br> 2120/28-8 <br> 2164-2-12 | $\begin{aligned} & 7 \\ & 7.95 \\ & 9.8 \\ & 8.2 \\ & 10.6 \\ & 8.2 \\ & 8.2 \\ & 8.2 \\ & 8 \\ & 2 \end{aligned}$ | $\begin{aligned} & 11 \\ & 11 \\ & 11.2 \\ & 12 \\ & 12.4 \\ & 12.4 \\ & 12.4 \\ & 12.4 \\ & 12.4 \\ & 12.4 \end{aligned}$ | $\begin{aligned} & \pm 1 \\ & \pm 0.5 \\ & 0.1 \\ & \pm 1 \\ & \pm .01 \\ & \pm 0.1 \\ & 0.1 \\ & .05 \\ & \pm 5 \\ & \pm 1 \end{aligned}$ | ina ina $5 / 10^{8}$ ina 1 ppm ina . 001 1/106 $\pm 0.1$ 20 ppm | $\begin{array}{\|l} \hline 100 \\ 25 \\ 500 \\ 10 \\ 75 \\ 50 \\ 60 \\ 50 \\ 20 \\ .001 \end{array}$ | $\begin{array}{\|l} 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 3 \end{array}$ | $\begin{aligned} & C, R \\ & C \\ & C, R \\ & C \\ & C \\ & R \\ & C, R \\ & C, R \\ & C \\ & C \end{aligned}$ | 1295 <br> 1425 <br> 4650 <br> 1300 <br> 5250 <br> 3790 <br> 4500 <br> 4950 <br> 5450 <br> 16,200 | b,h <br> d <br> b,d <br> d |
| OS-29 | S-A <br> FEL <br> LFE <br> Strand <br> FEL <br> FEL <br> Strand <br> Strand <br> LFE <br> Weinschel | 2164-1-12 <br> CG121K-50C <br> 814A-K-21 <br> 210 <br> CG121K-51C <br> CG121K-52C <br> 200 <br> 201 <br> 814A-K-22 <br> MS32/MO-4 | 0.95 <br> 12.8 <br> 12.4 <br> 12.5 <br> 14.2 <br> 15.8 <br> 15.5 <br> 15.5 <br> 15 <br> 12.4 | $\begin{aligned} & 12.4 \\ & 14.2 \\ & 14.5 \\ & 15 \\ & 15.8 \\ & 17.5 \\ & 17.5 \\ & 17.5 \\ & 17.5 \\ & 18 \end{aligned}$ | $\pm 1$ <br> $\pm .02$ <br> 0.1 <br> 0.1 <br> $\pm .02$ <br> $\pm .02$ <br> 0.1 <br> 0.1 <br> 0.1 <br> $\pm 0.1$ | 20 ppm 1 ppm 5/108 . 001 1 ppm <br> 1 ppm . 001 . 001 $5 / 10^{8}$ ina | .001 100 100 125 75 100 15 50 200 25 | $\begin{aligned} & 4 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & C \\ & C \\ & C, R \\ & C, R \\ & C \\ & C \\ & C, R \\ & C, R \\ & C, R \\ & R \end{aligned}$ | 20,400 request <br> 3950 <br> 4000 <br> request <br> request <br> 3600 <br> 3600 <br> 4950 <br> 4350 | d <br> d <br> b,d |
| OS-30 | LFE <br> S-A <br> Polarad <br> LFE <br> Strand <br> Polarad <br> S-A <br> Polarad <br> Polarad <br> Polarad | 831-K-1 <br> 2120/28-12.4 <br> EHF-S1821-5 <br> 817-K-24 <br> 150 <br> EHF-S2225-1 <br> 2120/28-18 <br> EHF-S2427-1 <br> EHF-S2730-1 <br> EHF-S2933-1 | 12.4 <br> 12.4 <br> 18 <br> 23 <br> 23 <br> 22 <br> 18 <br> 24.7 27.27 <br> 29.7 | 18 <br> 18 <br> 22 <br> 25 25 <br> 25 <br> 26.5 <br> 27.5 <br> 30 <br> 33.52 | $\begin{aligned} & 0.1 \\ & \pm 5 \\ & \pm 0.1 \\ & 0.1 \\ & 0.1 \\ & \pm 0.1 \\ & \pm 5 \\ & \pm 0.1 \\ & \pm 0.1 \\ & \pm 0.1 \end{aligned}$ | $\begin{aligned} & 2 / 10^{6} \\ & \pm 0.1 \\ & \text { ina } \\ & 1 / 107 \\ & .001 \\ & \\ & \text { ina } \\ & \pm 0.1 \\ & \text { ina } \\ & \text { ina } \\ & \text { ina } \end{aligned}$ | $\begin{aligned} & 40 \\ & 20 \\ & 10 \\ & 100 \\ & 40 \\ & 10 \\ & 10 \\ & 10 \\ & 10 \\ & 10 \\ & 10 \end{aligned}$ | $\begin{aligned} & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \\ & 1 \end{aligned}$ | $\begin{aligned} & C, R \\ & C \\ & C \\ & C, R \\ & C, R \\ & C \\ & C \\ & C \\ & C \\ & C \\ & C \end{aligned}$ | $\begin{aligned} & 5550 \\ & 5395 \\ & 3545 \\ & 6500 \\ & 4500 \\ & 3545 \\ & 6880 \\ & 3545 \\ & 3575 \\ & 3575 \end{aligned}$ | $d$ $d, i$ <br> $d, i$ <br> d <br> d,i <br> d,i <br> d,i |

Notes, abbreviations and manufacturers' index at end of this section.

Oscillators $36-75 \mathrm{GHz}$

|  | Oscillators Manufacturer |  | FREQUENCY |  |  |  | Output mW | \# of ranges | Type | Price \$ | Notes |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Model | $\begin{aligned} & \mathrm{Min} \\ & \mathrm{GHz} \end{aligned}$ | Max GHz | Acc \% | Stability \% |  |  |  |  |  |
| OS-31 | LFE | 817-K-35 | 34 | 36 | 0.1 | 5/108 | 100 | 1 | C,R | 7500 |  |
|  | Polarad | EHF-S3336-1 | 33.52 | 36.25 | $\pm 0.1$ | ina | 10 | 1 | C | 3575 | $d, i$ |
|  | Strand | 100 | 32 | 37 | 0.1 | . 001 | 16 | 1 | C,R | 5300 |  |
|  | Polarad | EHF-S3540-1 | 35.1 | 39.7 | $\pm 0.1$ | ina | 5 | 1 | C | 3575 | d,i |
|  | S-A | 2120/28-27 | 26.5 | 40 | $\pm 5$ | $\pm 0.1$ | 5 | 1 | C | 7150 | d |
|  | FEL | PLG122 | 2 | 40 | ina | ina | 50 | 1 | C | request | d |
|  | Polarad | EHF-S4046-1 | 39.6 | 46 | $\pm 0.1$ | ina | 3 | 1 | C | 3575 | d,i |
|  | Polarad | EHF-S4640-1 | 45.9 | 50 | $\pm 0.1$ |  | $3$ | 1 | C | $3575$ | d,i |
|  | Strand | $50$ | 50 | 75 | 0.1 | . 001 | 300 | 1 | $C, R$ | request |  |

## Oscillators Late arrivals

|  | Kruse-Storke | 6000-1 | 0.3 | 0.5 | $\pm .05$ | 1/108 | . 0015 | 1 | C,R | 3400 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Kruse-Storke | 6000-2 | 0.3 | 0.5 | $\pm .05$ | 1/108 | . 003 | 1 | C,R | 3600 |  |
|  | Kruse-Storke | 6000-3 | 0.5 | 0.7 | $\pm .05$ | 1/108 | . 001 | 1 | C,R | 3400 |  |
|  | Kruse-Storke | 6000-4 | 0.5 | 0.7 | $\pm .05$ | $1 / 10^{8}$ | . 002 | 1 | C,R | 3600 |  |
| OS-32 | Kruse-Storke | 6000-5 | 0.7 | 1.4 | $\pm .05$ | $1 / 10^{8}$ | . 0005 | 1 | $C, R$ | 3800 |  |
|  | Kruse-Storke | 6000-6 | 0.7 | 1.4 | $\pm .05$ | 1/108 | . 001 | 1 | C,R |  |  |
|  | Kruse-Storke | 6000-7 | 1.4 | 2.1 | $\pm .05$ | 1/108 | . 0005 | 1 | C,R | 4000 |  |
|  | Kruse-Storke | 6000-8 | 2.1 | 3.8 | $\pm .05$ | $1 / 10^{8}$ | . 0002 | 1 | C,R | 4000 |  |
|  | Kruse-Storke | 6000-9 | 2.1 | 3.8 | $\pm .05$ | $1 / 10^{8}$ | . 001 | 1 | $C, R$ | request |  |

Notes, abbreviations and manufacturers' index at end of this section.

## NOTES (Oscillators)

a. Battery operated
b. Also squarewave generator
c. Frequency set by pushbutton or rotary switch
d. Includes basic power supply with interchangeable tuning units
e. Input: $115 / 230 \mathrm{~V}, \pm 10 \%, 60-60 \mathrm{~Hz}$
f. Also squarewave and function generator
g. Also squarewave and pulse generator
h. Also pulse generator
i. Also squarewave and sawtooth generator
i. Programable
k. Frequency synthesizer

1. $+10 d B$ to $-50 d B$
2. $\$ 65$ wired
3. $140 \Omega$ or $600 \Omega$ balanced or unbalanced
4. $0-10 \mathrm{~V}$ in 1 mV steps
5. $0-9 \mathrm{~V}$ in 1 V steps
6. \$1335-2185 depending on options desired
7. Two independent oscillator sections
8. Output impedance $-600 \Omega$
9. Attenuator $111 \mathrm{~dB}, 3$ decade
10. Uncalibrated potentiometer
11. Output impedance $-600-1250 \Omega$
12. Crystal controlled
13. Requires $22-30 \mathrm{~V}$ dc
14. Contains standby power supply
15. Selectable in steps of .01 Hz , also variable through 1 MHz
16. -30 to +10 dBm
17. Input: 48 V dc, $\pm 4 \mathrm{~V}$ positive ground
18. Input: $30 \mathrm{~V} \mathrm{dc}, \pm 3 \mathrm{~V}$ positive ground
19. Includes meter calibrated in volts or dBm
20. Includes X20 meter expand
21. Output impedance $-4000 \Omega$
22. Also 12 V and 60 V
23. Also 15 V and 30 V

## ABBREVIATIONS

C - Cabinet
R - Rack mount
ina - Information not available R-C OSCILLATORS YOU GET MORE THAN ADJUSTABLE FREGUENCY!


MODEL 4004, one of the new K-H all-silicon Variable R-C Oscillators, provides continuously adjustable frequency over the range of 0.001 Hz to 100 kHz . Programmed units also available.

A stable low-distortion signal source is essential for today's complex electronic measurements. You get unsurpassed signal stability and purity in K-H's new line of all-silicon broad band variable R-C Oscillators. Amplitude stability is described, below. Distortion is plotted.


TYPICAL HARMONIC DISTORTION PLOT of K-H Series 4000 R-C Variable Frequency Oscillators.

Stability and signal purity are only two examples of the extra value you get from these modern Krohn-Hite electronic instruments. Other values increase user confidence further by providing simpler, faster and lowercost operation.

Excellent Amplitude Stability: 0.01\%, cycle-to-cycle; 0.01\% per hour.

Sine- and Square-Wave Outputs: Pure sine-wave output - no diode-shaped approximations to produce stepfunction or waveform discontinuities. Square-wave rise and fall times less than 20 nanoseconds.

Quadrature Outputs: Sine and cosine outputs remain within $\pm 1^{\circ}$ of quadrature. Ideal as driver for polyphase variable power sources or simulators for rotary or linear encoders.

There's more in K-H Data Sheet 4000.

## Write for a copy.

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580 Massachusetts Avenue, Cambridge, Mass. 02139 Telephone: 617/491-3211

Index of Manufacturers and Model Numbers
(keyed to table locator symbols)

| Airborne Instrument Laboratory | 1211-C | (OS-16) |
| :---: | :---: | :---: |
|  | 1214-A | (OS-1) |
| 125 (OS-21) | 1214-M | (OS-11) |
|  | 1215-C | (OS-17) |
| Applied Microwave Laboratory | 1218-B | (OS-20) |
| (App Microwave) | 1220-Al | (OS-21) |
|  | 1220-A2 | (OS-21) |
| C201 (OS-24) | 1220-A3 | (OS-22) |
| C202 (OS-19) | 1220-A4 | (OS-23) |
| PGIK (OS-24) | 1220-A5 | (OS-23) |
| PG5K (OS-25) | 1220-A6 | (OS-24) |
| PH5K (OS-24) | 1220-A7 | (OS-25) |
| PH2OK (OS-24) | 1220-A8 | (OS-25) |
|  | 1304-B | (OS-5) |
| Arenburg Ultrasonic Laboratory, Inc (Arenburg) | 1305-A | (OS-2) |
|  | 1307-A | (OS-2) |
|  | 1308-A | (OS-4) |
| PG-650C (OS-17) | 1309-A | (OS-7) |
| PG-650C (OS-17) | 1310-A | (OS-14) |
| B \& K Instruments, Inc | 1311-A | (OS-3) |
|  | 1330-A | (OS-17) |
| 1013 (OS-8) | 1360-B | (OS-22) |
| 1017-A (OS-2) | 1361-A | (OS-19) |
| 1022 (OS-4) |  |  |
| 1024A (OS-3) | Grundig |  |

Barker \& Williamson, Inc (B \& W)
210 (OS-6)
Century Electronics \& Instruments

| $820 B$ | $(O S-11)$ |
| :--- | :--- |
| $821 B$ | $(O S-12)$ |
| $822 B$ | $(O S-13)$ |
| $823 B$ | $(O S-13)$ |
| $824 B$ | $(O S-13)$ |
| $825 B$ | $(O S-13)$ |

Clough-Brengle Co

| $179-A$ | $(O S-3)$ |
| :--- | :--- |
| 402 | $(O S-6)$ |
| 405 | $(O S-6)$ |
| 411 | $(O S-12)$ |
| 420 | $(O S-12)$ |

Electronic Instrument Co, Inc (EICO)
377 (OS-9)

Frequency Engineering Laboratory (FEL)

| CG121C-30C | $($ OS-23) |
| :--- | ---: |
| CG121C-31C | $(O S-23)$ |
| CG12IC-32C | $(O S-24)$ |
| CG121C-33C | $(O S-25)$ |
| CG121K-50C | $(O S-29)$ |
| CG121K-51C | $(O S-29)$ |
| CG121K-52C | $(O S-29)$ |
| CG121L-10C | $(O S-21)$ |
| CG121S-20C | $(O S-21)$ |
| CG121S-21C | $(O S-22)$ |
| CG121S-22C | $(O S-22)$ |
| CG121X-40C | $(O S-26)$ |
| CG121X-41C | $(O S-27)$ |
| CG121X-42C | (OS-27) |
| CG121X-43C | $(O S-28)$ |
| G100C-1R | $(O S-23)$ |
| G110C-1C | $(O S-24)$ |
| PLG122 | $(O S-31)$ |
|  |  |
| General Radio Co (Gen Rad |  |
| 1208-C | $(O S-18)$ |
| $1209-C$ | $(O S-19)$ |
| $1209-C L$ | $(O S-18)$ |
| $1210 C$ | $(O S-9)$ |


| 295 | $(\mathrm{OS}-4)$ |
| :--- | ---: |
| Hallicrafters Co |  |
| CFS-180A | $(\mathrm{OS}-11)$ |
| CFS-250A | $(\mathrm{OS}-11)$ |
| MHS-400 | $(\mathrm{OS}-16)$ |
|  |  |
| Hathaway |  |
|  |  |
| $\mathrm{N}-1$ | $(\mathrm{OS}$ nstruments, Inc |
| $\mathrm{N}-2 \mathrm{~A}$ | (OS-13) |
|  |  |
| Heath Co |  |
|  |  |
| EUW-27 | (OS-12) |
| IG-72 | (OS-7) |
| IG-82 |  |
|  |  |
| Hewlett-Packard | Co (H-P) |


| 100E | (OS-12) |
| :---: | :---: |
| 101A | (OS-11) |
| 106A | (OS-14) |
| 106B | (OS-14) |
| 107AR | (OS-14) |
| 107BR | (OS-15) |
| 200AB | (OS-5) |
| 200CD | (OS-10) |
| 2005 | (OS-10) |
| 201 C | (OS-4) |
| 202-A | (OS-2) |
| 202C | (OS-7) |
| 203A | ( OS-6) |
| 204B | (OS-10) |
| 205AG | (OS-3) |
| 206A | (OS-4) |
| 208A | (OS-10) |
| 236A | (OS-10) |
| 241A | (OS-12) |
| 651B | (OS-15) |
| 652A | (OS-15) |
| 3200B | (OS-18) |
| 3300A/3301A | (OS-8) |
| 5100A/5110A | (OS-17) |
| 5102A | (OS-13) |
| 5103A | (OS-15) |
| H30-241A | (OS-3) |
| H48-241A | (OS-3) |
| Holt Instrument Co |  |
| 448 | (OS-7) |

Industrial Test Equipment Co (Ind Test Equip)

| 600 | $(O S-1)$ |
| :--- | :--- |
| 1040 | $(O S-1)$ |
| $1040-A$ | $(O S-2)$ |
| 1400 | $(O S-1)$ |
| JF-400 | $(O S-1)$ |
| OPS-100 | $(O S-1)$ |

International Electronic Research Corp (IERC)

ADO-102
(OS-7)
ITT - Industrial Products Division

| $74186-C$ | $(O S-3)$ |
| :--- | :--- |
| $74188-D$ | $(O S-11)$ |
| $74188-E$ | $(O S-11)$ |
| $74188-F$ | $(O S-11)$ |
| $74191-A$ | $(O S-1)$ |
| $74191-B$ | $(O S-1)$ |
| $74191-C$ | $(O S-3)$ |
| $74195-B$ | $(O S-16)$ |
| $74213-A$ | $(O S-4)$ |
| $74222-A$ | $(O S-14)$ |
| $74233-B$ | $(O S-4)$ |
| $74254-A$ | $(O S-9)$ |
| $74306-A$ | $(O S-16)$ |
| $74308-A$ | $(O S-14)$ |
|  |  |
| Jerrold Electronics Corp |  |

CM-11
(OS-17)
Kay Electric Co
$990 \quad$ (OS-17)
Krohn-Hite Corp

| $400-C$ | $(O S-2)$ |
| :--- | :--- |
| $420-C$ | $(O S-6)$ |
| $430-A B$ | $(O S-9)$ |
| $440-A$ | $(O S-8)$ |
| $440-B$ | $(O S-2)$ |
| 450 | $(O S-5)$ |
| 452 | $(O S-5)$ |
| 4000 | $(O S-8)$ |
| 4010 | $(O S-8)$ |
| 4020 | $(O S-8)$ |
| 4030 | $(O S-6)$ |

Kruse-Storke Electronics

| $6000-1$ | $(O S-32)$ |
| :--- | :--- |
| $6000-2$ | $(O S-32)$ |
| $6000-3$ | $(O S-32)$ |
| $6000-4$ | $(O S-32$ |
| $6000-5$ | $(O S-32)$ |
| $6000-6$ | $(O S-32)$ |
| $6000-7$ | $(O S-32)$ |
| $6000-8$ | $(O S-32)$ |
| $6000-9$ | $(O S-32)$ |

Laboratory For Electronics, Inc (LFE) Electronics Division

| $814 \mathrm{~A}-\mathrm{C}-1$ | $(O S-24)$ |
| :--- | :--- |
| $814 \mathrm{~A}-\mathrm{C}-10$ | $(O S-24)$ |
| $814 \mathrm{~A}-\mathrm{C}-12$ | $(O S-25)$ |
| $814 \mathrm{~A}-\mathrm{C}-31$ | $(O S-25)$ |
| $814 \mathrm{~A}-\mathrm{K}-21$ | $(O S-29)$ |
| $814 \mathrm{~A}-\mathrm{K}-22$ | $(O S-29)$ |
| $814 \mathrm{~A}-\mathrm{L}-9$ | $(O S-20)$ |
| $814 \mathrm{~A}-\mathrm{S}-1$ | $(O S-21)$ |
| $814 \mathrm{~A}-\mathrm{S}-2$ | $(O S-21)$ |
| $814 A-S-31$ | $(O S-23)$ |
| $814 A-X-2$ | $(O S-27)$ |
| $814 A-X-3$ | $(O S-28)$ |
| $814 A-X-5$ | $(O S-26)$ |
| $814 A-X-12$ | $(O S-27)$ |
| $814 A-X-21$ | $(O S-27)$ |
| $817-K-24$ | $(O S-30)$ |
| $817-\mathrm{K}-35$ | $(O S-31)$ |


(A) SERIES S1077 OSCILLATORS -100 KHz to 10 MHz

- $1 \times 10^{-10} / \mathrm{C}^{\circ}$ from $-20^{\circ}$ to $+55^{\circ} \mathrm{C}$
- $1 \times 10^{-10} \mathrm{RMS}$ Short Term Stability
- Less Than $1 \times 10^{-9} /$ Day Aging
- Voltage Adjust

Coarse and Fine-Internal
Voltage Variable and
Mechanical Fine-External

- Flexible Power Input System
(A) All silicon solid state design using proportional ovens with glass-enclosed crystals assures unexcelled performance -with guaranteed specifications-in frequency and time applications. Ideal for use in digital frequency counters, phase-locked receivers, synthesizers, SSB systems, missile guidance and satellite tracking systems, navigation, computer and communications equipment.
(B) SERIES SLN6039 OSCILLATORS-60 KHz to 10 MHz
- Industry's Fastest Warm-Up-within $5 \times 10^{-9}$ in 10 minutes
- $5 \times 10^{-10}$ or $1 \times 10^{-9} /$ Day Aging
- High MTBF
(B) This oscillator with its wide dynamic range proportional oven and glass-enclosed precision crystal meets many MIL specifications for both airborne and ground equipment.

For full specifications call or write: Motorola Communications \& Electronics, Inc., 4501 Augusta Blvd., Chicago, Illinois 60651. (312) 772-6500. A Subsidiary of Motorola Inc.


## Exclusive!

# Single Dial Source and Detector 



# Simultaneous Tuning of Source and Detector with New Wayne Kerr SR268 (100kHz-100MHz) 

With other systems, it is necessary to tune the source to a specific frequency and then the detector must be tuned to the exact same frequency.
The new Wayne Kerr SR268 Source \& Detector performs both functions simultaneously in a single operation over the range $100 \mathrm{kHz}-100 \mathrm{MHz}$ at a short-term frequency stability of $0.01 \%$. Frequency accuracy over this range is $\pm 2 \%$.

The simplicity of operation provided by ganged tuning is furthered by the incorporation of common-mode rejection transformers in the input and output networks, reducing any interference or cross-talk from unwanted signals.

Operable simultaneously from an external nine-volt battery and a six-volt battery for pilot light indications, SR268 is ideal for field work, too. SR268 is an ideal companion instrument to Wayne Kerr R. F. Bridge B601, VHF Bridge B801B and precision R. F. Bridge B201.

| SPECIFICATIONS |  |
| :--- | :---: |
| Frequency | 100 kHz to 100 MHz |
| Range: | in 9 bands: |
| BAND 1 | $100 \mathrm{kHz} \cdot 216 \mathrm{kHz}$ |
| BAND 2 | $216 \mathrm{kHz} \cdot 465 \mathrm{kHz}$ |
| BAND 3 | $465 \mathrm{kHz} \cdot 1000 \mathrm{kHz}$ |
| BAND 4 | $1.00 \mathrm{MHz} \cdot 2.16 \mathrm{MHz}$ |
| BAND 5 | $2.16 \mathrm{MHz} \cdot 4.65 \mathrm{MHz}$ |
| BAND 6 | $4.65 \mathrm{MHz} \cdot 10.0 \mathrm{MHz}$ |
| BAND 7 | $10.0 \mathrm{MHz} \cdot 21.6 \mathrm{MHz}$ |
| BAND 8 | $21.6 \mathrm{MHz} \cdot 46.5 \mathrm{MHz}$ |
| BAND 9 | $46.5 \mathrm{MHz} \cdot 100 \mathrm{MHz}$ |

## Oscillator Output Level:

Maximum output into 75?: BANDS $1-7,2 \mathrm{rms} ;$ BAND 8, IV rms; BAND 9, 0.5 V rms

Output Level Control: 39 dB in 3dB Steps (75?)

## Detector Sensitivity:

Maximum Input Required for 10\% Meter Reflection: BANDS $1-6,1 \mu \mathrm{~V}$ x $(\mathrm{fMHz})^{1 / 2}$; BANDS $7-8,10 \mu \mathrm{~V}$; BAND $9,30 \mu \mathrm{~V} 46.5 \mathrm{MHz} \cdot 70 \mathrm{MHz}, 20 \mu \mathrm{~V} 70$ $\mathrm{MHz} \cdot 90 \mathrm{MHz}, 10 \mu \mathrm{~V} 90 \mathrm{MHz} \cdot 100 \mathrm{MHz}$ Input Level Control: 4 Steps of 20 dB (nominal)

Weston-Boonschaft \& Fuchs
711A-1
(OS-1)
Manufacturers' addresses and literature offerings in master cross index at front of issue.

| Strand Laboratories, Inc |  |
| :--- | ---: |
| 50 | $(O S-31)$ |
| 100 | $(O S-31)$ |
| 150 | $(O S-30)$ |
| 200 | $(O S-29)$ |
| 201 | $(O S-29)$ |
| 210 | $(O S-29)$ |
| 230 | $(O S-27)$ |
| $300-A$ | $(O S-27)$ |
| 400 | $(O S-28)$ |
| 500 | $(O S-27)$ |
| 700 | $(O S-25)$ |
| $700-1$ | $(O S-24)$ |
| $700-2$ | $(O S-25)$ |
| $700-3$ | $(O S-25)$ |
| 750 | $(O S-26)$ |
| 800 | $(O S-23)$ |


| CPO-1A | $(O S-16)$ |
| :--- | :--- |
| CPS-1 | $(O S-14)$ |
| PMO-4 | $(O S-15)$ |
| TRX-1 | $(O S-16)$ |
| TTG-2 | $(O S-2)$ |
| TTG-2 | $(O S-14)$ |
| VOX-5 | $(O S-17)$ |

Tektronix, Inc
191 (OS-17)
Waveforms, Inc

| 401B | $(O S-7)$ |
| :--- | :--- |
| 401 C | $(O S-7)$ |
| 401 F | $(O S-13)$ |
| 401 H | $(O S-10)$ |
| 402 A | $(O S-14)$ |
| $403 B$ | $(O S-8)$ |
| 452 | $(O S-7)$ |
| 471 B | $(O S-7)$ |
| 471 F | $(O S-13)$ |
| 472 C | $(O S-3)$ |
| $473 B$ | $(O S-7)$ |
| 510B | $(O S-12)$ |
| 510C | $(O S-12)$ |
| 511A | $(O S-15)$ |
| 512F | $(O S-9)$ |

Wayne-Kerr Corp

| O-22D | (OS-15) |
| :--- | :--- |
| S-121 | (OS-8) |

Weinschel Engineering Co, Inc

| C772A | $(O S-26)$ |
| :--- | :--- |
| L772A | $(O S-20)$ |
| $M S-1$ | $(O S-17)$ |
| $M S-2$ | $(O S-18)$ |
| $M S-3$ | $(O S-20)$ |
| $M S-8 / M O-3$ | $(O S-20)$ |
| $M S-9 / M O-3$ | $(O S-23)$ |
| $M S-10 / M O-3$ | $(O S-25)$ |
| $M S-11 / M O-3$ | $(O S-27)$ |
| $M S-12 A / M O-3$ | $(O S-18)$ |
| $M S-13 / M O-3$ | $(O S-19)$ |
| $M S-30 / M O-4$ | $(O S-27)$ |
| $M S-31 / M O-4$ | $(O S-28)$ |
| $M S-32 / M O-4$ | $(O S-29)$ |
| S772A | $(O S-22)$ |
| X772A | $(O S-28)$ |

Random noise generators $35 \mathrm{~Hz}-5400 \mathrm{MHz}$
For information on how to use these tables, turn to page 2

|  |  |  | FRE | ENCY |  | UT |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Manufacturer | Model | Min. MHz | Max. MHz | dB | Meter | Noise Source | Type | $\begin{gathered} \text { Price } \\ \$ \end{gathered}$ | Notes |
| $\begin{gathered} \text { NG- } \\ 1 \end{gathered}$ | Elgenco Elgenco Beckman Belkman Elgenco | 301A 311A 1179 R 1179 A 321A | 0 0 0 0 0 | 35 Hz $35 \mathrm{~Hz} \mathbf{z}^{(6)}$ $35 \mathrm{~Hz}(17)$ 35 Hz 105 Hz | 12 V 12 V 12 V 12 V 12 V | yes yes yes yes yes | note 1 note 1 note 1 note 1 note 1 | $\begin{aligned} & R \\ & R \\ & R \\ & R \\ & R \end{aligned}$ | $\begin{array}{r} 1995 \\ 2895 \\ \text { request } \\ \text { request } \\ 2095 \end{array}$ |  |
|  | Elgenco | 632A | 0 | 350 Hz (10) | 1 V | none | note 8 | C,R | 2475 |  |
|  | Marconi | 7816 | 300 Hz | . 0034 | 1 mW | yes | note 8 | C, R | 1395 |  |
|  | ITT | 74216-A | 20 Hz | . 004 | 20 dBm | yes | note 2 | C | 890 |  |
|  | Allison | 349A | 37 Hz | . 0192 | 2 V | none | note-2 | R | 2050 |  |
|  | Northeast | TTS-56 | 20 Hz | . 02 | $\pm 10 \mathrm{dBm}$ | yes | note 3 | C | 370 |  |
| $\begin{gathered} \text { NG- } \\ 2 \end{gathered}$ | B \& K | 1402 | 20 Hz | . 02 | 40 V |  |  | C,R | 975 |  |
|  | Elgenco | 331A | 10 Hz | . 02 | 5 V | yes | note 5 | R | $1295$ |  |
|  | Beckman | 1179R | 10 Hz | . $022^{(18)}$ | 15 V | yes | note 1 | R | request |  |
|  | Elgenco | 311A |  | . 02 (7) | 12 V | yes | note 1 | R | 2395 |  |
|  | Allison | 650 | 5 Hz | . 03 | 1.5 V | yes | note 3 | C,R | 310 | c |
|  | Elgenco | 632A | 10 Hz | .035(11) | 1 V | none | note 8 | C,R | 2475 |  |
|  | Allison | 348A | 22 Hz | . 045 | 2 V | none | note 2 | R | 1825 |  |
|  | H H Scott | $811-B C$ | 2 Hz | 1.5 | 2.5 V | yes | note 1 | C,R | 275 |  |
|  | Gen Radio | 1390-B 602 A | 5 Hz 5 5 Hz | 5 5 | 3 V 3 V | yes yes | note 1 note 8 | C,R C, R | 335 290 |  |
| $\begin{gathered} \text { NG- } \\ 3 \end{gathered}$ | Elgenco | 603A | 5 Hz | 5 | 3 V | yes | note 8 | C,R | 495 |  |
|  | Elgenco | 624A Series | 5 Hz (9) | 5(9) | 3 V | yes | note 8 | C,R | 245-525 |  |
|  | Elgenco | 610A | 5 Hz | 5 | 1 V | yes | note 8 | C,R | 1175 |  |
|  | R \& S | SUF | 30 Hz | 6 | $1{ }_{\mu} \mathrm{V}-1 \mathrm{~V}$ | yes | note 5 | C | 1590 |  |
|  | Marconi | TF2091 | . 012 | 12.388 | 100 mW | yes | note 4 | C,R | 1495 |  |
|  | Kay | 770 | . 001 | 20 | 0-10 | none | note 19 | C | 250 |  |
|  | H-P | 345B | 30 | 30 |  | yes | note 3 | C,R |  | $a, b$ |
|  | Kay | 240 | 5 | 220 | 0-23.8 | yes | note 3 | C | $375$ |  |
|  | Airborne Kay | $\begin{aligned} & 07006 \\ & 600 \end{aligned}$ | 10 5 |  | $\begin{aligned} & 0-16 \\ & 0-23.8 \end{aligned}$ | none yes | note 5 note 3 | C | $\begin{aligned} & 125 \\ & 1595 \end{aligned}$ |  |
| $\begin{gathered} \text { NG- } \\ 4 \end{gathered}$ |  | 403 | 3 | 500 | 0-19 | yes | note 3 | C | 375 |  |
|  | ARI | NS-C | 1 | 500 | 0-16 | yes | note 3 | C | 450 |  |
|  | Gen Micro | 504 | 1 | 500 | 15.2 | yes | note 3 | C | 225 (16) | $a, b$ |
|  | Gen Micro | 503 | 1 | 500 | 0-19 | yes | note 3 | C | 350 |  |
|  | ARI | NS-LB | 100 Hz | 500 | 0-16 | yes | note 3 | C | 850 | c |
|  | H-P | 343A | 10 | 600 | 5.2 | yos | note 3 | C,R | 100 (23) | $a, b$ |
|  | PRD | 904-A | 30 | 1000 | 0-10,20 | yes | note 5 | C | 490 |  |
|  | Kay | 771 | 10 | 1000 | 0-10 | none | note 19 | C | 250 |  |
|  | R \& S | SKTU | 3 | 1000 |  | yes | note 3 | C | $632$ |  |
|  | Kay | 310A | 1200 | 1400 | $15.8{ }^{(20)}$ | yes | note 1 | C |  | $a, b$ |
| $\begin{gathered} \text { NG- } \\ 5 \end{gathered}$ | Kay | 311A | 1200 | 1400 | 15.8(21) | yes | note 1 | C | 395 (22) | $a, b$ |
|  | Kay | 312A | 1120 | 1700 | 15.8 | yes | note 1 | C | $595(22)$ | $a, b$ |
|  | Airborne | 07002 | ${ }^{0}$ | 2000 | 5.83 | none | note 14 | C | ${ }_{495}^{1100}$ |  |
|  | Kay | 8704 | 1700 | 2600 | 15.8 | yes | note 1 | C | 495 (22) | $a, b$ |
|  | Airborne | 07010 | 200 | 2600 | 15.6 | yes | note 1 | C | $330{ }^{(12)}$ | $a, b$ |
|  | Gen Micro | N501C | 200 | 2600 | 15.6 | yes | note 1 | C | 265 (16) | $a, b$ |
|  | Signalite | TN-3 | 2700 | 2900 | 18.5 | none | note 1 | C | $225{ }^{(25)}$ | $a, b$ |
|  | Kay | 780 |  | 3000 | $20$ | yes | note 3 | C |  |  |
|  | Kay | 880 A | 2200 | 3300 | 15.8 | yes | note 1 | C | $\begin{aligned} & 495(22) \\ & 175(22) \end{aligned}$ | $a, b$ |
|  | Kay | 261A | 2600 | 3900 | 15.8(21) | yes | note 1 | C |  | $a, b$ |
| $\begin{gathered} \text { NG- } \\ 6 \end{gathered}$ |  | 260A | 2600 | 3900 | 15.8(20) | yes | note 1 | C |  |  |
|  | Airborne | 07048 | 2600 | 3950 | 15.3 | yes | note 1 | C | 250 (12) | $a, b$ |
|  | D-B | DBL-140-T | 2600 | 3950 | 16 | yes | note 1 | C | 318 (15) | $a, b$ |
|  | Gen Micro | S501C | 2600 | 3950 | 15.2 | yes | note 1 | ${ }_{c}$ | 300 (16) | $a, b$ |
|  | H-P | S347A | 2600 | 3950 | 15.1 | yes | note 1 | C,R |  | $a, b$ |
|  | Signalite | XN-727 | 2600 | 3950 | 14.5 | none | note 1 | C | request | $a, b$ |
|  | Waveline | 2200-2 | 2600 | 3950 | ina | yes | note 1 | C | $175(24)$ | $a, b$ |
|  | H-P | 349A | 400 | 4000 | 15.6 | yes | note 1 | C,R | 325 (23) | $a, b$ |
|  | Airborne | 07012 | 2000 | 5000 | 15.65 | yes | note 1 | C | 395 (12) | $a, b$ |
|  | Signalite | TN-17 | 4600 | 5400 | 18.5 | none | note 1 | C | request | $a, b$ |

Notes, abbreviations and manufacturers' index at end of this section.

Random noise generators $5800-120,000 \mathrm{MHz}$


Notes, abbreviations and manufacturers' index at end of this section.

## Impulse noise generators $35-21,000 \mathrm{MHz}$



| NOTES | other at $373.1^{\circ} \mathrm{K}$, coaxial switch permits selection. |
| :---: | :---: |
| a. Meter mounted on power supply. | 15. Model DB-2140 power supply add \$200. |
| b. Power supply separate from noise source. <br> c. Battery operated. | 16. Model 551 A automatic noise figure meter add $\$ 1,095$; Model 301 A , add $\$ 125$. |
|  | 17. Dual output, $10 \mathrm{~Hz}-20 \mathrm{kHz}$. |
| 1. Gas tube. | 18. Dual output, $0-35 \mathrm{~Hz}$. |
| 2. Zener diode. | 19. Heated resistive element. |
| 3. Noise diode. | 20. Flourescent source. |
| 4. Silicon diode. | 21. Argon source. |
| 5. Noise pentode. | 22. Model 323-C power supply, add \$125. |
| 6. Dual output, also $0-20 \mathrm{kHz}$. | 23. Model 340B and 342A noise figure meters |
| 7. Dual output, also $0-35 \mathrm{~Hz}$. | at \$715 and \$815 respectively. |
| 8. Solid state. | 24. Model 2200 M or 2200 power supply at |
| 9. Fixed frequencies available, $5,10,20$, 50 and $200 \mathrm{~Hz} ; 20,50,100,200,500 \mathrm{kHz}$ | $\$ 125$ and $\$ 300$, respectively. <br> 25. Type TA-3 power supply, add $\$ 125$. |
| 50 and 200 Hz ; 20, 50, 100, 200, 500 kHz and 5 MHz . | 25. Type TA-3 power supply, add $\$ 125$. |
| 10. Dual output, also $10 \mathrm{~Hz}-35 \mathrm{kHz}$. |  |
| 11. Dual output, also $0-350 \mathrm{~Hz}$. |  |
| 12. Type 71 power supply add \$165; type 74A | ABBREVIATIONS: |
| noise figure indicator add \$765. |  |
| 13. Type 07112 power supply add $\$ 150$ or type | C - Cabinet |
| 74 A noise figure indicator, add \$765. | R - Rack mount |
| 14. Two resistive elements one at $77.3^{\circ} \mathrm{K}$, the | ina - information not available |

## Index of Manufacturers and Model Numbers

(keyed to table locator symbols)

| INDEX |  | B \& K Instruments, Inc |  | 331A | (NG-2) | $\times 501 \mathrm{C}$ | (NG-10) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 1402 | (NG-2) | 602A | (NG-2) | 503 | (NG-4) |
| Aerospace Research, Inc (ARI) |  |  |  | 603A | (NG-3) | 504 | (NG-4) |
|  |  | 610A |  | (NG-3) |  |  |
| NS-C | (NG-4) |  | Beckman Instruments, Inc |  | 624 A Series | (NG-3) | General | Co (Gen Radio) |
| NS-LB (NG-4) |  | $\begin{aligned} & \text { 1179A } \\ & 1179 \mathrm{R} \end{aligned}$ | (NG-1) | 632 A | (NG-1) | 1390-B | (NG-2) |
|  |  | (NG-1) |  |  |  |  |
| Airborne Instrument Laboratory |  |  | Empire Products Singer-Metrics Div |  | Hewlett-Packard Co (H-P) |  |
| 07002 | (NG-5) |  |  |  |  |
| 07004 | (NG-8) | De Mornay-Bonardi Corp (D-B) |  | IG-102 |  |  | (NG-13) | G347A | (NG-7) |
| 07006 | (NG-3) |  |  | IG-115 | (NG-13) | H347A | (NG-9) |
| 07010 | (NG-5) | DBD-140-T | (NG-12) | 118A | (NG-13) | J347A | (NG-8) |
| 07012 | (NG-6) | DBE-140-T | (NG-11) | 118B | (NG-13) | P347A | (NG-11) |
| 07048 | (NG-6) | DBF-140-T | (NG-10) | General Microwave Corp (Gen Micro) |  | S347A | (NG-6) |
| 07049 | (NG-7) | DBG-140-T | (NG-10) |  |  | X347A | (NG-10) |
| 07050 | (NG-8) | DBH-140-T | (NG-9) | A501C | (NG-12) | 343 A | (NG-4) |
| 07051 | (NG-9) | DBJ-140-T | (NG-8) | C501C | (NG-8) | 345 B | (NG-3) |
| 07052 | (NG-10) | DBK-140-T | (NG-7) | E501C | (NG-12) | 349A | (NG-6) |
| 07053 | (NG-11) | DBL-140-T | (NG-6) | F501C | (NG-12) |  |  |
| 07091 | (NG-11) |  |  | G501C | (NG-7) | ITT Indu | oducts Div |
| 07096 | (NG-12) | Elgenco, Inc |  | J501C | (NG-9) |  |  |
|  |  |  |  | K501C | (NG-11) | 74216-A | (NG-1) |
| Allison Laboratories, Inc |  | 301A | (NG-1) | M501C | (NG-12) |  |  |
| 348A | (NG-2) | 311 A | (NG-1) | N501C | (NG-5) | Kay Elec | ompany |
| 349A | (NG-1) |  | (NG-2) | S501C | (NG-6) | 240 | (NG-3) |
| 650 | (NG-2) | 321 A | (NG-1) | U501C | (NG-11) | 260A | (NG-6) |


| 261A | (NG-5) |
| :---: | :---: |
| 270A | (NG-7) |
| 271A | (NG-7) |
| 280A | (NG-8) |
| 281A | (NG-8) |
| 290A | (NG-9) |
| 291A | (NG-9) |
| 300A | (NG-10) |
| 301A | (NG-10) |
| 310A | (NG-4) |
| 311A | (NG-5) |
| 312A | (NG-5) |
| 403 | (NG-4) |
| 521A | (NG-10) |
| 531A | (NG-11) |
| 600 | (NG-3) |
| 770 | (NG-3) |
| 771 | (NG-4) |
| 780 | (NG-5) |
| 870A | (NG-5) |
| 880A | (NG-5) |

Marconi Instruments

| TF2091 | (NG-3) |
| :--- | :---: |
| 7816 | (NG-1) |
| Northeast Electronics Corp |  |
| TTS-56 | (NG-1) |

PRD Electronics,Inc
904-A (NG-4)
Polarad Electronic Instruments

| IC-120A | (NG-13) |
| :--- | :--- |
| IC-120B | (NG-13) |
| IC-121B | (NG-13) |
| IC-122B | (NG-13) |

Rohde \& Schwarz Sales Co, Inc (R\&S)

| SKTU | (NG-4) |
| :--- | :--- |
| SUF | (NG-3) |

H H Scott, Inc
811-BC (NG-2
Signalite, Inc

| TN-1 | (NG-9) |
| :--- | :--- |
| TN-2 | (NG-8) |
| TN-3 | (NG-5) |
| TN-6 | (NG-10) |
| TN-7 | (NG-11) |
| TN-8 | (NG-12) |
| TN-10 | (NG-7) |
| TN-13 | (NG-9) |
| TN-17 | (NG-6) |
| XN-725 | (NG-7) |
| XN-726 | (NG-8) |
| XN-727 | (NG-6) |
| XN-867 | (NG-9) |
| XN-895 | (NG-7) |

Stoddart Electro Systems

| 91263-1 | (NG-13) |
| :--- | :--- |
| $93453-1$ | (NG-13) |

Waveline, Inc

| $2200-2$ | (NG-6) |
| :--- | :--- |
| $2200-3$ | (NG-7) |
| $2200-4$ | (NG-8) |
| $2200-5$ | (NG-9) |
| $2200-6$ | (NG-10) |
| $2200-7$ | (NG-11) |
| $2200-8$ | (NG-11) |
| $2200-10$ | (NG-12) |

Manufacturers' addresses and literature offerings in master cross index at front of issue.


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## Squarewave generators $100 \mathrm{~Hz}-10,000 \mathrm{kHz}$

For information on how to use these tables, turn to page 2

|  |  |  |  | FREQU | ENCY |  |  |  | PUT |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Manufacturer | Model | Min <br> Hz | Max <br> kHz | Rise <br> $\mu \mathrm{s}$ | Fall <br> $\mu_{\mathrm{s}}$ | Min Volts | Max <br> Volts | Imp. ohms | Atten dB | Type | Price \$ | Notes |
| $\begin{gathered} S Q- \\ 1 \end{gathered}$ | ENSCO | FG-113 | 0.1 | 100 Hz | 10 | 10 | 20 | 20 | 600 | note 1 | C | 295 | a |
|  | Weinschel | MO-1C | 1 kHz |  | 5 | 5 | 0 | 150 | 100 k | note 2 | R | 750 |  |
|  | Krohn-Hite | 400-C | . 009 | 1.1 | 2 | 2 | 0 | 10 | 10 k | note 2 | C,R | 465 | a |
|  | Alfred | 305A | 850 | 1.15 | 0.2 | 2 | 0 | 60 | 2.5 k | note 2 | C | 120 |  |
|  | EICO | 377 | 60 | 50 | ina | ina | 10 | 10 | 1 k | cal pot | C | 50 | a |
|  | Krohn-Hite | 420-C | 0.35 | 52 | 2 | 2 | 0 | 20 | 10 k | none | C, R | 410 | a |
|  | Ind Comp |  | 100 kHz | 100 | 1 | 1 | 20 | 2 k |  | none | R | 2250 | - |
|  | Gen Radio | 1309-A | $10$ | 100 | 0.1 | ina | $5$ | 5 | 600 | $20$ | C | 325 | a |
|  | Marconi | TF 1370A | 10 | 100 | 0.4 | ina | . 003 | 3 | note 4 | note 5 | $C, R$ | 995 | a |
|  | Measurements | 71 | 6 | 100 | 0.1 | ina | 0 | 75 | 20/V | note 1 | C | 195 |  |
| SQ-2 | Krohn-Hite | 440-A | . 001 | 100 | 0.5 | 0.5 | 0 | 5 | 1.5 k | none | $C, R$ | 625 | a |
|  | Krohn-Hite | 442-R | . 001 | 100 | 0.5 | 0.5 | 0 | 5 | 1.5 k | note 2 | R | 2375 | a |
|  | RCA | WA-44C | 20 | 200 | 0.15 | 0.15 | 10 | ina | 100 k | ina | C | 99 | a |
|  | Precise | 636 | 20 | 200 | 0.15 | ina | 0 | 10 | 5 k | note 2 | C | 73 | a |
|  | Gen Radio | 1210-C | 20 | 500 | 0.33 | ina | 0 | 30 | 2.5 k | 0-50 | C | 215 | a |
|  | Prec.Apparatus | E-310 |  |  |  |  |  |  | 600 | note 1 | C | 200 | a |
|  | Prec.Apparatus | G-34 | $7$ | $750$ | $0.15$ | ina | 0 | $20$ | 0-3 k |  | C | 100 | a |
|  | Tektronix | 107 | 400 kHz | 1000 | . 003 | ina | 0.1 | 0.5 | $52$ | note 2 | C | 190 |  |
|  | Century Tektronix | $\begin{aligned} & 8207 \\ & 106 \end{aligned}$ | $\begin{aligned} & 100 \\ & 10 \end{aligned}$ | $\begin{aligned} & 1000 \\ & 1000 \end{aligned}$ | $\begin{aligned} & 0.1 \\ & .001, .012 \end{aligned}$ | ina .001 | $\begin{aligned} & 0 \\ & .05(3) \end{aligned}$ | $\begin{aligned} & 10 \\ & 12(3) \end{aligned}$ | $\begin{aligned} & 100 \\ & 50,600 \end{aligned}$ | ina note 2 | $R$ $C$ | $\begin{array}{r} 3400 \\ 590 \end{array}$ | a |
|  | Tektronix |  |  |  | .001,.012 | . 001 |  |  | 50,600 |  | C |  |  |
| SQ-3 | Heath | IG-82 | 20 | 1000 |  |  | 0 |  |  | note 1 |  |  |  |
|  | Century | 821A | 10 | 1000 | 0.1 | ina | 0 | 10 | $100$ | ina | R | 3400 | a |
|  | Hickok | 1715A | 1 | 1000 | . 02 | ina | 7 | 55 | 75,600 | 60 | C | 340 |  |
|  | Century | 822A | 1 | 1000 | 0.1 | ina | 0 | 10 | 100 | ina | R | 3400 | a |
|  | H-P | 211A | 1 | 1000 | .02,0.1 | ina | 3.5 | 27 | 75,600 | 60 | $C, R$ | 350 |  |
|  | Century | 823A | 0.1 | 1000 | 0.1 | ina | 0 | 10 | 100 | ina | R | 3400 | a |
|  | Century | 824A | . 01 | 1000 | 0.1 | ina | 0 | 10 | 100 | ina | R | 3400 | a |
|  | Century | 825A | . 001 | 1000 | 0.1 | ina | 0 | 10 | 100 | ina | R | 3400 | a |
|  | Measurements | 72 | 5 | 5000 | . 05 | ina | 0 | 2,12 | 75,500 | ina | C | 248 |  |
|  | Fairchild | 791A | 25 | 10,000 | . 006 | . 003 | 4 | 40 | 50,600 | note 2 | $C, R$ | 420 |  |

Notes, abbreviations and manufacturers' index at end of this section.

## NOTES

Squarewave Generators
a. Also oscillator.

1. Calibrated potentiometer.
2. Uncalibrated potentiometer.
3. In two steps, $.05-0.5 \mathrm{~V}$ and $0.5-12 \mathrm{~V}$.
4. Four switched settings, $75,100,130$ and 600 ohms.
5. Six 10 dB steps between -50 dB and +10 dB .

## NOTES

Function Generators
a. Output - sine, squarewave and triangle.
b. Output - squarewave, pulse and ramp.
c. Output - sine, squarewave and phase.
d. Output - sine, squarewave, triangle, peak and phase.
e. Output - sine, squarewave, triangle and ramp.
f. Output - sine, squarewave, triangle, ramp and slope.
g. Output - sine, squarewave, pulse and cosine.
h. Battery operated or $110-220 \mathrm{~V}, 50-400 \mathrm{~Hz}$.

1. Varies, $300-0.3 \mathrm{~ms}$.
2. Includes independent timing, triggering and gating which allows cross programing of function.
3. This unit is part of modular system 1000 and can be combined with any number of modules to produce a variety of outputs.
4. Includes variable attenuator and 10 X multiplier.
5. Does not include dc offset and internal modulation.
6. Includes de offset and internal modulation.
7. Direct reading decade attenuator.
8. Uncalibrated potentiometer.
9. Voltage controlled generator, seven simultaneous outputs.
10. Voltage controlled generator, nine outputs, differential output. Starting phase and trigger levels adjustable.
11. Sweep, trigger, voltage controlled generator, nine outputs.
12. Trigger, phase lock, voltage controlled generator, nine outputs.
13. Trigger, phase lock, tone burst, voltage controlled generator, nine outputs.

## ABBREVIATIONS

$C$ - Cabinet
R - Rack mount
ina - information not available.

## Function generators $50 \mathrm{~Hz}-1000 \mathrm{kHz}$

For information on how to use these tables, turn to page 2

|  |  |  |  | FREQU | NCY |  |  |  | TPUT |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Manufacturer | Model | Min Hz | Max kHz | Rise <br> $\mu \mathrm{s}$ | Fall <br> $\mu_{s}$ | Min Volts | Max Volts | Imp. ohms | Atten dB | Type | Price \$ | Notes |
| $\begin{gathered} \text { FG- } \\ 1 \end{gathered}$ | Houston | SG88 | . 005 | 50 Hz | note 1 | ina | 0.2 mV | 22 | 300-3k | ina | C | 2300 | a |
|  | Servo | 1995 | . 005 | $1^{(6)}$ | ina | ina | 0 | 40 | 600 | note 7 | C,R | 3275 | a |
|  | Servo | 1990 | . 005 | $1(5)$ | ina | ina | 0 | 40 | 600 | note 4 | C,R | 2850 | a |
|  | Servo | 1980 | . 005 | $1^{(5)}$ | ina | ina | 0 | 40 | 600 | note 7 | C,R | 2355 | a |
|  | Exact | 331 | . 001 | 1 | 0.5 | 0.5 | 0 | 25 | 500 | 0-100 | $C, R$ | 1195 | a |
|  | Exact | 330 | . 001 | 1 | 0.5 | 0.5 | 0 | 25 | 500 | 0-100 | C,R | 1500 | f |
|  | Canoga | 903A | . 001 | 1 | 200 | 200 | 0 | 30 | ina | ina | R | 3500 | a |
|  | H-P | 202A | . 008 | 1.2 | ina | ina | 0 | 30 |  | 0-100 | C,R | 550 | a |
|  | Antlab | 7207 | 500 | 2.5 | 10 | 10 | 0 | 150 | 100 k | note 1 | C | 372 | b |
|  | Antlab | 7227 | 500 | 2.5 | 10 | 10 | 0 | 150 | 100 k | note 1 | R | 475 | b |
| $\begin{gathered} \text { FG- } \\ 2 \end{gathered}$ | S-A |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  | 2140 | 400 |  |  | ina | 0 | 100 | ina | 0-20-40 | R | 350 | b |
|  | Exact | 255 | . 001 | $10^{(2)}$ | 5 | 5 | 0 | 30 | 400 | 0-100 | $C, R$ | 785 | e |
|  | Exact | 251 | . 001 | 10 | 5 | 5 | 0.1 | 30 | 400 | 50 | C,R | 685 | $f$ |
|  | Exact | 240 | . 001 | 10 | 5 | 5 | 0.1 | 30 | 200 | 50 | C,R | 475 | a |
|  | Exact | 250 | . 001 |  | 5 | 5 | 0.1 | 30 | 400 | 50 | $C, R$ | 595 | e |
|  | H-P | 203A | . 005 | 60 | 0.2 | 0.2 | 0 | 30 | 600 |  | C,R |  |  |
|  | Canoga | 910A | . 01 | 99 | 10 | 10 | 0 | 10 | 1 | cal pot | C,R | $4285$ | d |
|  | Krohn-Hite | 4030 | 0.1 | 99.9 | . 02 | . 02 | 0 | 5 | ina | note 8 | R | request | g |
|  | Krohn-Hite $\mathrm{H}-\mathrm{P}$ | $\begin{aligned} & 4004 \\ & 3300 \mathrm{~A} \end{aligned}$ | 0.1 | 100 | . 02 | . 02 | 0 | 5 | 50 | note 1 | C, R | 1025 | b |
|  |  | 3301A | . 01 | 100 | 0.25 | 0.25 | 0 | 35 | 600 | yes | C,R | 590 | a |
| $\begin{gathered} \text { FG- } \\ 3 \end{gathered}$ | Exact | G1103 | . 01 | 100 | note 3 | note 3 | 10 | 10 | 50 | none | note 3 | 165 (3) |  |
|  | Argonaut | LRG051 | $\text { . } 01$ | $100$ | $2$ | $2$ | 0 | 100 | 1 k | yes | C | 225 | b |
|  | Krohn-Hite | 4024 | . 001 | 100 | $.02$ | . 02 | 0 | 5 | 50 | note 1 | $C, R$ | $1100$ | b |
|  | Exact | G1102 | . 0005 | 100 | note 3 | note 3 | 10 | 10 | 50 | none | note 3 | 190(3) |  |
|  | Anadex | CU-2 | 0.5 | 600 | . 09 | ina | 0 | 20 | 1 k | note 2 | C | 650 |  |
|  | Exact | G1101 |  |  |  | note 3 |  | $10$ | 50 | note 3 | note 3 | $165(3)$ |  |
|  | Wavetek | 155 | . 01 | 1000 | . 005 | . 005 | $\text { ו } 0 .$ | $10$ | 50 | note 7 | R | $1195$ |  |
|  | Wavetek | 110 | . 005 | 1000 | . 005 | . 005 | . 015 | 32.5 | 50 | note 8 | $C, R$ | $445$ | $a, h$ |
|  | Exact | $301$ | $.001$ | $1000$ | $\text { . } 01$ | $\text { . } 01$ | $0$ | $10$ | 52 | ina | $C, R$ | $550$ | a |
|  | Wavetek |  | . 0015 |  |  |  | . 015 |  | 50 | note 8 | $C, R$ | $795$ | e,h |
| FG- | Wavetek | 112 | . 0015 | $1000{ }^{(10)}$ | . 005 | . 005 | . 015 | 32.5 | 50 | note 8 | C,R | 695 | e,h |
|  | Wavetek | 111 | . 0015 | $1000{ }^{(9)}$ | . 005 | . 005 | . 015 | 32.5 | 50 | note 8 | C,R | 545 | e,h |
|  | Wavetek | 116 | . 0015 | $1000{ }^{(13)}$ | . 005 | . 005 | . 015 | 32.5 | 50 | note 8 | C,R | 845 | e,h |
|  | Wavetek | 115 | . 0015 | 1000(12) | . 005 | . 005 | . 015 | 32.5 | 50 | note 8 | $C, R$ | 745 | e,h |

Notes, abbreviations and manufacturers' index at end of this section.

# Index of Manufacturers and Model Numbers 

(keyed to table locator symbols)

| Canoga Electronic Products |  | Alfred Electronics |  |
| :---: | :---: | :---: | :---: |
| 903A | (FG-1) | 305A | (SQ-1) |
| 910A | (FG-2) |  |  |
|  |  | Anadex | ents, Inc |
| Century Electronics \& Instruments |  |  |  |
|  |  | $\mathrm{CU}-2$ | (FG-3) |
| 820A | (SQ-2) |  |  |
| 821A | (SQ-3) | Antlab, |  |
| 822A | (SQ-3) | Antlab, |  |
| 823A | (SQ-3) |  |  |
| 824A | (SQ-3) | $\begin{aligned} & 7207 \\ & 7027 \end{aligned}$ | (FG-1) |
| 825A | (SQ-3) | 7227 | (FG-1) |
| Electronic Instrument Co, Inc (EICO) |  | Argonaut Associates, Inc |  |
| 377 | (SQ-1) | LRG 05 | (FG-3) |



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| ELECTRONIC NEWS | 9 | 9 | 19.7 | 49.6 |

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As always, Electronic Design welcomes suggestions from its readers. Has this issue helped you? Have you any suggestions on how to make issues such as this more useful to design engineers? Drop us a line and let us know.

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